

# MK 66 ROCKET MOTOR/HELICOPTER COMPATIBILITY PROGRAM

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### **ERIC HAWLEY**

Contact Information Ph: (301) 744-1822 Fax: (301) 744-4410 hawleyej@ih.navy.mil

### INDIAN HEAD DIVISION NAVAL SURFACE WARFARE CENTER INDIAN HEAD, MD



# **Helicopter Engine Compatibility Background**

- Problem description:
  - AH-1F downed with fatalities in 1988 while firing MK 66 Rocket Motors
  - Army investigation concluded that the accident was caused by engine ingestion of high-temperature, oxygen-depleted rocket exhaust gasses
    - AH-1 physical mod implemented (air scoop)





# **Helicopter Engine Compatibility Background**

- AH-64 testing identifies rocket exhaust ingestion into engines still a problem
  - Causes engine torque splits and torque fluctuations (surges)
  - Physical mod to aircraft considered not practical
  - Firing restrictions in effect





# **Helicopter Engine Compatibility Background**

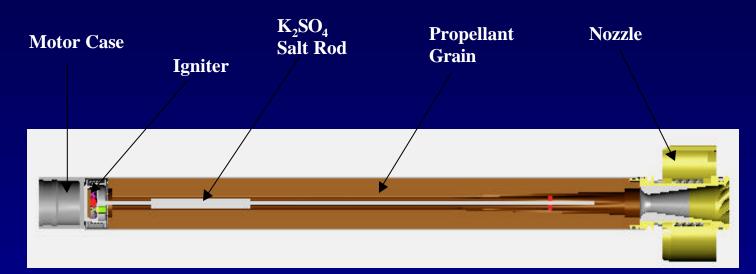
- High temperature oxygen depleted rocket exhaust caused by secondary combustion
- Secondary combustion (afterburning) occurs when CO and H<sub>2</sub> in the exhaust react with oxygen in atmosphere

Combustion Component	Exit Composition (mole fraction)
$CO_2$	0.1898
CO	0.33007
$H_2O$	0.18146
$H_2$	0.17295
$N_2$	0.12218
Pb	0.00177
Cu	0.00177

### **Current MK 66 exhaust components**



# MK 66 Rocket Motor Background



### MK 66 MOD 4 ROCKET MOTOR



# **Helicopter Engine Compatibility Approach**

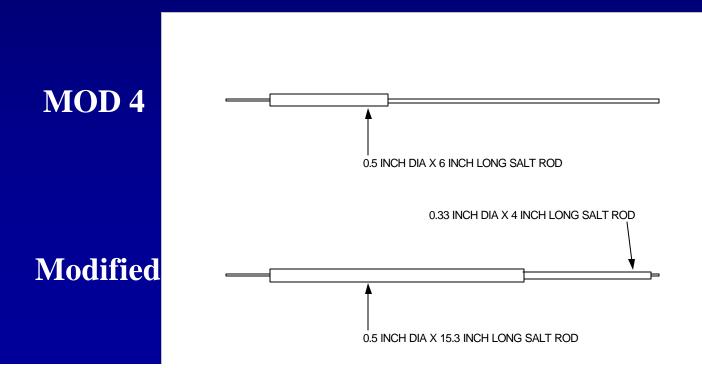
- Secondary combustion can be suppressed by introducing more potassium sulfate (K<sub>2</sub>SO<sub>4</sub>) into motor exhaust
  - Mod 0-4 Salt Rod addresses rocket exhaust ingestion issue in fixed wing aircraft
  - Helicopter ingestion situation is the same
    - Ingestion timeline is different
    - Existing salt rod consumed in 6 feet of motion
    - Helicopters need salt rod effect through rotor downwash
    - Army Aviation Engineering specifies 30 feet as necessary





# **Salt Rod Modification**

- There is a linear relationship between salt volume and duration of afterburning suppression
- Amount and shape of salt rod modified to increase effectiveness for 30 feet
- Enlarged salt rod contains ~ 3x more K<sub>2</sub>SO<sub>4</sub>



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# **Exhaust Chemical Analysis**

