



# Chemical Agent Fate Program (CAFP)

## Development of an Evaporation Model for HD on Non-Porous Surfaces

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# Objectives

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- To develop a **simple engineering** tool that can **predict** the evaporation rate of HD on non-porous surfaces and provide information about
  - The amount of mass being evaporated and transported by the wind
  - The amount of mass being absorbed/desorbed into a porous substrate
  - The basic behavior of a drop under the outdoor conditions



# Scientific Problems to Be Addressed

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## ➤ Evaporation

- Modeling sessile drop behavior

## ➤ Validation

## ➤ Generalization

- How to generalize our efforts to enhance prediction capability by

- ✓ A hybrid approach
- ✓ Imposing outdoor conditions

## ➤ Linkage to porous substrate



# Evaporation Module

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- A module that is mostly based on first principles and provides the following information
  - Forcing function - the evaporation rate,  $\dot{m}$ 
    - ✓ Can be modified, improved, replaced, ...
  - Topology of the droplet by solving a differential equation using the forcing function
  - Evaporated mass being added to the atmospheric air
  - Remaining mass to be transported through the porous substrate



# Evaporation Module (*cont'd*)

## Model Development

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### ► Forcing Function

#### ■ Constant base area for a drop (Model A)

$$\dot{m} = 2\pi C R_s f \frac{\mu}{R} (F + C_1 Re^m r^n) \ell n(1 + B) = 2\pi C R_s \frac{\mu}{R} (F + C_1 Re^m r^n) \ell n(1 + B_M)$$

$$C = \frac{h}{R}$$

#### ■ Shrinking base area for a drop (Model B)

$$\dot{m} = 2\pi R_s (1 - \varphi) f \frac{\mu}{R} (F + C_1 Re^m r^n) \ell n(1 + B) \quad or$$

$$\dot{m} = 2\pi R_s (1 - \varphi) f \frac{\mu}{R} (F + C_1 Re^m r^n) \ell n(1 + B_M)$$



# Evaporation Module (*cont'd*)

## Model Development

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### ► Interaction among drops – Group Theory

■ **Model 1:**  $G_{evap} = \frac{1}{1 + G_c}$  with  $G_c = \frac{C(F + C_1 \dots m \dots n) N^q \left(\frac{r}{\lambda}\right)}{1}$

Where  $C$  and  $q$  can be determined experimentally.  $C=3$  and  $q=2/3$

■ **Model 2:**

$$G_c = \sum_{n=0}^{\infty} \frac{(-1)^n \eta_0}{[(n+1)\eta_0]}$$

Where  $\eta_0 = \dots^{-1} \left(\frac{\lambda}{R}\right)$  and  $2\lambda$  represents the distance between two drops

$$\lambda = \frac{1}{2N^p}$$

where  $N$  is the number of drops and  $p = 1/3$

$$G_{evap} = \begin{cases} G_c^q & \text{for } N \geq n \\ \frac{1}{q} G_c^q & \text{for } N < n \end{cases}$$



# Evaporation Module (*cont'd*)

## Model Development

➤ ( $\dot{m}$  is a function of time also)

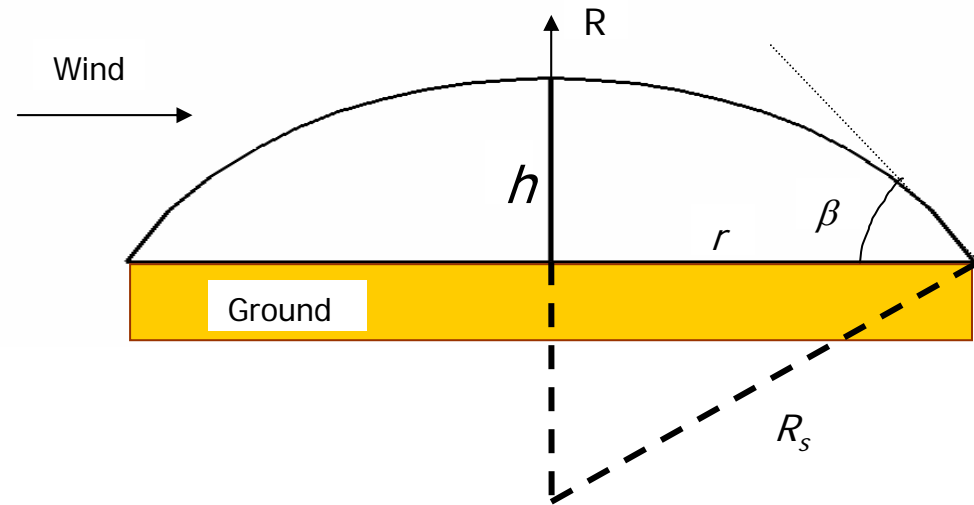
➤ Model A

$$\frac{dh}{dt} = \frac{-\dot{m}}{\pi \rho_\ell h^2 \left( \frac{3}{C} - 1 \right)}$$

$$h/R = C$$

➤ Model B

$$\frac{dh}{dt} = \frac{-\dot{m}}{\rho_\ell \frac{\pi}{2} (r^2 + h^2)}$$





# Evaporation Module (*cont'd*)

## How to Predict Other Scenarios?

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- Validate Model
- Create a matrix for the entire possible domain of operation
- Fill the matrix using the analytical model
- Use neural network curve-fit
- Create a simple engineering equation for application

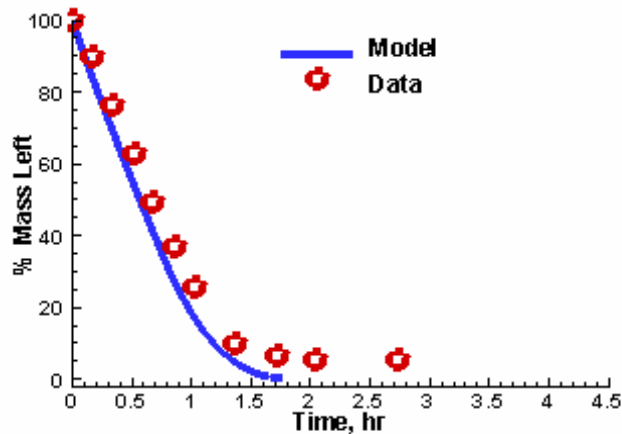




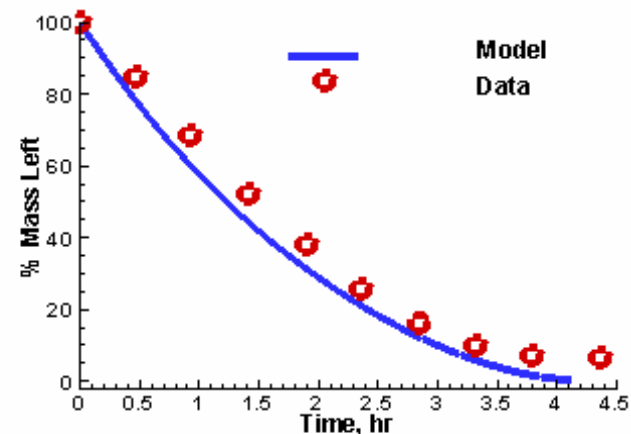
# Evaporation Module (*cont'd*)

## Validation

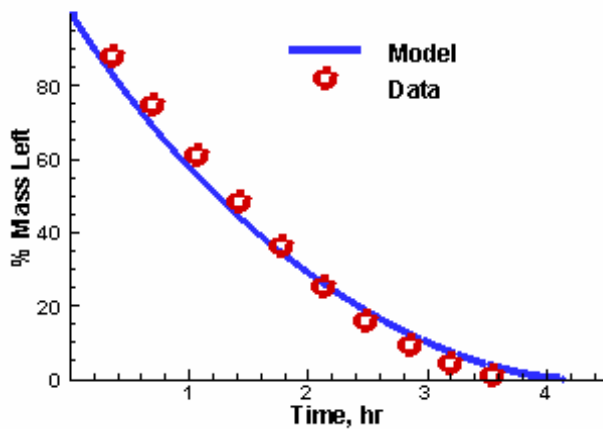
HD on Glass, Wind Velocity = 1.77 m/s, Drop Size = 1  $\mu\text{L}$   
Air Temperature = 35°C, m=1.180 mg



