

Increased Bed Erosion Due to Ice

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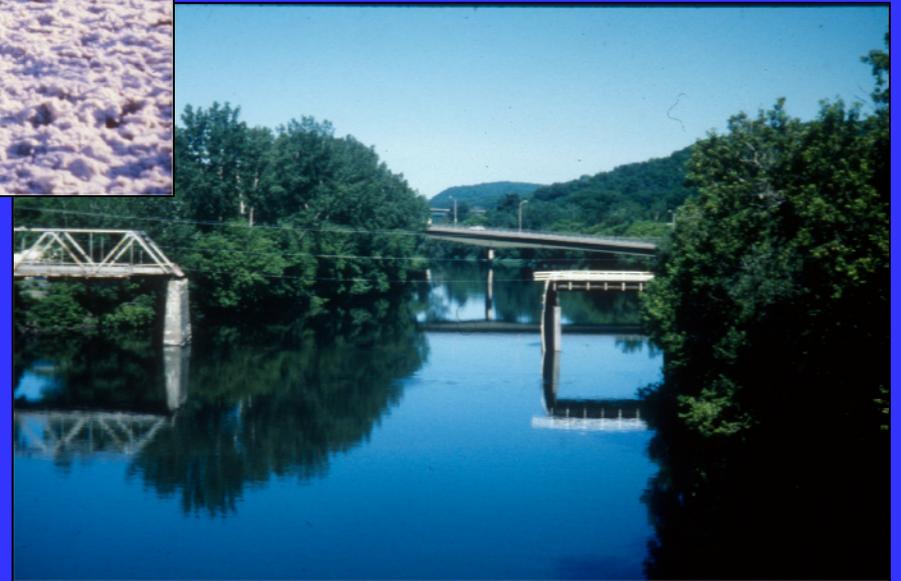
Bridge Street Bridge Late 60's



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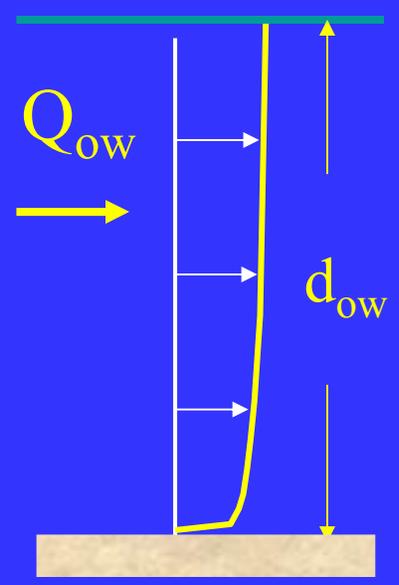
What Happened?



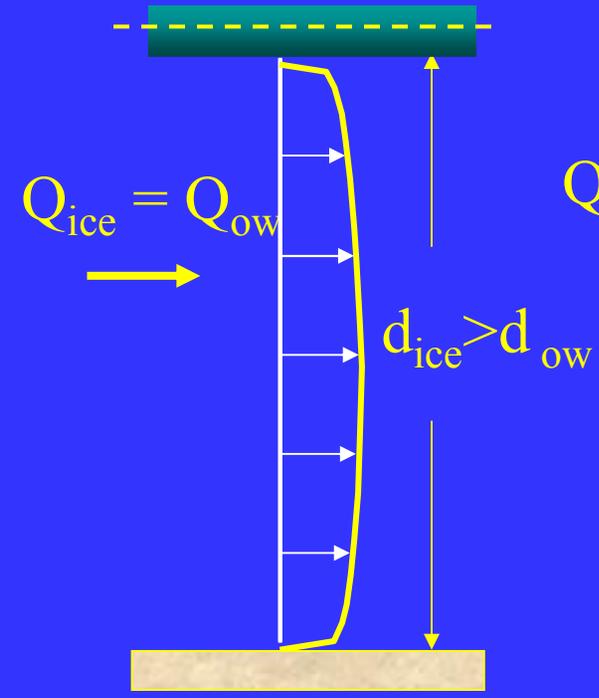
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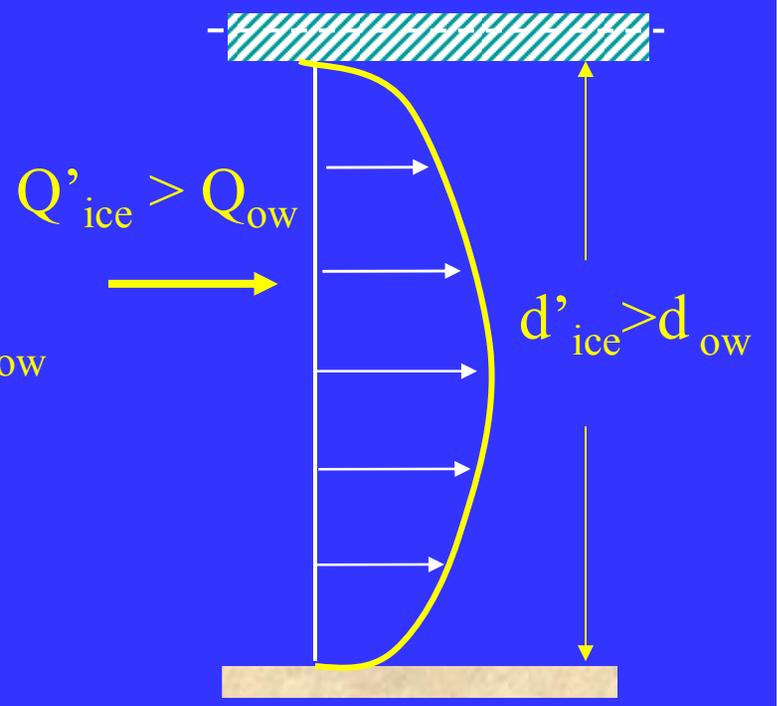
Open Water