• K<sub>2</sub>SO<sub>4</sub> reactions

- Afterburning reaction:  $2CO + 3H_2 + 2OH + 2O_2 => 2CO_2 + 4H_2O$ 

Atmospheric oxygen

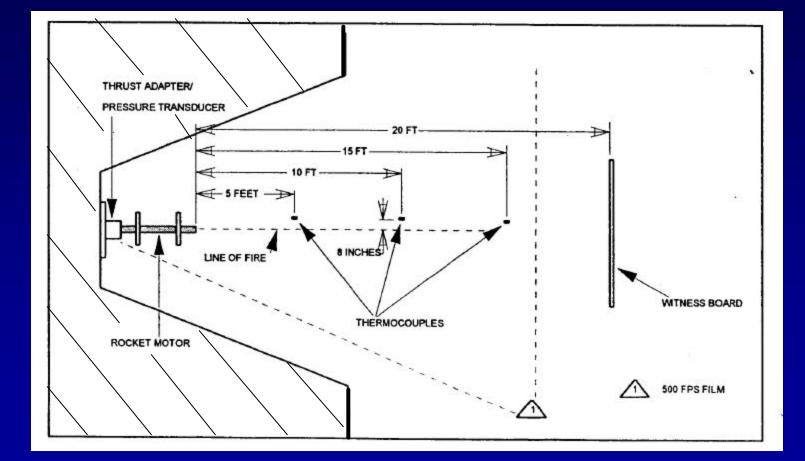
– Reaction with K<sub>2</sub>SO<sub>4</sub>:

 $\overline{K_2SO_4 + 2CO + 3H_2 + 2OH + 2O_2} = 2CO_2 + 3H_2O + H_2S + KO + K + 2O_2$ 

- K<sub>2</sub>SO<sub>4</sub> provides oxygen to the exhaust, which delays the overall reaction of the exhaust fuels (H<sub>2</sub> and CO) with the atmospheric oxygen (O<sub>2</sub>)



## **Static Fire Test**

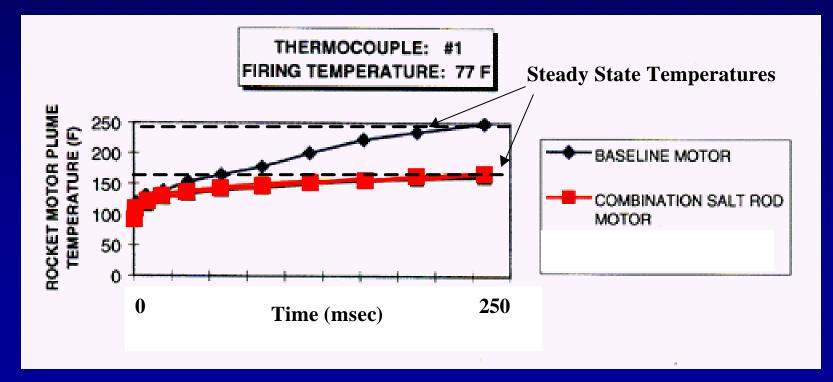


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### **Static Fire Test Results**

 Motor exhaust temperature found to be more than 20% lower than current MK 66 motors at 77 F and 150 F

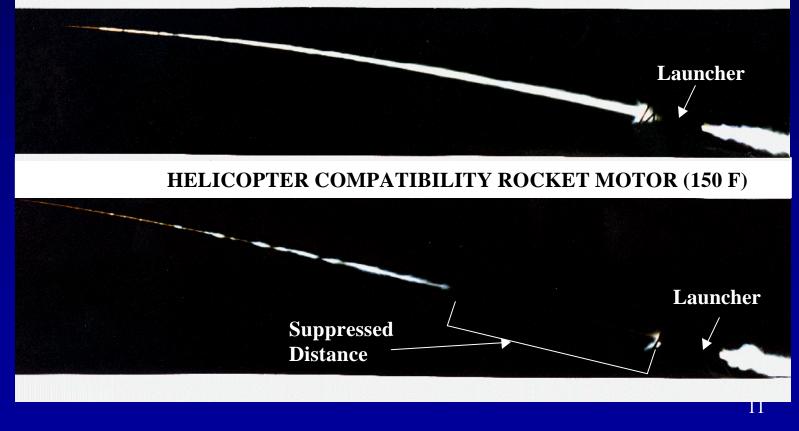




## **Ground Launch Results**

## • Suppressed flight distance >30 ft average

MK 66 MOD 3 ROCKET MOTOR (150 F)