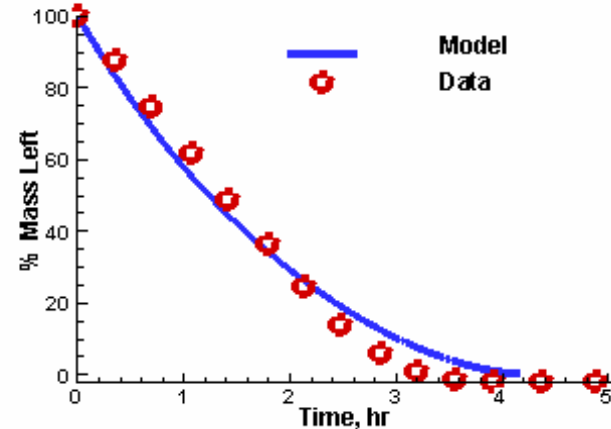
HD on Glass, Wind Velocity = 0.26 m/s, Drop Size = 1  $\mu\text{L}$   
Air Temperature = 35°C, m=1.184 mg



HD on Glass, Wind Velocity = 0.26 m/s, Drop Size = 1  $\mu\text{L}$   
Air Temperature = 35°C, m=1.192 mg



HD on Glass, Wind Velocity = 0.26 m/s, Drop Size = 1  $\mu\text{L}$   
Air Temperature = 35°C, m=1.204 mg

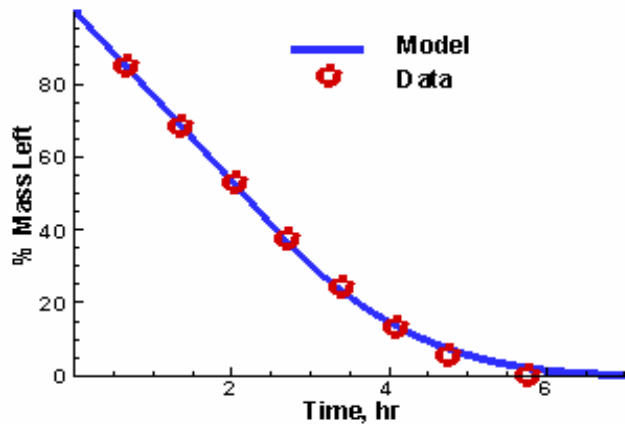




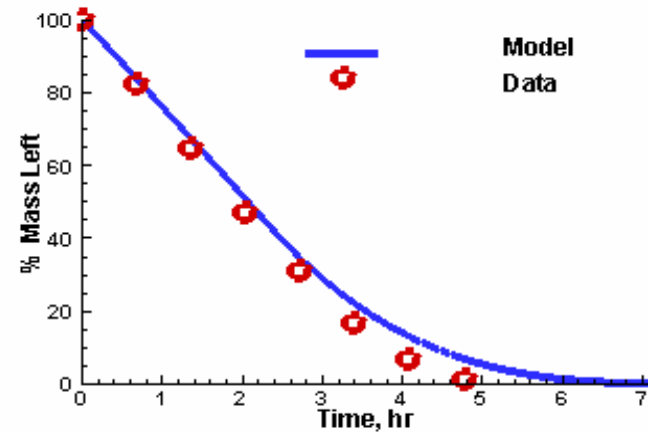
# Evaporation Module (*cont'd*)

## HD on Non-Porous Surface

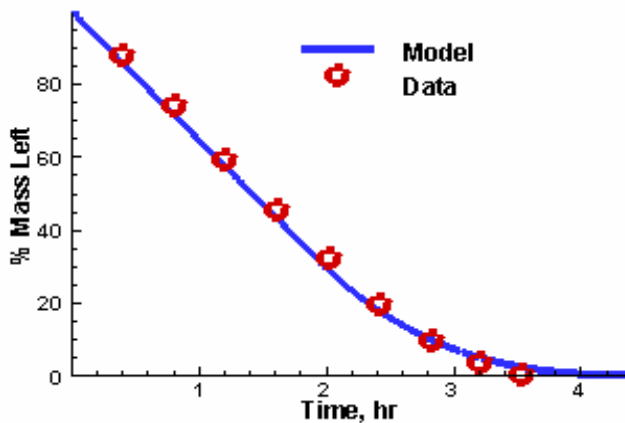
HD on Glass, Wind Velocity = 3.66 m/s, Drop Size = 1  $\mu\text{L}$   
Air Temperature = 15°C, m=1.200mg



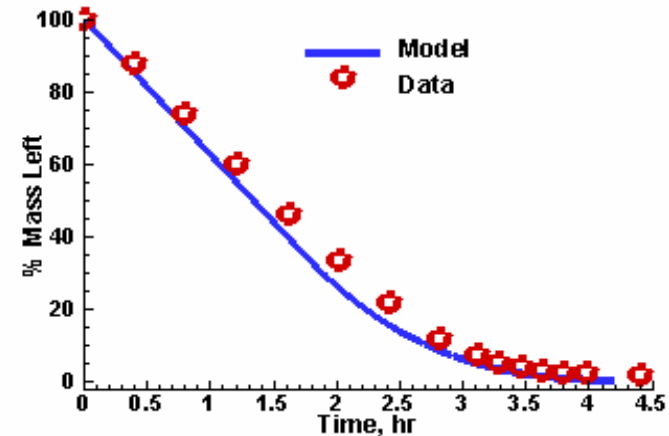
HD on Glass, Wind Velocity = 3.66 m/s, Drop Size = 1  $\mu\text{L}$   
Air Temperature = 15°C, m=1.264 mg



HD on Glass, Wind Velocity = 1.77 m/s, Drop Size = 6  $\mu\text{L}$   
Air Temperature = 35°C, m=6.884 mg



HD on Glass, Wind Velocity = 1.77 m/s, Drop Size = 6  $\mu\text{L}$   
Air Temperature = 35°C, m=7.000mg

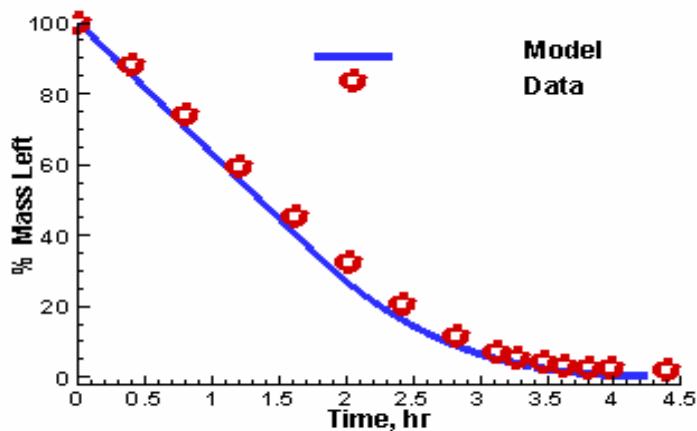




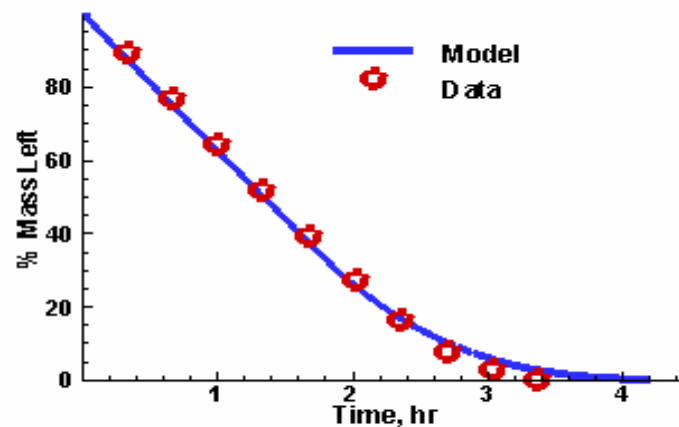
# Evaporation Module (*cont'd*)