Stationary-Floating Cover

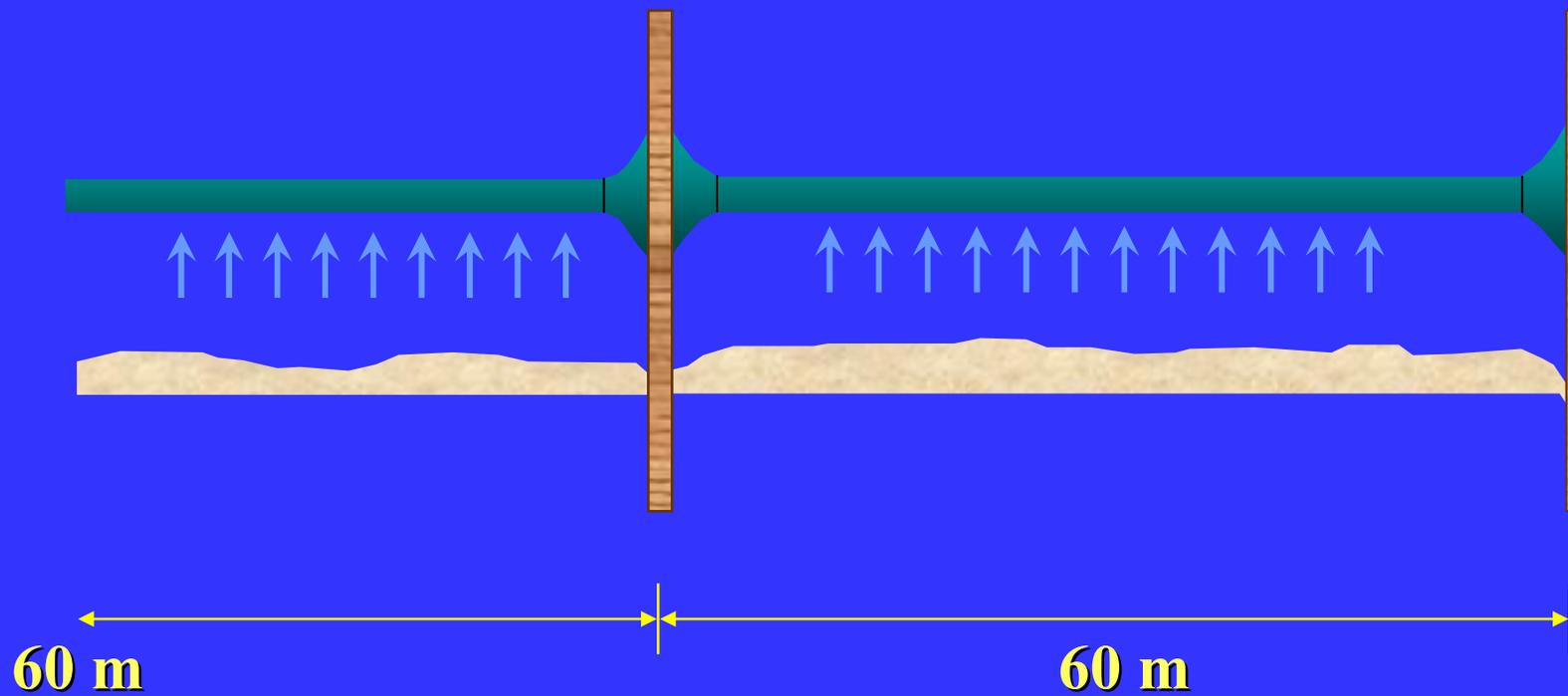


Fixed Cover



Ice Cover Effects on Narrow Rivers

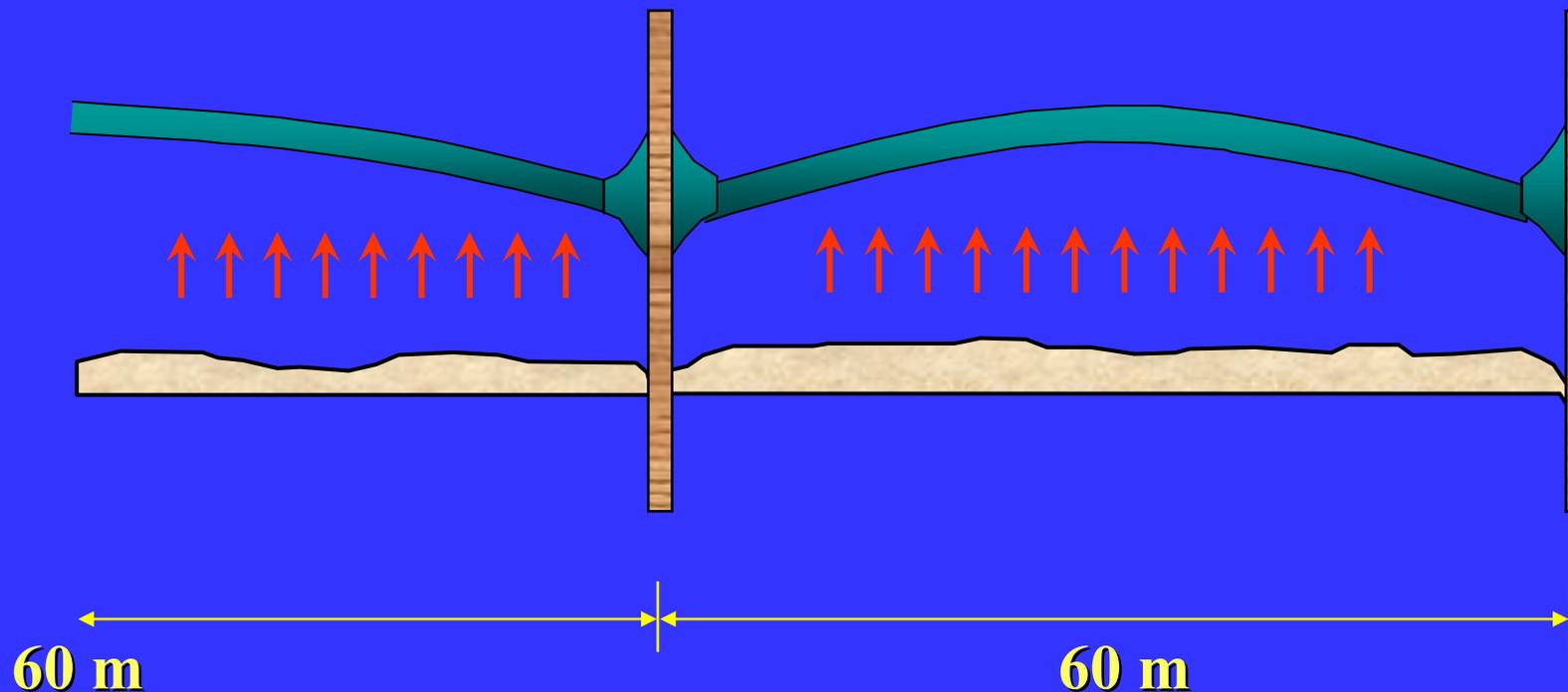
Initial Water Level



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Ice Cover Effects on Narrow Rivers Rising Water Level



Characteristic length (l) for 50 cm ice thickness (h)

Approximated by $16h^{3/4}$, $l = 9.5$ m

Radius of Influence ($5 \cdot l$) is \gg Half the Span



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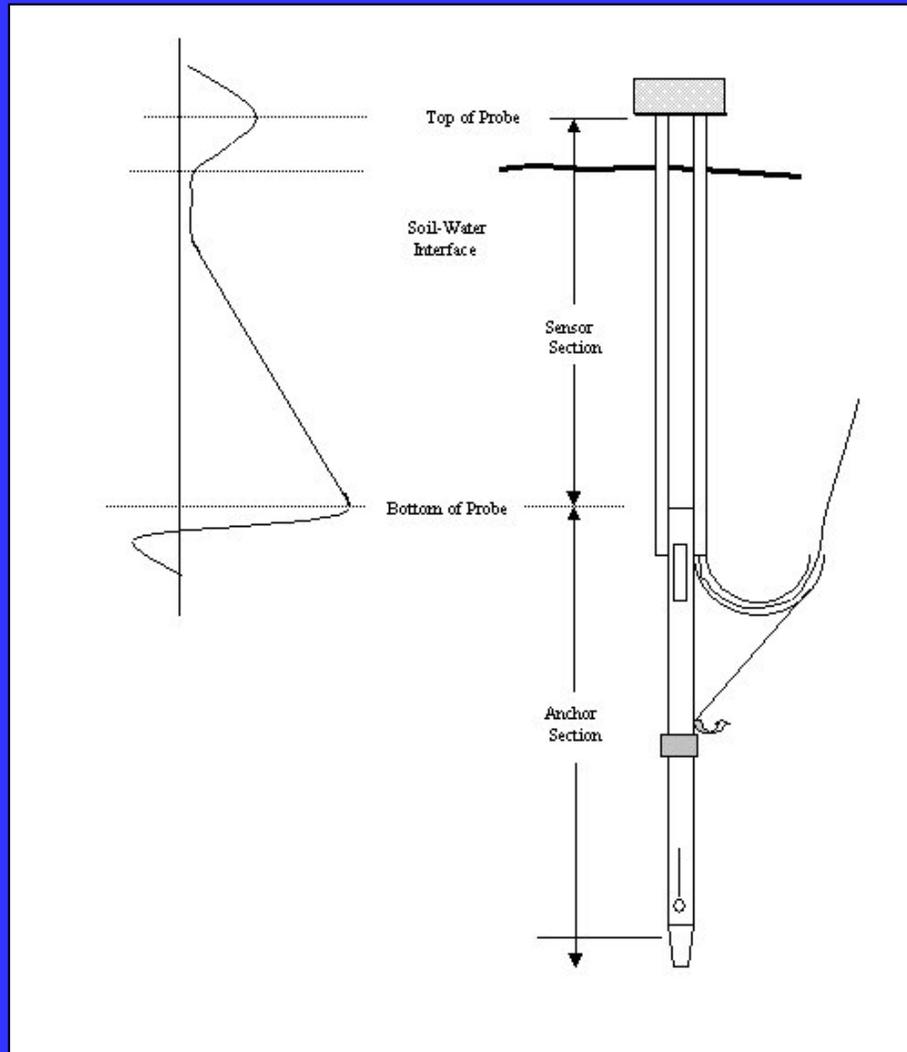