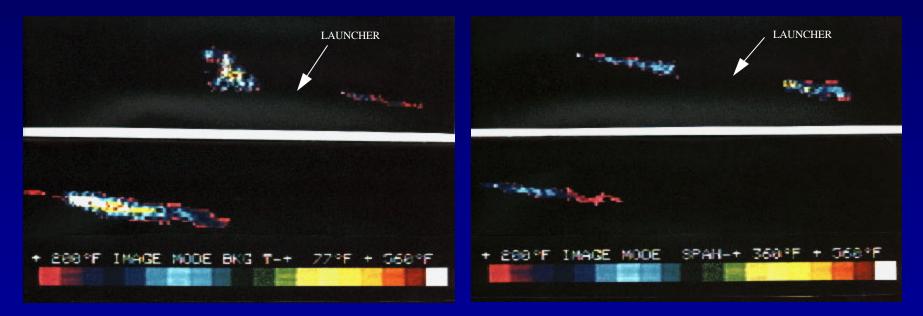


## **Ground Launch Results**

### • Ground launch thermal data

#### MK 66 MOD 3 ROCKET MOTOR (150 F)

#### HELICOPTER COMPATIBILITY ROCKET MOTOR (150 F)





# **Air Launch Verification**

- Air launch test on an instrumented AH-64A with MK 66 motors w/ enlarged salt rod conducted in 1998
- Test conditions
  - 10 knot wind restrictions
  - Altitude was 150 ft
  - Air temperature was in upper 70s, 70-80% RH
  - Test pass/fail criteria:
    - Torque split exceeds 15%,
    - Main engine torque fluctuations of ±15%,
    - Tail rotor torque fluctuations of ±500 ft-lbs



# **Air Launch Results**

# • All engine surge conditions eliminated except one

### - Hover: All surge conditions eliminated

### - 40 kts forward flight: All conditions but one eliminated

CONDITION	LEFT OU	TBOARD	LEFT IN	BOARD	RIGHT I	NBOARD	RIGHT O	UTBOARD	MK 66 MOD 3	HELICOPTER COMP
	ROCKET	ROCKETS	ROCKET	ROCKETS	ROCKET	ROCKETS	ROCKET	ROCKETS	ROCKET MOTOR	ROCKET MOTOR
	DENSITY	FIRED	DENSITY	FIRED	DENSITY	FIRED	DENSITY	FIRED		
HOVER	10	2								
	8	8								
	12	12								
	19	19								
	19	19					19	19		
			14	2					1	TESTED TWICE
			12	4					1	TESTED TWICE
			8	8						
					19	2				
					17	2				
					15	2				
	16	4								
	12	12								
	19	19								
			19	2/1					1	1, 1 (NOTE 1)
			17	2/1					1	1 (NOTE 2)
40 KTAS FORWARD			15	2						
			2	2						
					19	2			1	TESTED TWICE
					17	2			1	TESTED TWICE
					15	2			1	TESTED TWICE
	12	4					12	4	1	TESTED TWICE
	8	8					8	8	5	



## Air Launch Results (cont.)

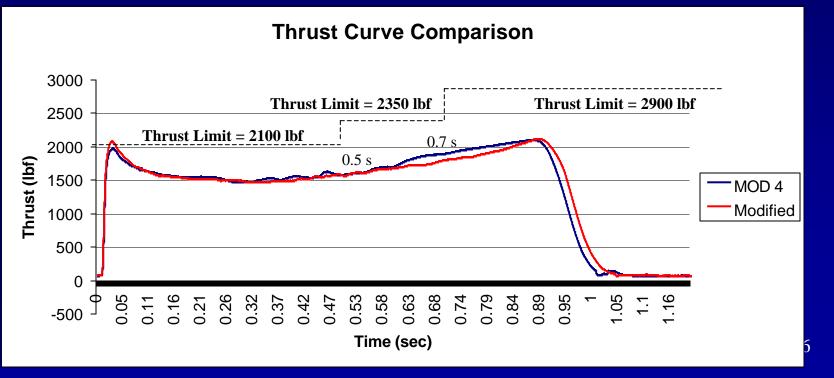
• Worst condition: 40 kts forward flight, one or two rockets fired from left inboard launcher