## HD on Non-Porous Surface

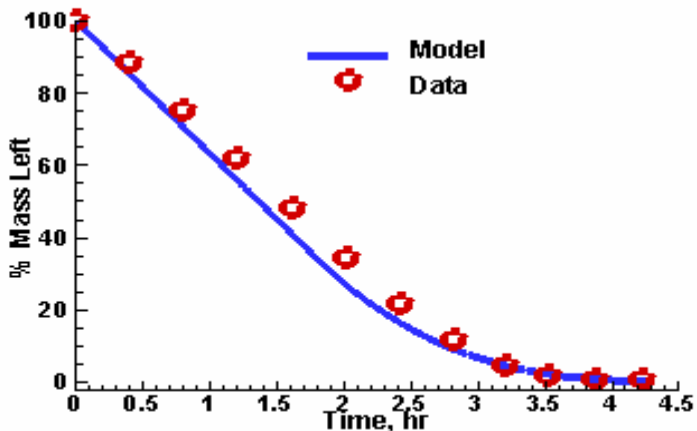
HD on Glass, Wind Velocity = 1.77 m/s, Drop Size = 6  $\mu\text{L}$   
Air Temperature = 35°C, m=7.244 mg



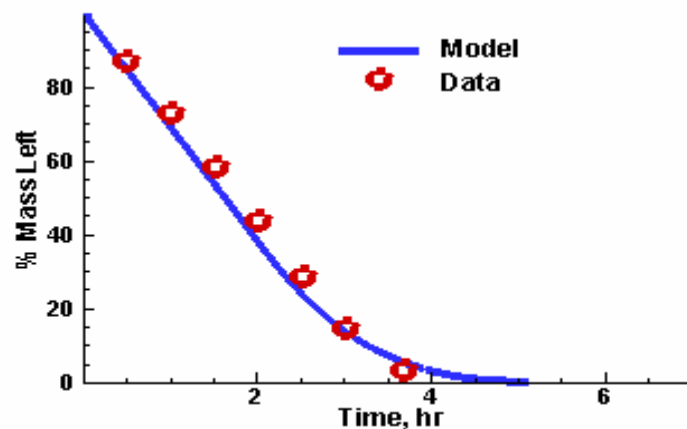
HD on Glass, Wind Velocity = 1.77 m/s, Drop Size = 6  $\mu\text{L}$   
Air Temperature = 35°C, m=7.022 mg



HD on Glass, Wind Velocity = 1.77 m/s, Drop Size = 6  $\mu\text{L}$   
Air Temperature = 35°C, m=7.364 mg



HD on Glass, Wind Velocity = 1.77 m/s, Drop Size = 9  $\mu\text{L}$   
Air Temperature = 35°C, m=12.033 mg





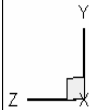
# Evaporation Module (*cont'd*) - HD on Non-Porous Surface - *Droplet Topology*

## ➤ Sample animated droplet topology

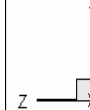
1  $\mu\text{L}$  drop @ 35°C,  $u^*$  @ 0.1038 m/s @ 35°C  
1.33 hours



6  $\mu\text{L}$  drop @ 35°C,  $u^*$  @ 0.1038 m/s @ 35°C  
3.08 hours



9  $\mu\text{L}$  drop @ 35°C,  $u^*$  @ 0.1038 m/s @ 35°C  
3.44 hours

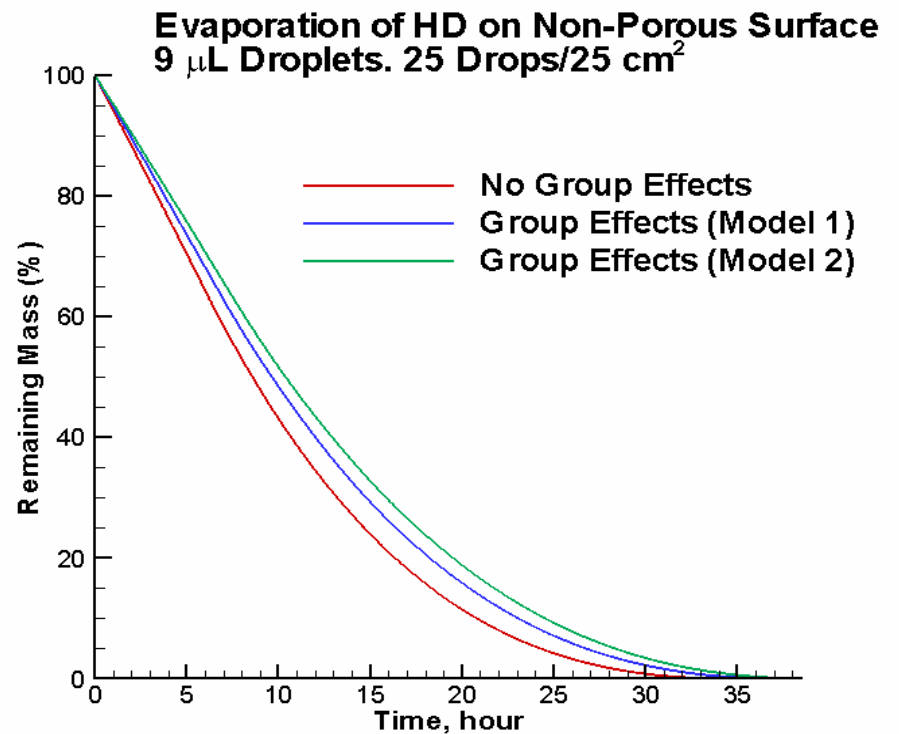
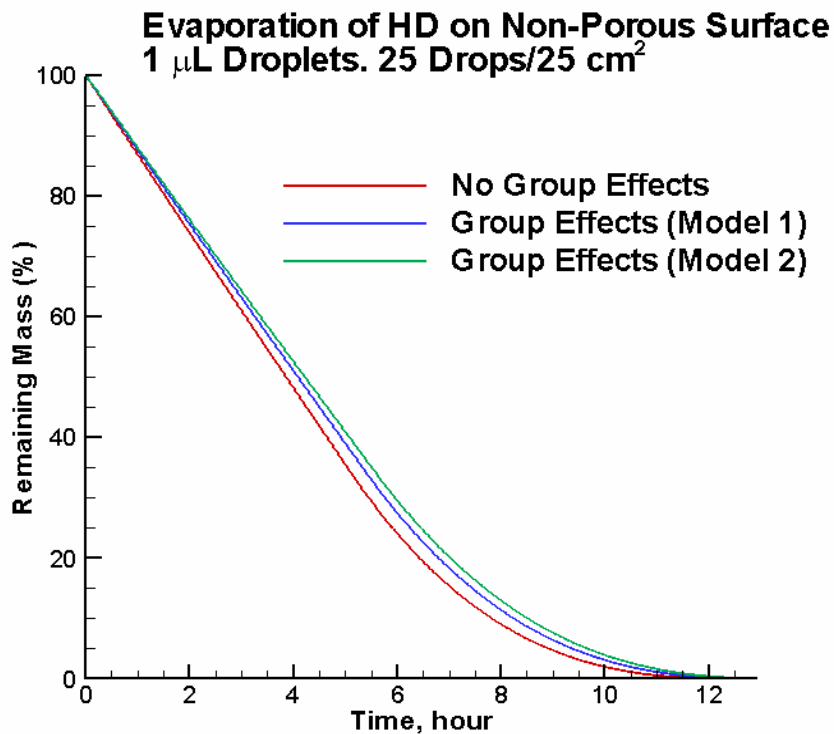




# Evaporation Module (*cont'd*)

## HD on a Non-Porous Surface – *Group Theory*

- There are two group models embedded in the code
  - Negligible for small sparse drops
  - More significant for larger and denser drops