General Background

- Field Measurements
 - Scour probes using Time-Domain Reflectometry-independent of surface conditions
 - Stage must increase 2-4 times the ice thickness before break-up
 - Ice cover does not immediately respond to changes in stage
 - Increases above the freeze-up discharge but below the break-up threshold → increases in mean velocity



TDR Scour Probes



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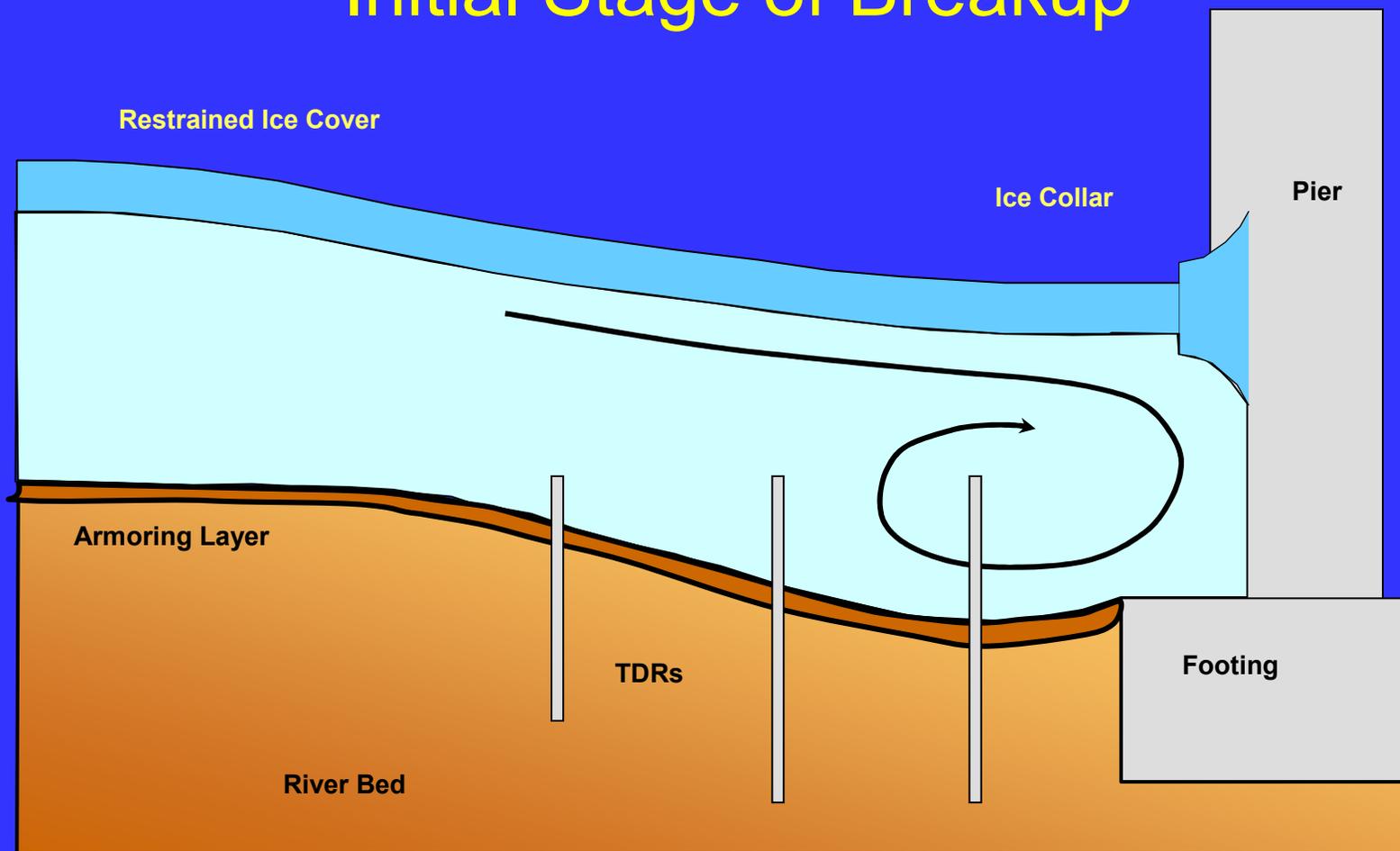
Ice Cover Rt. 5 Bridge



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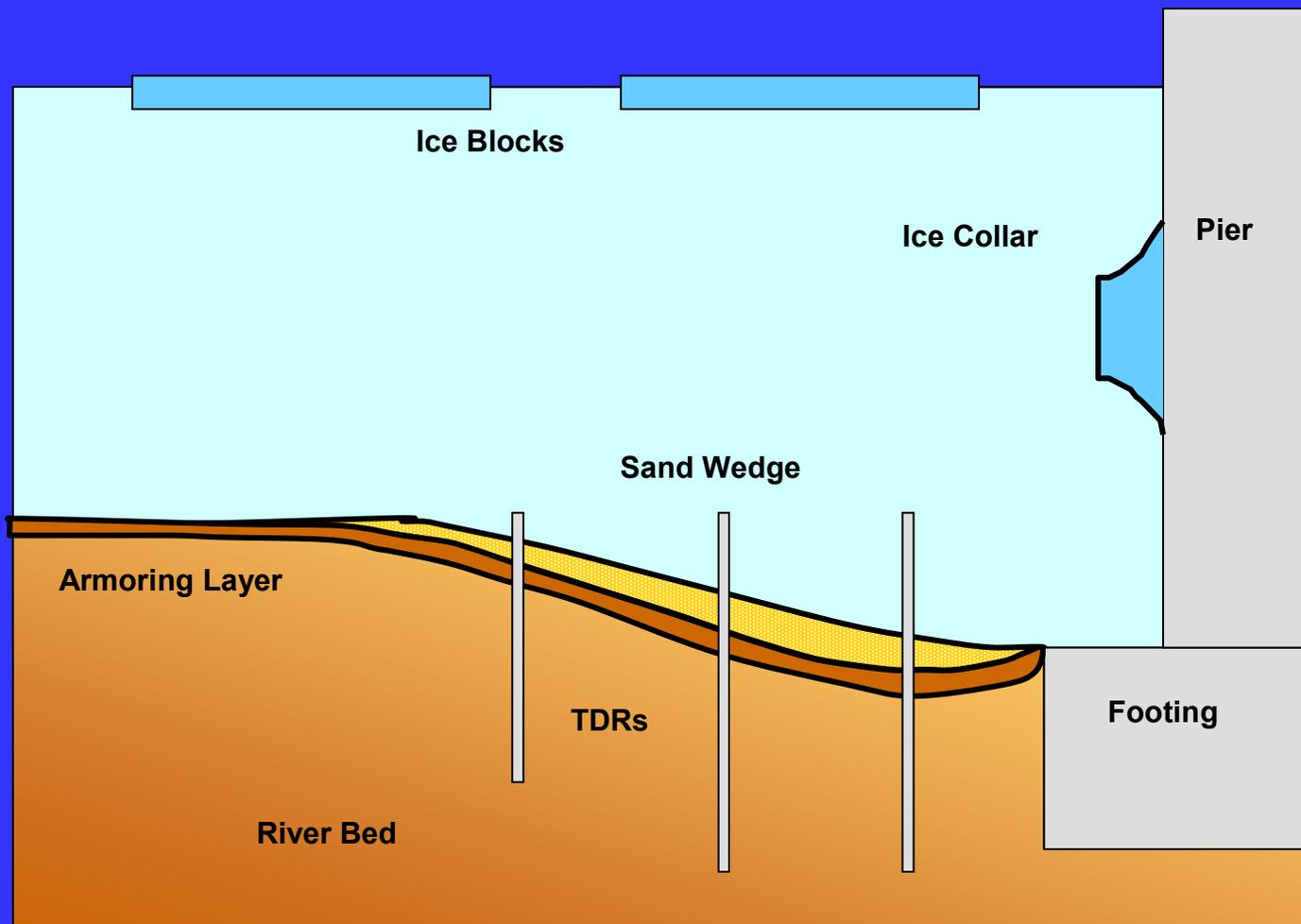
Scour Under an Ice Cover Initial Stage of Breakup