## **Internal Pressure Concerns**

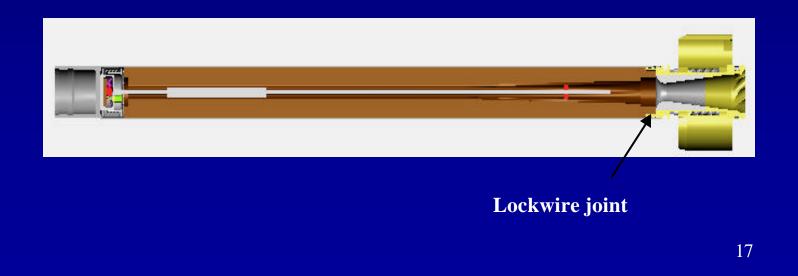
- Enlarged salt rod causes ignition pressure spikes
  - Enlarged salt rod known to increase pressure, and therefore thrust during ~ 0.10 second of burn
  - Measured thrust values near MK 66 specification limit of 2100 lbf





## **Pressure Differential Test**

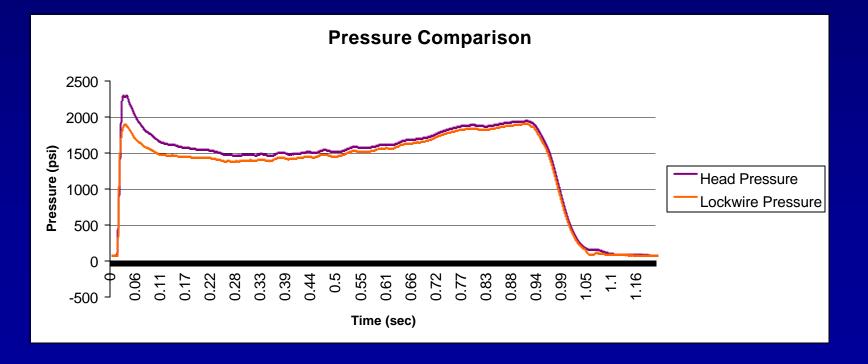
- Thrust requirement derived from internal forward end measured pressures
- Aft end known to be weakest point on motor (lockwire joint)
- Efforts made to measure pressure at aft end





## **Pressure Differential Test**

- Pressure differential test performed at Indian Head in June 2002
  - Previous analysis predicted a 350 500 psi drop at 150°F
  - Aft pressures measured ~400 psi lower than forward end during first 0.10 seconds at 150°F

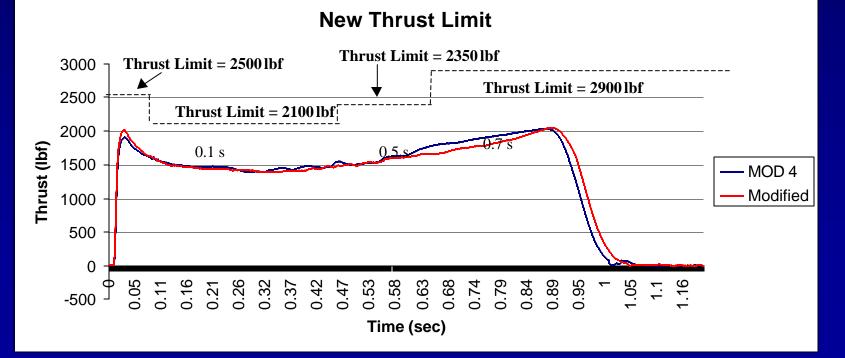




## **Pressure Differential Test Results**

• Thrust limit redefined based on aft end pressures

- Recommended a new thrust limit of 2500 lbf for the first 0.10 seconds of burn
  - Maintains motor tube factor of safety of 1.5
  - Verified by analysis and historical data





# **Future Work**

- Enlarged salt rod design will be incorporated into the MK 66 MOD 6
- Qualification of MOD 6 scheduled to begin in this spring
  - Qualification includes:
    - Environmental Tests
    - Ground Launch
    - Air Launch
- Due to enter production midway through FY04



# Questions

## **Contact Information**

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