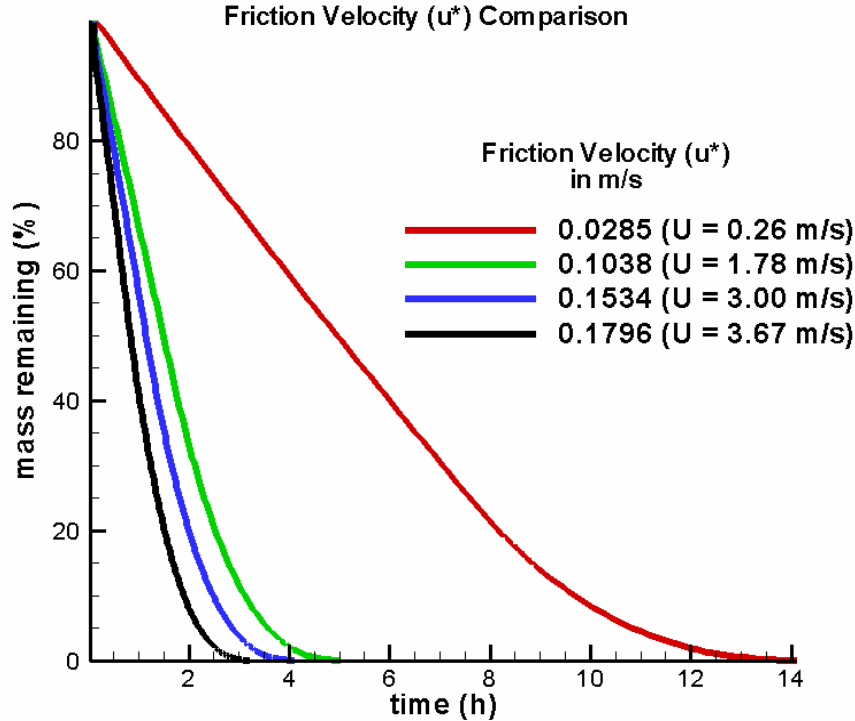
# Evaporation Module (*cont'd*)

## HD on a Non-Porous Surface – Parametric Studies

### ➤ Effect of Velocity and Air Temperature on Evaporation

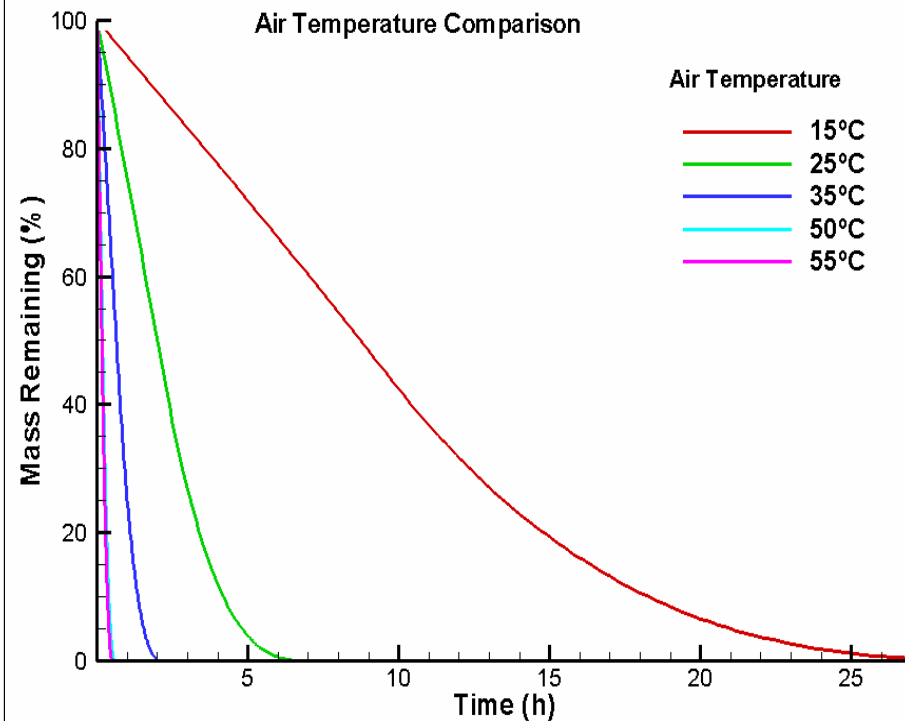
HD on Non-Porous Surface  
6  $\mu\text{L}$  drop @ 35°C, Air Temperature @ 35°C

Friction Velocity ( $u^*$ ) Comparison



HD on Non-Porous Surface  
6  $\mu\text{L}$  drop @ 17°C,  $u^*$  @ 0.1038 m/s

Air Temperature Comparison





# Evaporation Module (*cont'd*)

## Model Generalization

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- All the scenarios presented in the matrix will be connected by two methods:
  - Classical curve-fit
    - ✓ To have a simple engineering tool
  - Neural network
    - ✓ To have a more sophisticated tool with prediction capabilities





# Evaporation Module (*cont'd*)

## Model Generalization

### Caltech Work: Overview

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- Motivating hypothesis (Navaz): The relevant velocity scale for fluid evaporation rate is not the freestream speed ( $U_\infty$ ), but the “friction velocity”

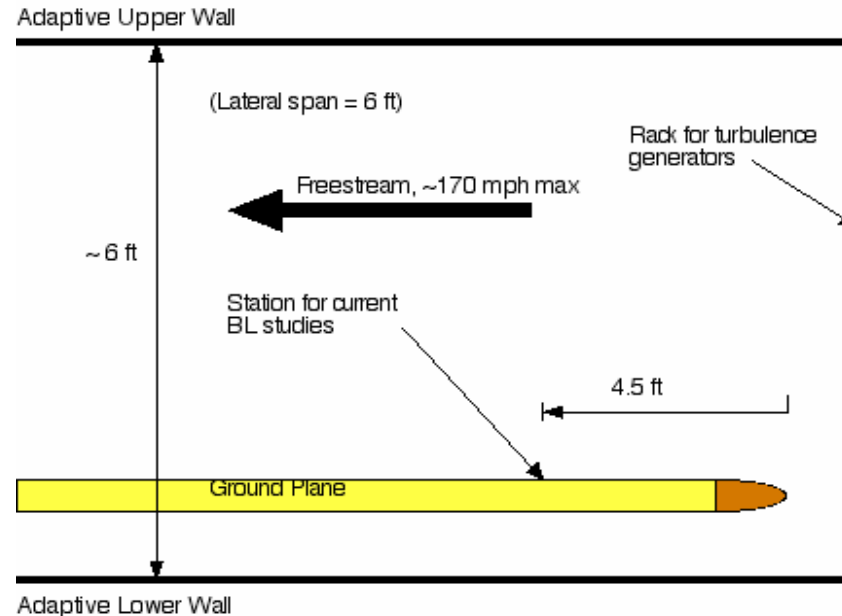
$$u_\tau = \sqrt{\frac{\tau_w}{\rho}}$$

- Variation of  $\tau_w$  (and thus friction velocity) for given free stream speed demonstrated
- Simple case of drop evaporation rate evaluated experimentally
- Variation in evaporation rate with friction velocity observed
- Future experiments