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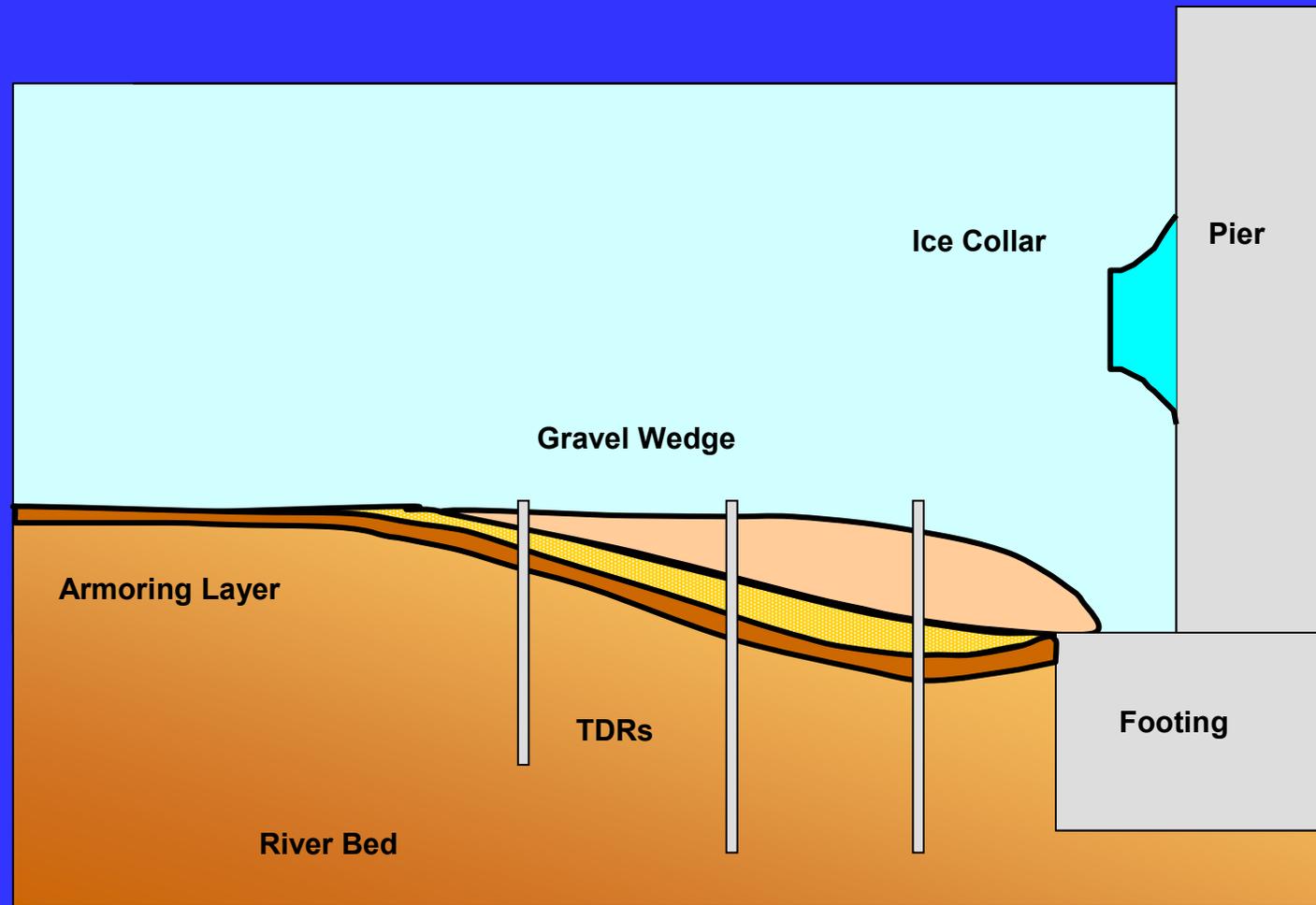
Scour Under an Ice Cover Immediately Following Breakup



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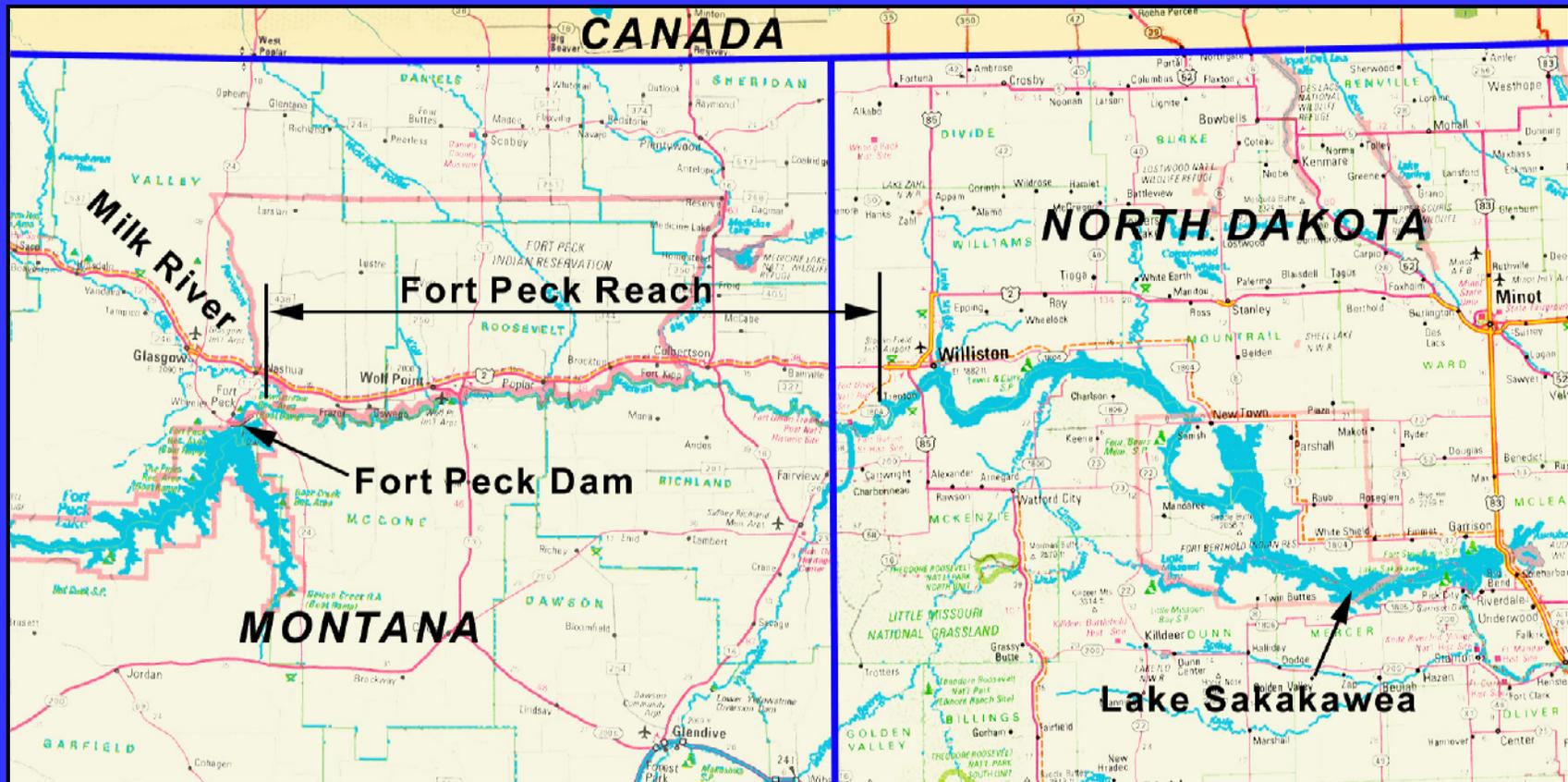
Scour Under an Ice Cover High Water Following Breakup



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Fort Peck Reach of Missouri River



Five sites with periodic and continuous monitoring along the 170 mile reach



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Culbertson, Montana

October

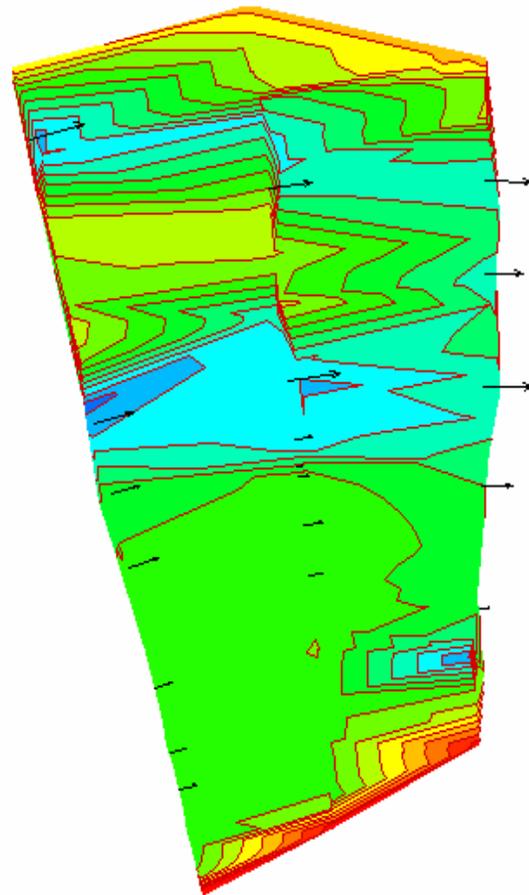


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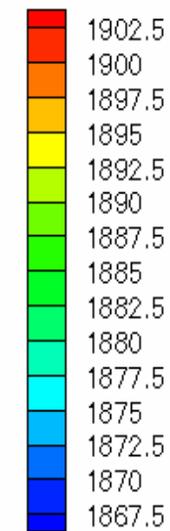
Culbertson, Montana

Culbertson Site
RM 1620
October 1988



Reference Velocity
Vector 2-ft/sec
→

Elevation (ft)



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Culbertson, Montana

January

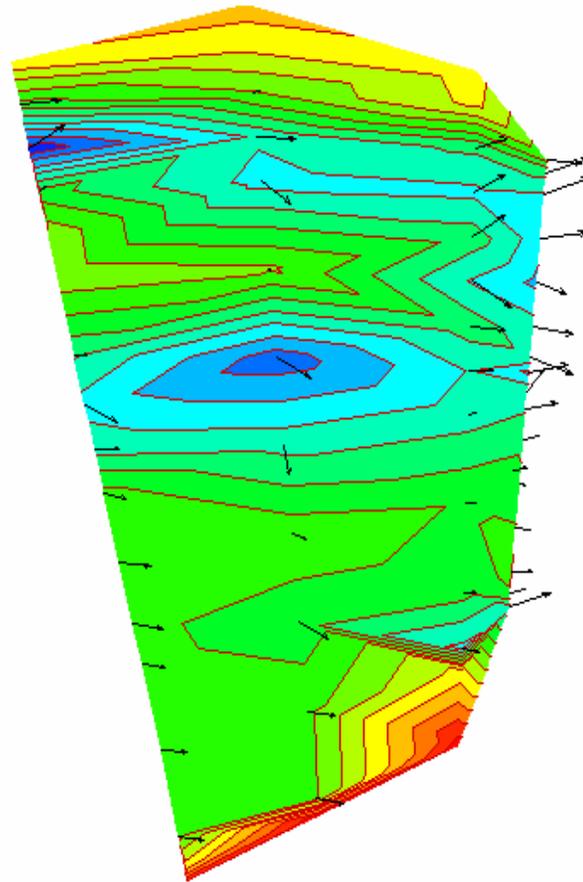


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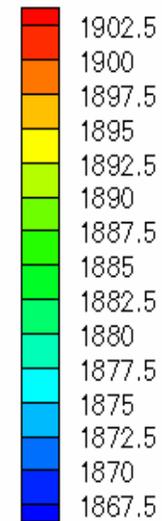
Culbertson, Montana

Culbertson Site
RM 1620
January 1999



Reference Velocity
Vector 2-ft/sec
→

Elevation (ft)



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Culbertson, Montana

February

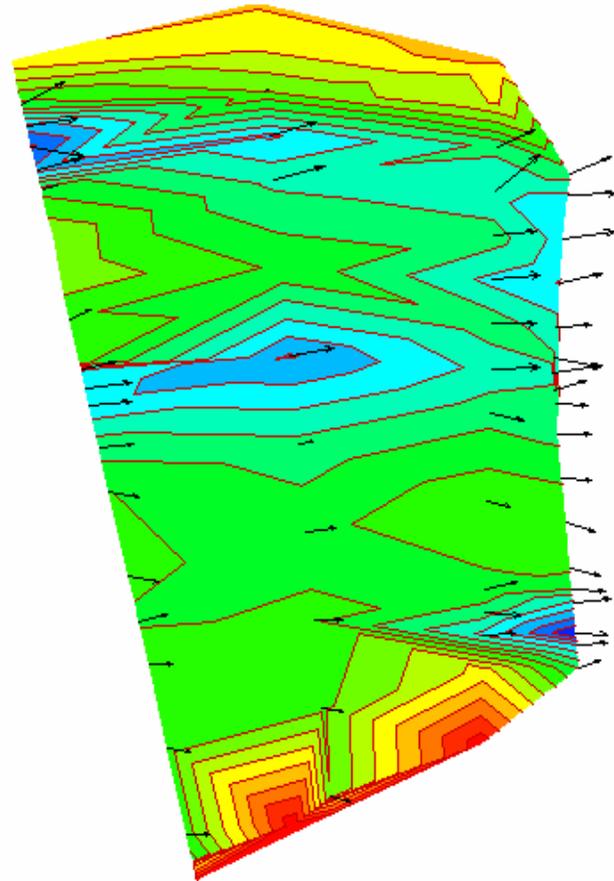


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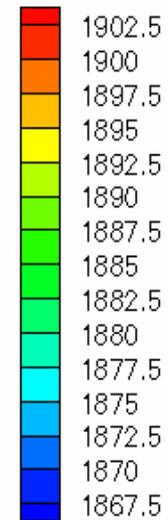
Culbertson, Montana