# John W. Lucas Adaptive Wall Wind Tunnel (GALCIT)

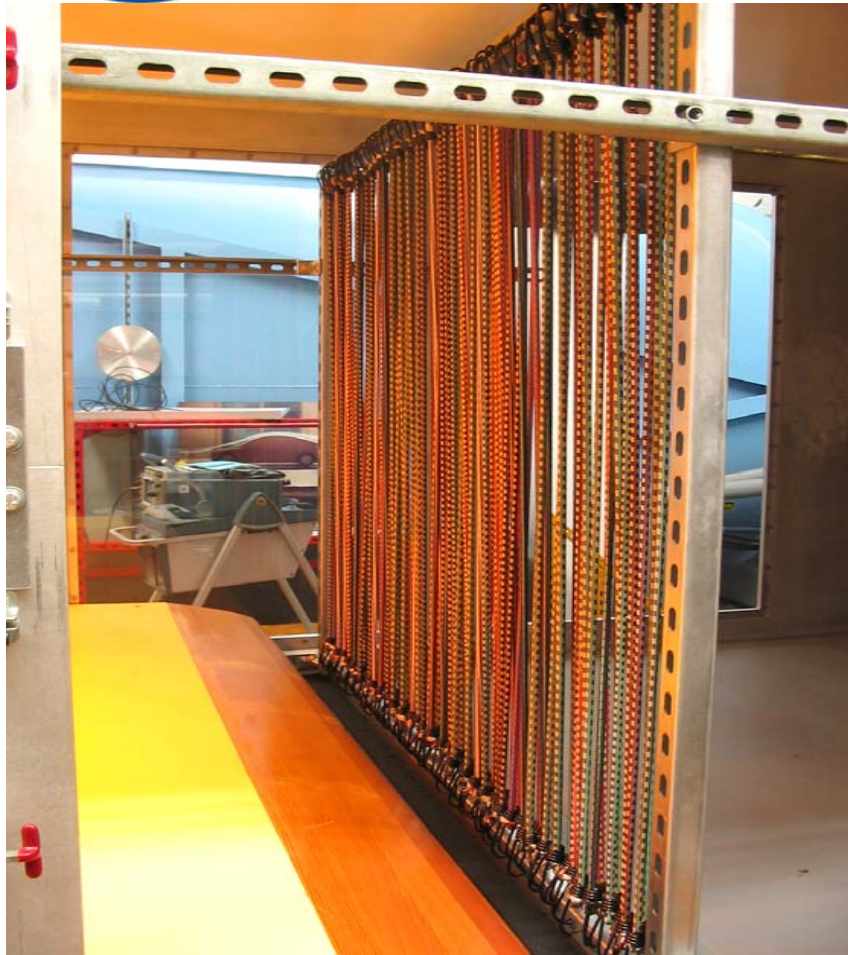
Test Section Schematic



- Turbulence generators (may be) placed in rack upstream of ground plane to increase freestream turbulence level.
- Boundary layer properties examined on ground plane at specified distance from leading edge.



# Free Stream Turbulence Generation

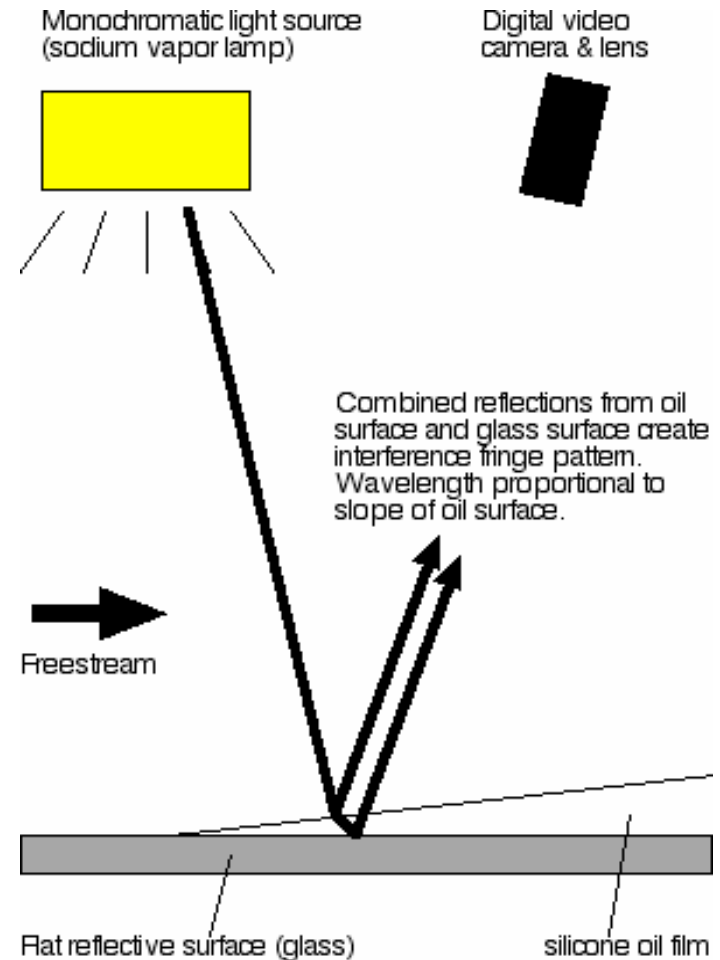


- Bungee cords stretched within frame in free stream.
- Act as turbulence generator; also vibrate quite a bit at high speeds.
- Various configurations available to "dial in" turbulence level.
- Idea: Bahram Valiferdowsi



# Wall Shear Stress Measurement

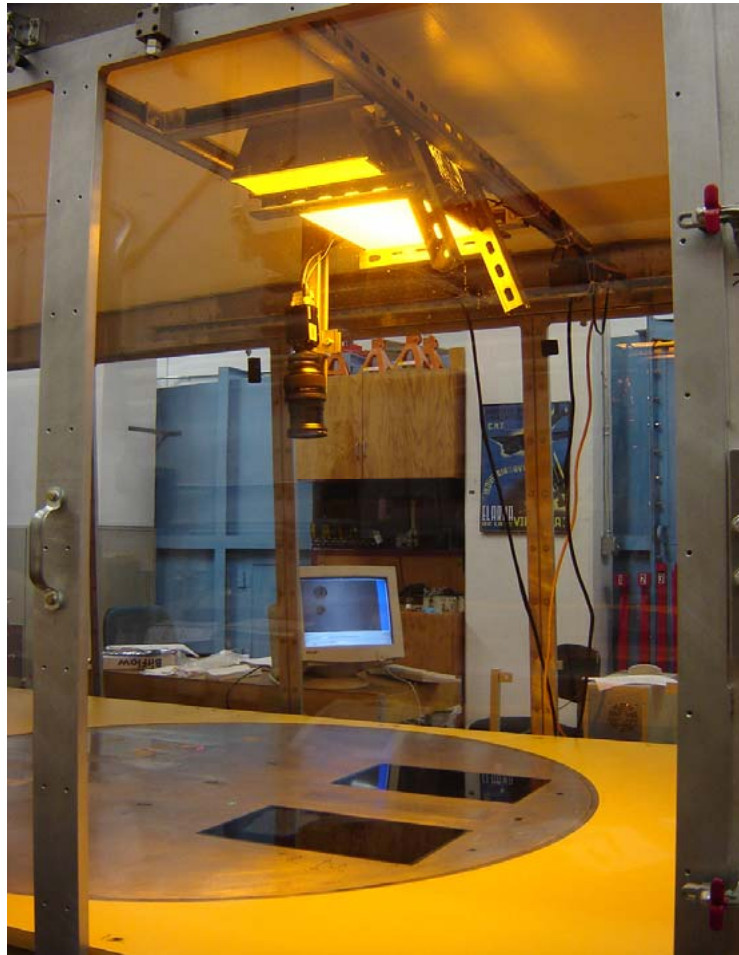
- Oil film technique used by Nagib and others.
- *Relatively* non-intrusive - camera and lamp placed in tunnel, but near test section roof.
- By observing interference fringes growing with time, wall shear stress may be calculated.