Culbertson Site
RM 1620
February 1999



Reference Velocity
Vector 2-ft/sec

Elevation (ft)



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Culbertson, Montana

March



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Culbertson, Montana

April

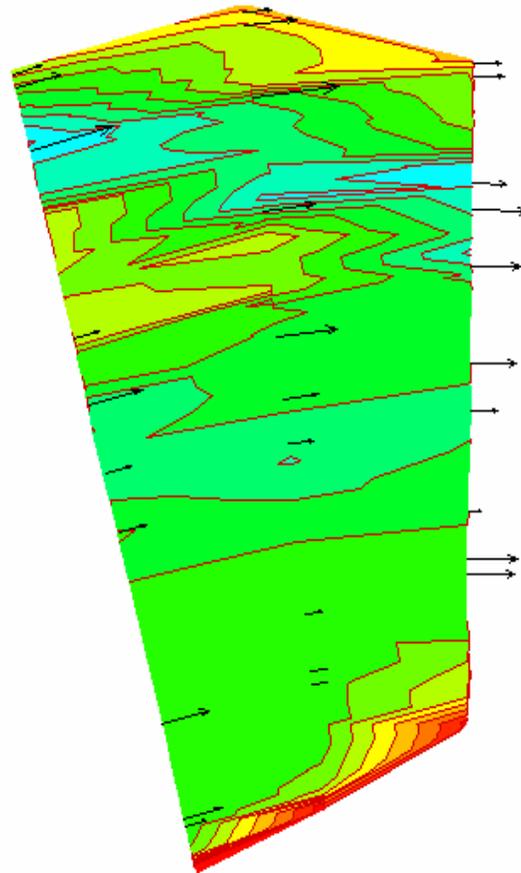


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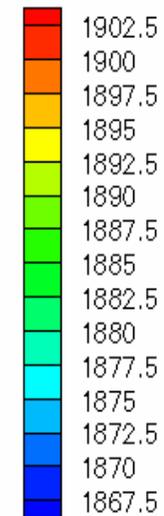
Culbertson, Montana

Culbertson Site
RM 1620
April 1999



Reference Velocity
Vector 2-ft/sec

Elevation (ft)



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Milltown Dam located 120 miles downstream of historic Butte and Anaconda copper mining operations.



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Testing Parameters

- Clear Water Scour
- Cylindrical Pier
- Smooth & Rough Cover
- One type of Uniform Sediment
($d_{50} = 0.13$ mm)
- Two Pressure Conditions
 - 3” of head
 - 6” of head



Effect of Flow Intensity: V/V_c

- Clear-water Scour- no sediment transport on the bed

$$V_c > V \geq 0.5 V_c$$

- Live-bed Scour- sediment transport on the bed

$$V \geq V_c$$

- For the sediment in this study, $V_c = 0.9$ fps





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Test Conditions

Number of Tests	Cover Condition	Relative Cover Roughness
6	Open Water/Free Surface	N/A
5	Floating	Smooth
1	Floating	Rough
6	Fixed	Smooth
2	Fixed	Rough