# Shear Stress Measurement Apparatus

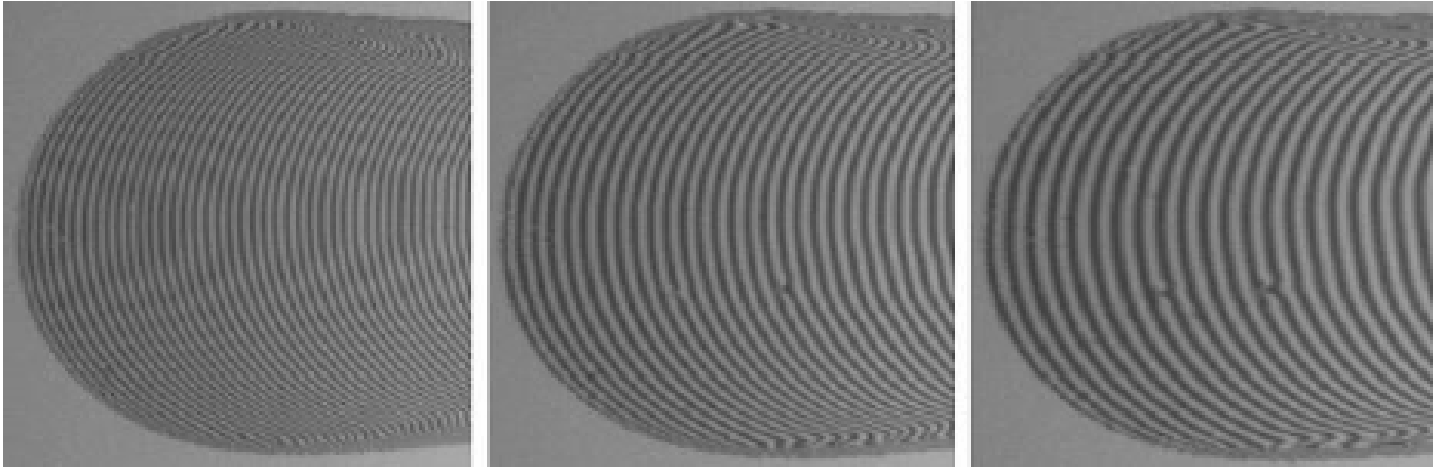
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# Wall Shear Stress Measurements

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- Numerous images taken at 10-30 sec intervals.
- Fringe spacing growth rate,  $ds/dt$ , easy to evaluate.

$$\tau_w = \frac{2n\mu}{\lambda} \frac{ds}{dt}$$

- $n$  = oil index of refraction;  $\mu$  = dynamic viscosity;  $\lambda$  = light wavelength.





# Wall Shear Stress Variation with Free Stream Turbulence

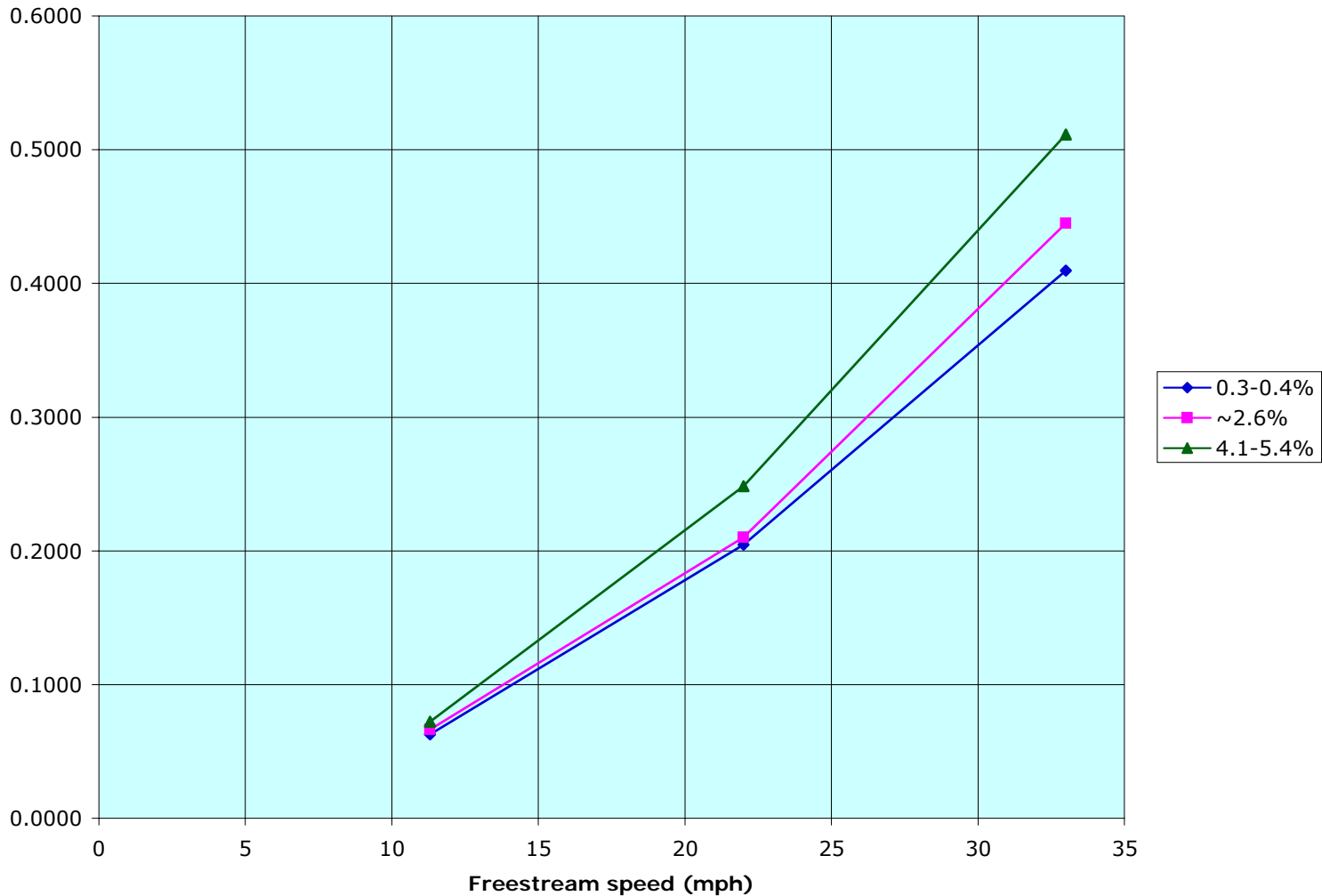
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Speed (mph)	Turbulence Level		
	0.3-0.4%	~2.6%	4.1-5.4%
11.3	0.0626	0.0663	0.0723
22	0.2048	0.2102	0.2483
33	0.4096	0.4450	0.5115

- Wall shear stress ( $\tau_w$ ) given above in Pa.
- Notable increase in  $\tau_w$  as turbulence level increases.
- Data at 1% turbulence level showed slight *decrease* in  $\tau_w$ ; calibration drift of pitot-static pressure transducer suspected.



# Free Stream Turbulence Intensity Affecting $\tau_w$ - Plot

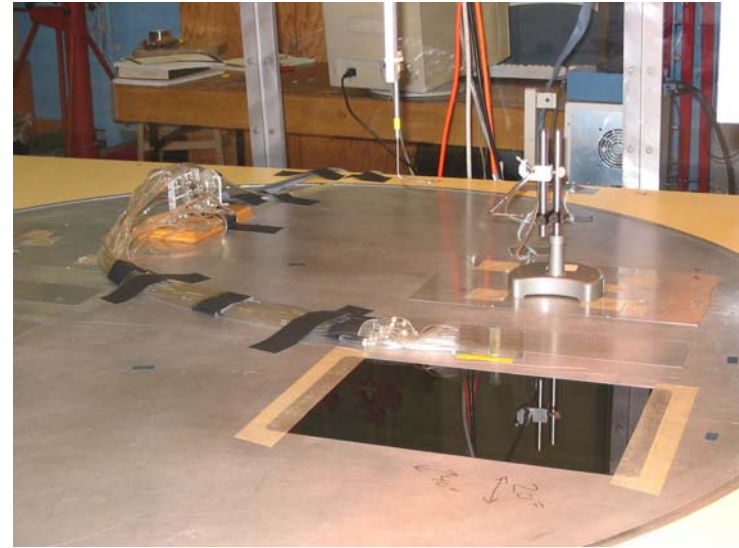
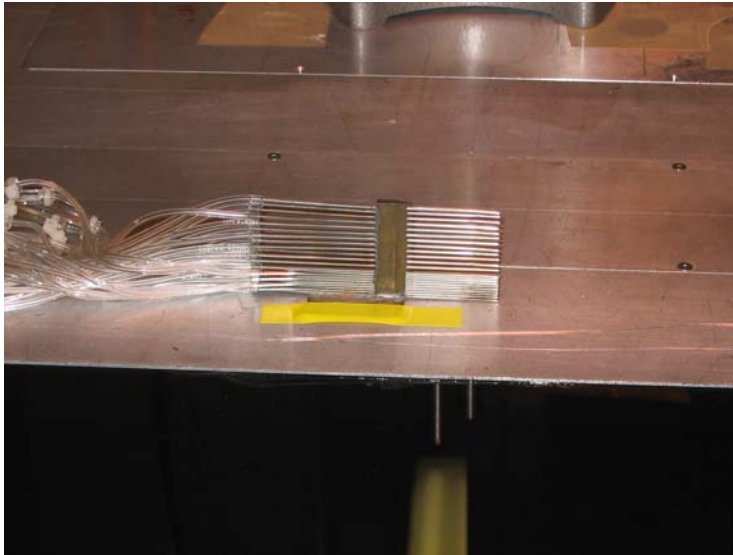