Smooth Cover



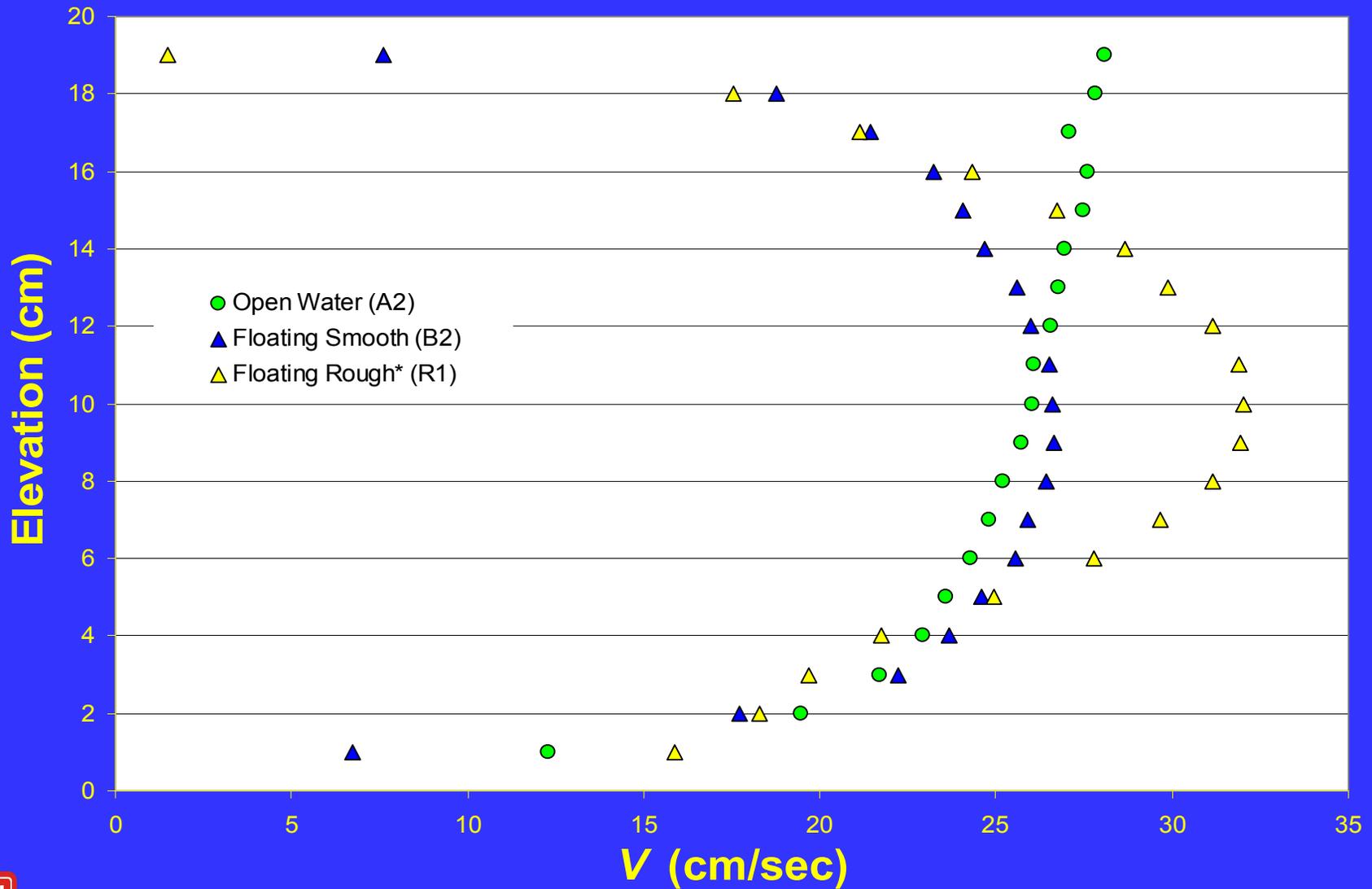
Rough Cover



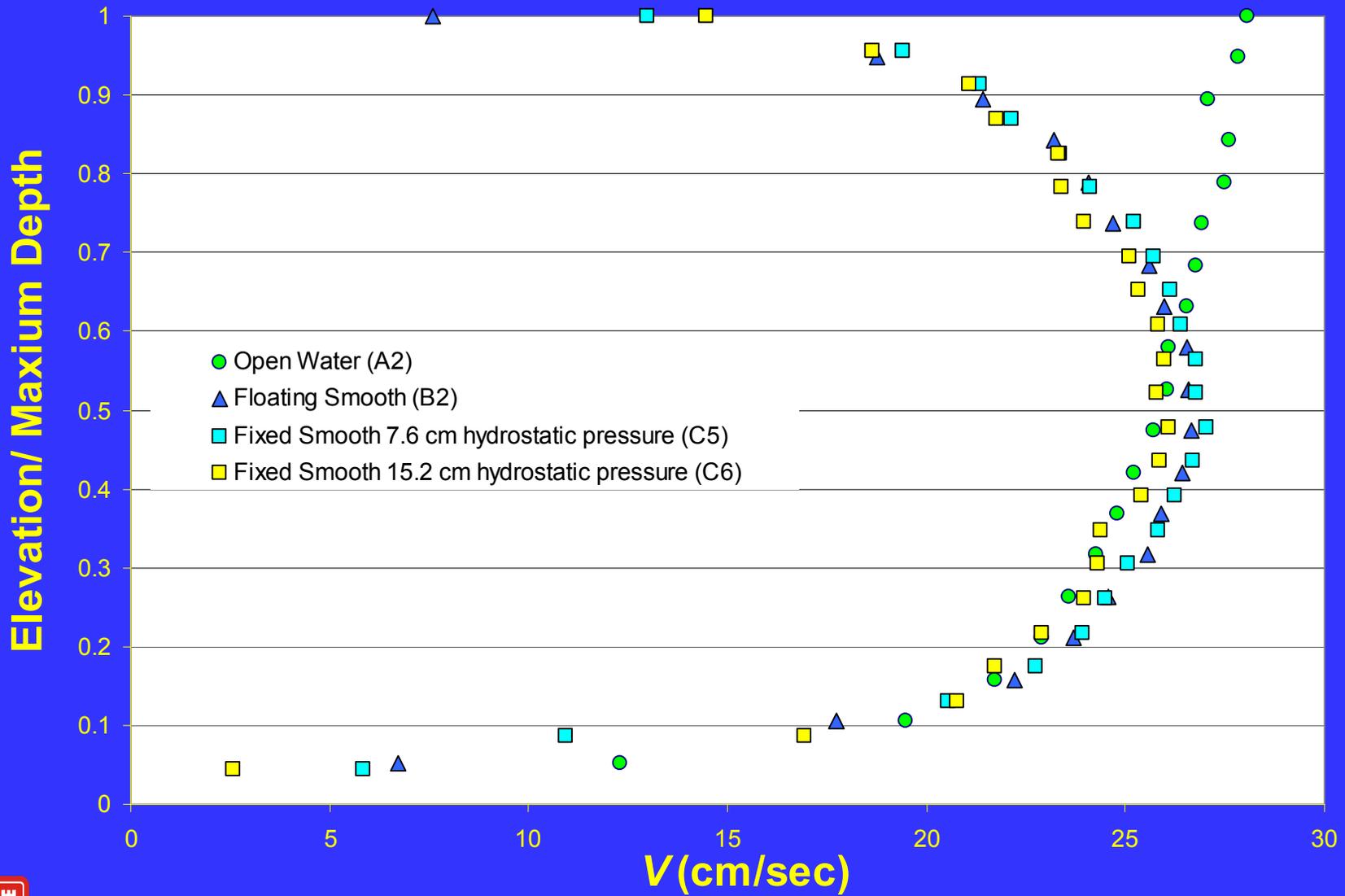
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Velocity 1.96 cm/s, $V_{avg}/V_c = 0.8589$



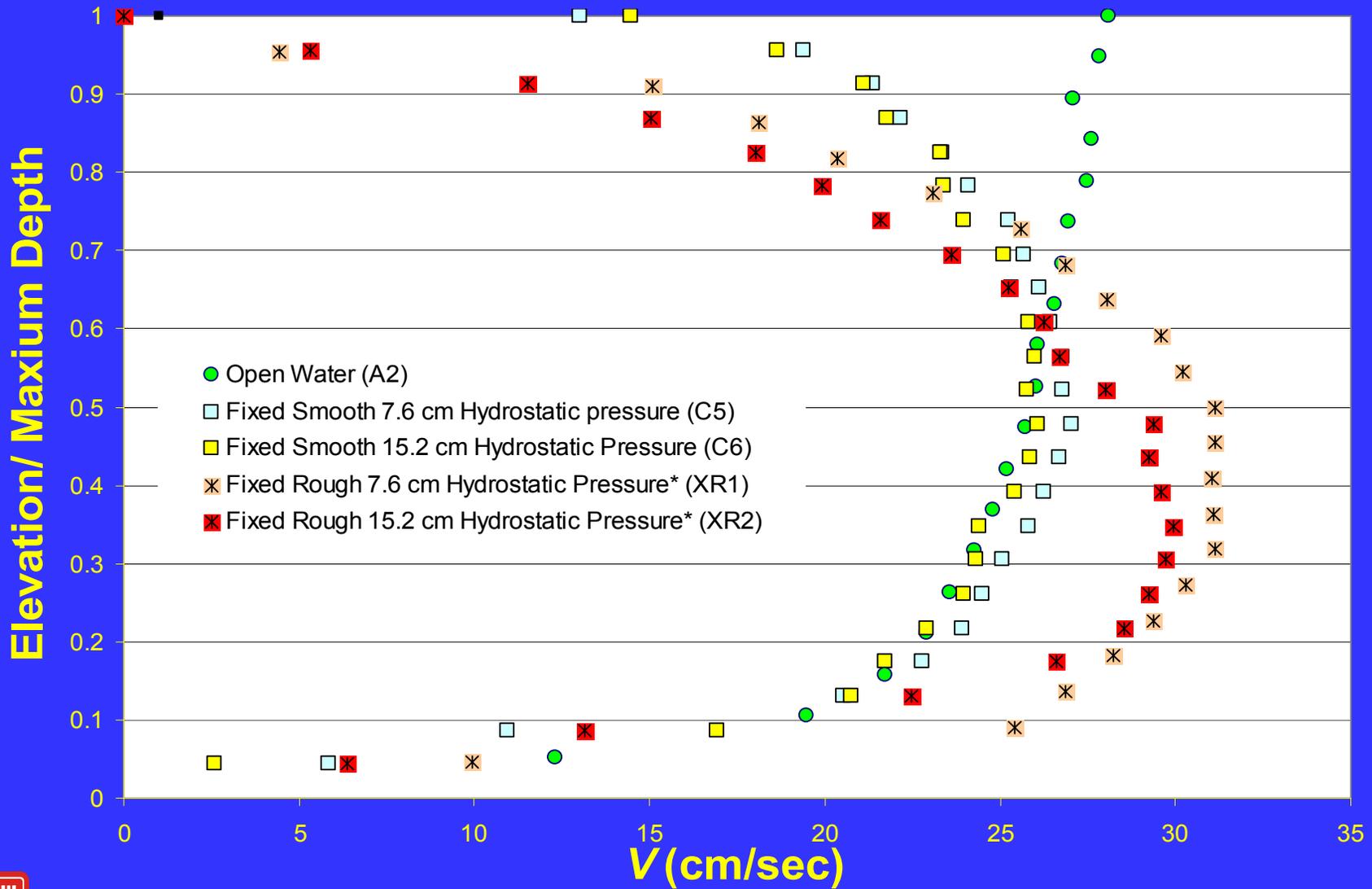
Velocity 1.96 cm/s, $V_{avg}/V_c = 0.8589$