# Boundary Layer Profile Measurement

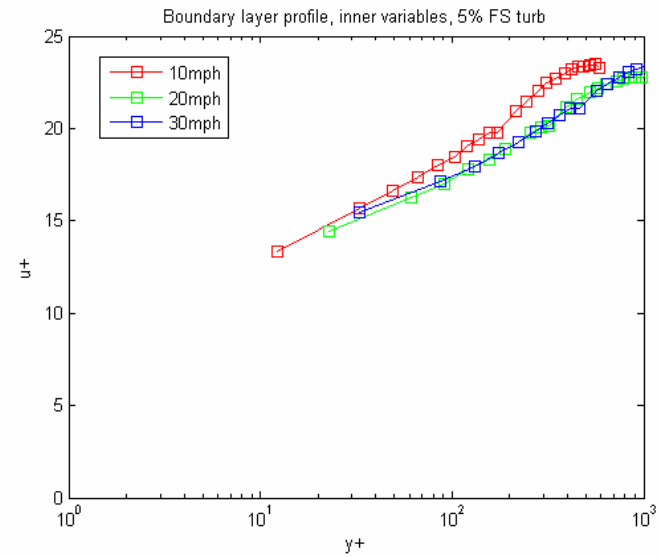
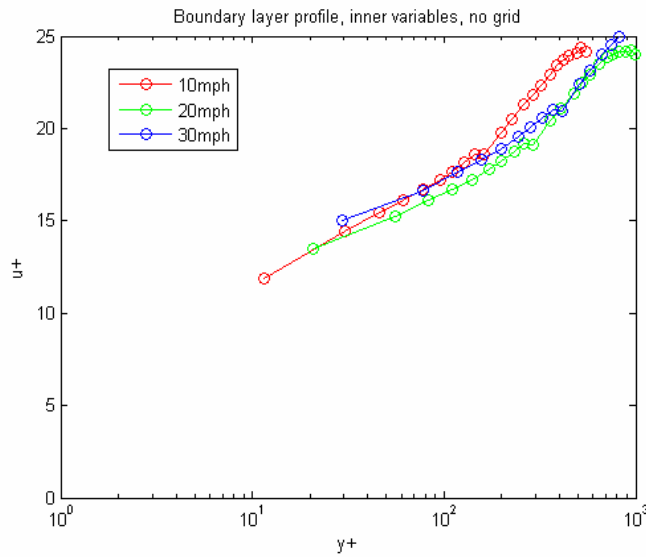
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- 22-element boundary layer rake used to measure dynamic pressures at select heights
- Static pressure taken from nearby pitot-static tube



# Boundary Layer Profile Comparison - ~0.4% vs. 5% free Stream Turbulence

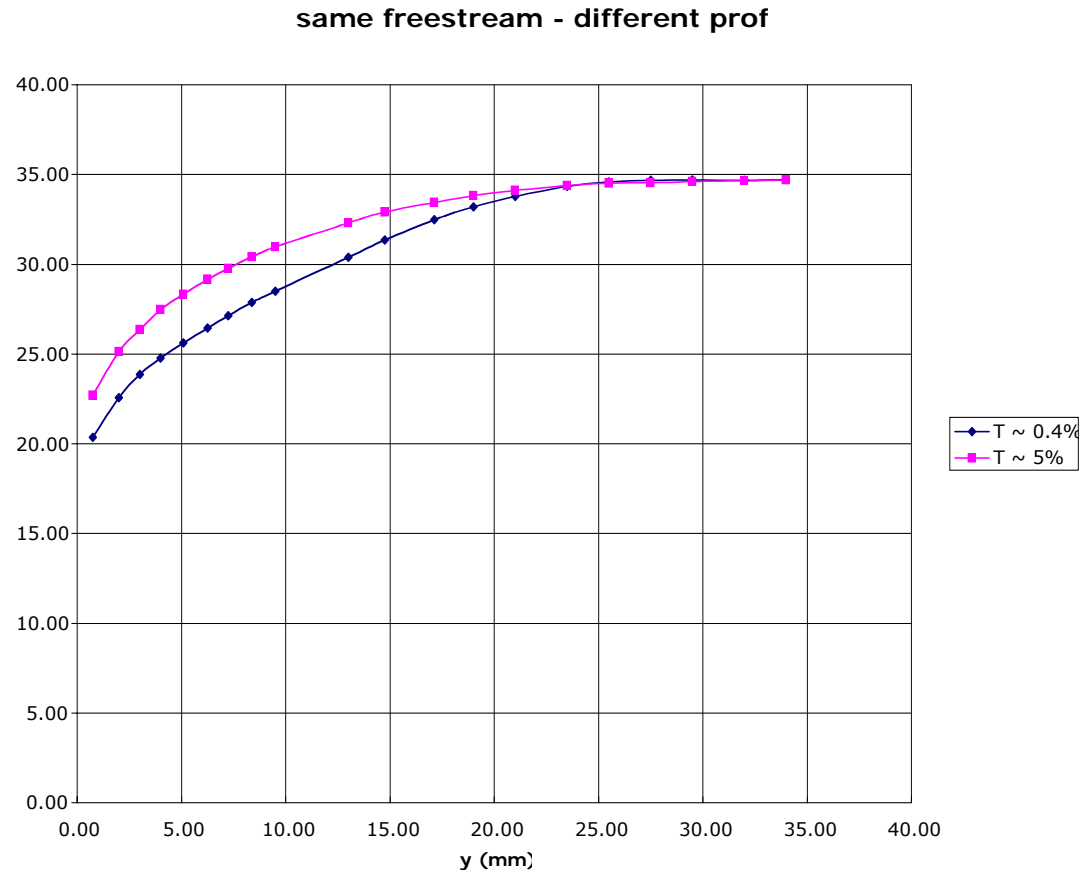


- Both profiles follow Clauser turbulent boundary layer profile; shape changes slightly near free stream transition
- In no case is laminar sub-layer accessible ( $y^+ < 5$ ).



# Profile Shape Change with Free Stream Turbulence Level

- At the same freestream speed, the shape of the boundary layer visibly varies with added freestream turbulence  $T$ .
- The higher  $T$  curve "stays high" lower, requiring a more abrupt reduction to zero.
- This agrees with the observed higher shear stress at the wall.





# Critical Parameter for Evaporation: Wall Shear?

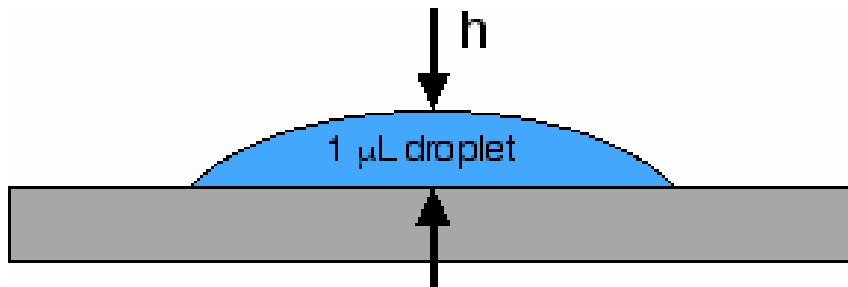
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- It is hypothesized (Navaz) that evaporation rate of liquid droplets is based on the friction velocity ( $u_\tau$ ) rather than the free stream speed ( $U_\infty$ ).
- Current experiments demonstrate that for a constant  $U_\infty$ ,  $\tau_w$  may be increased by up to 25% by imposing 5% turbulence intensity on the free stream flow.
- 25% increase in  $\tau_w$   $\rightarrow$  12% increase in  $u_\tau$ .
- Change in evaporation rate by up to 20% thus expected by model.



# Relative Sizes: 1 $\mu\text{L}$ Droplet and Laminar Sub-Layer

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- 10 mph free stream and low turbulence level, present BL experiments
- Laminar sub-layer thickness ( $y^+ = 5$ ) is  $\sim 0.3$  mm
- 1  $\mu\text{L}$  droplet has height  $h$  of  $\sim 0.2$  mm (Navaz)
- Droplet lies entirely within laminar sub-layer, where friction velocity  $u_\tau$  is the dominant flow parameter (and only velocity scale!).



# Proof-of-Concept Experiment

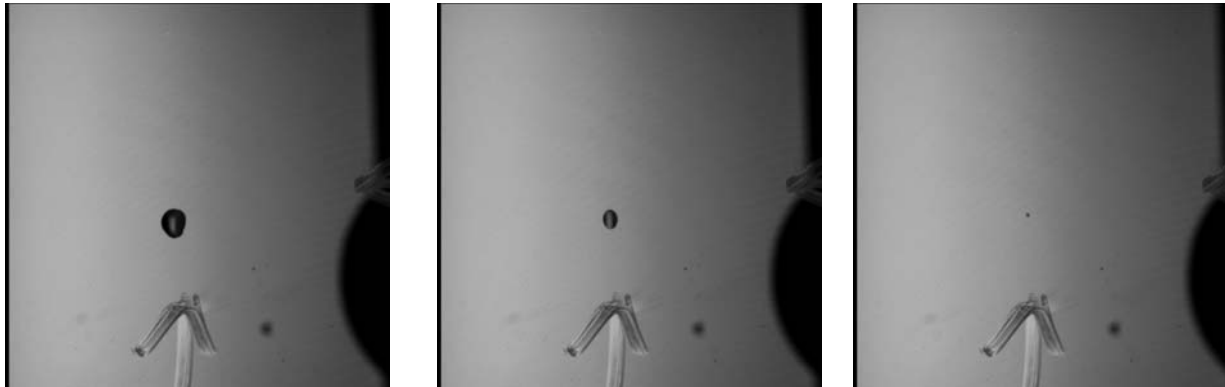
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- Evaporation rate of 2.5 ml water drop in 10 mph free stream examined at turbulence intensity levels of 0.4% and 5%.
- Droplet dispensed on glass, video camera observes evaporation.
- Ensembles for each case taken, mean evaporation time recorded.



# Droplet Evaporation Experiment

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Turbulence intensity level (%)	0.4	5
Friction velocity (m/s)	0.23	0.25
Mean drop evaporation time (sec)	<b>900</b>	<b>850</b>



# Upcoming Work at Caltech

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- Evaporation rate measurement
  - Instantaneous rate measurement
  - More accurate optical techniques
  - Mass measurement (microbalance?)
- Still higher turbulence intensity levels
- Further collaboration/verification with numerical model of H. Navaz
- Different surfaces (concrete, etc.)

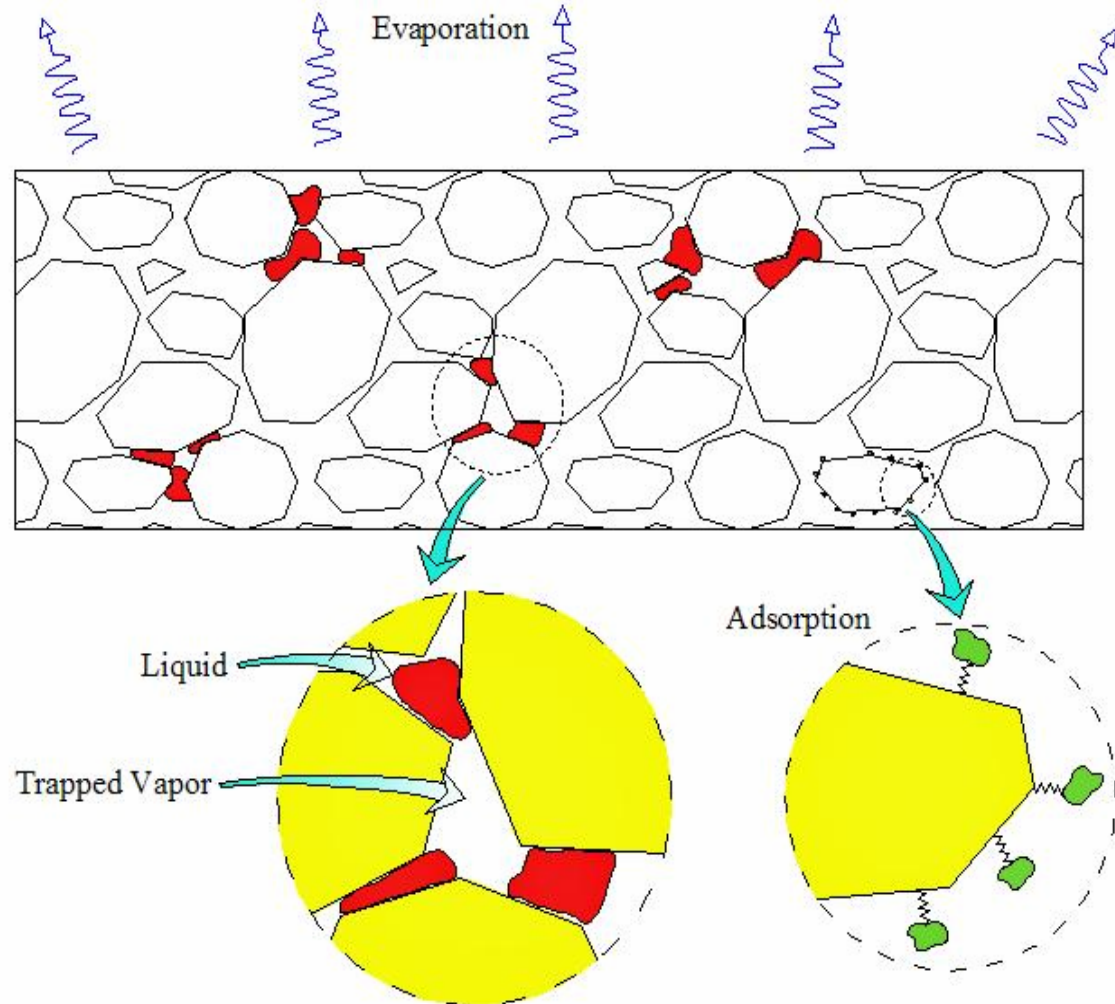




# Evaporation Module

## Link to the Porous Surface

- ▶ Simultaneous process present with evaporation
  - Capillary diffusion
  - Secondary evaporation
  - Vapor entrapment
  - Adsorption





# Porous Media/Substrate Modeling Observations

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- Liquid simulants established a finite network in a porous domain (Czech concrete)





# Porous Media/Substrate Modeling Proposed Approach

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- Modeling effort
  - Solve the governing equation by capillary network model (CNM)
- Verification effort
- Generating the Design of Experiment matrix
- Obtaining solution for the entire matrix
- Curve fitting
  - Classical
  - Neural Network



# Porous Media/Substrate Modeling

## Adding Adsorption Model

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- Add adsorption model to the porous substrate model
- Ensure robustness of the algorithm
- Validate model by
  - Conducting laboratory tests
- Verify the model
  - Laboratory
  - Outdoor



# Conclusion

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- Developed an evaporation model
- Verified the model with experimental data
- Extended the domain of applicability by using a hybrid analytical/experimental method
- Developed a framework for tackling a more complex problem – HD on porous substrate
- Resolving wind/turbulence/shear stress issues
- Incorporating the effects of wind turbulence intensity on evaporation





# Evaporation Rate Validation

**Evaporation of HD on Glass. 25 Drops/25 cm<sup>2</sup>  
Each Drop = 1  $\mu$ L - Wind Velocity = 5.8 ft/s**