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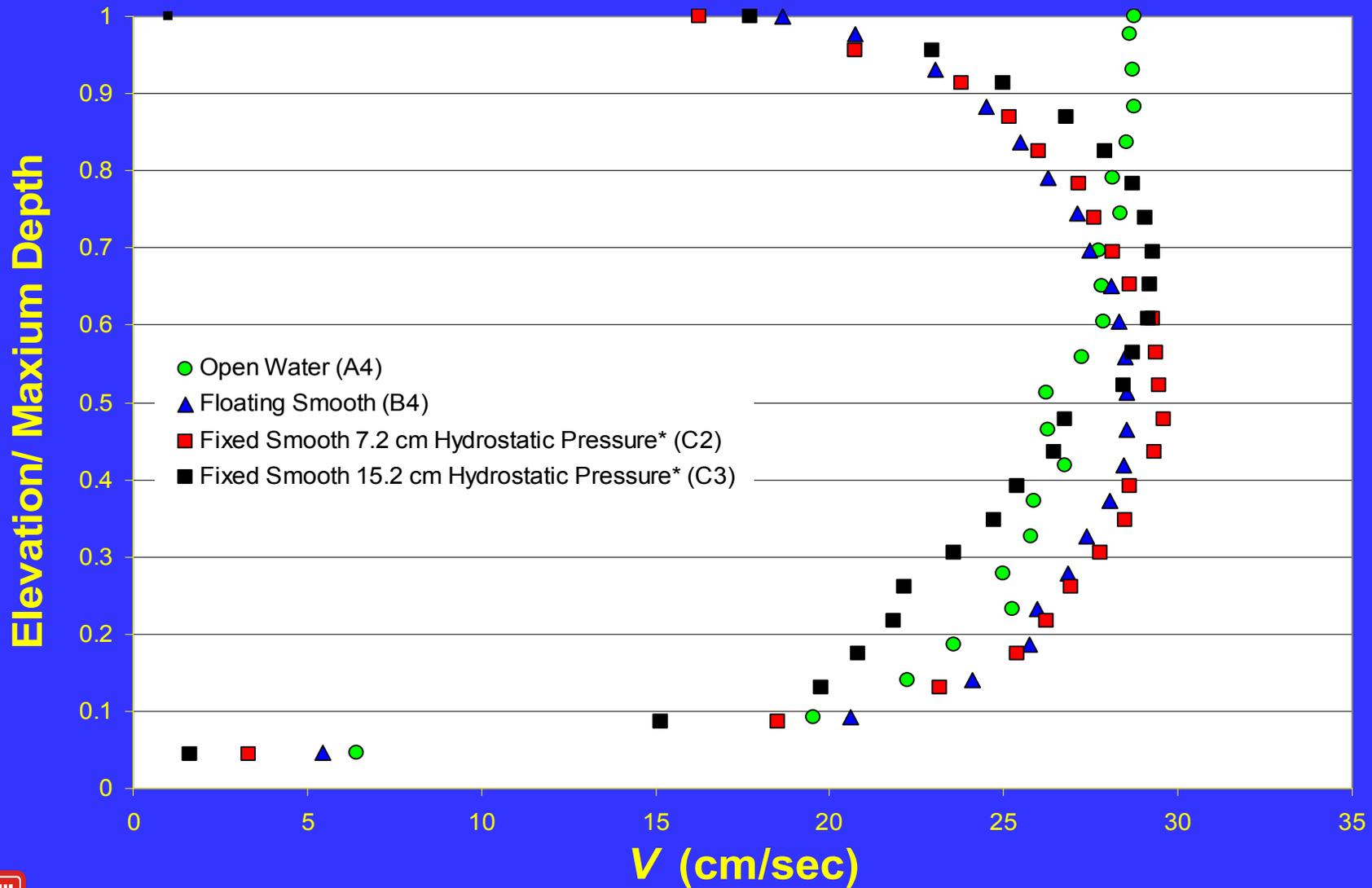
Velocity 1.96 cm/s, $V_{avg}/V_c = 0.8589$



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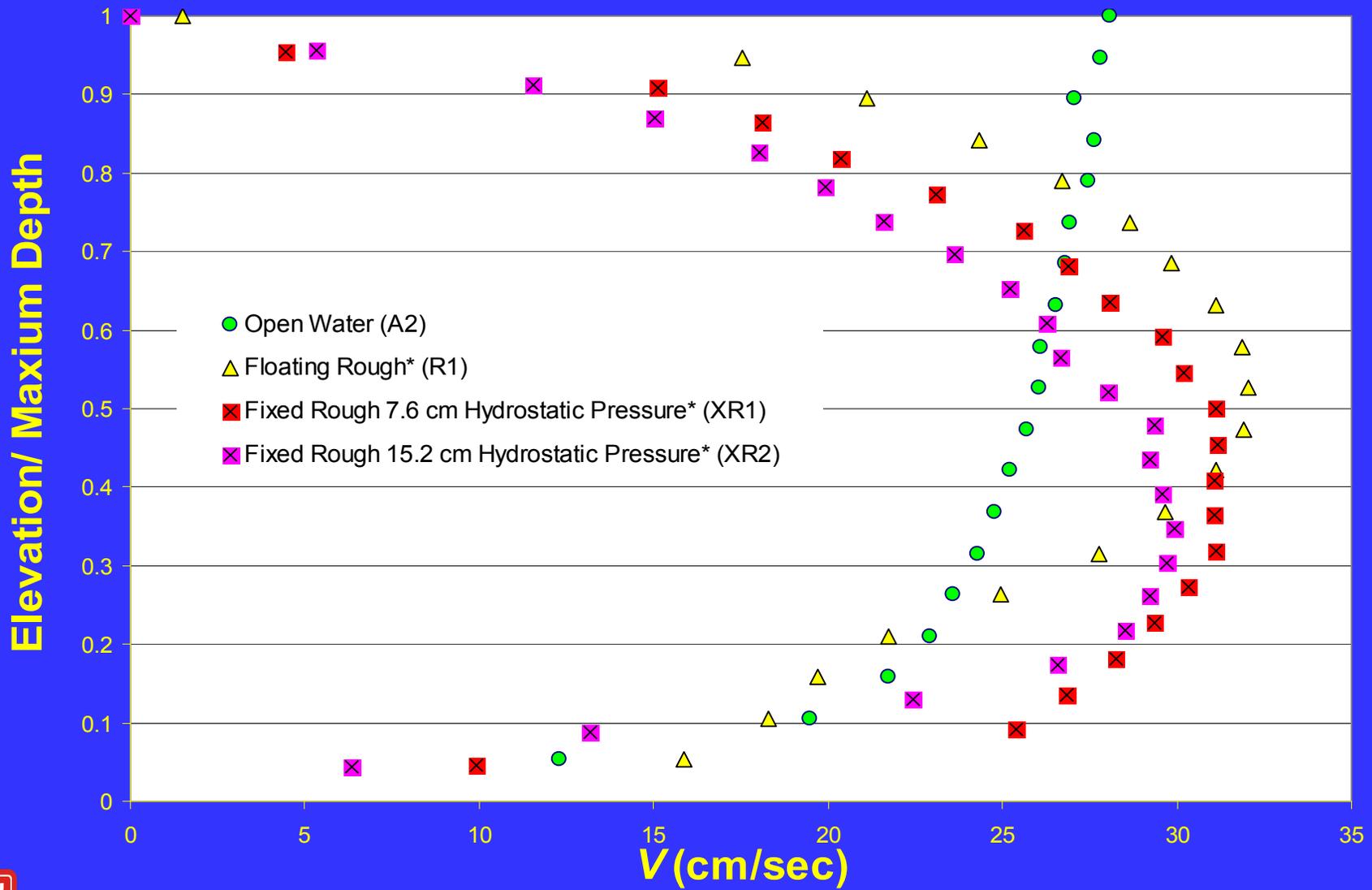
Velocity 2.12 cm/s, $V_{avg}/V_c = 0.9278$



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Velocity 1.96 cm/s, $V_{avg}/V_c = 0.8589$



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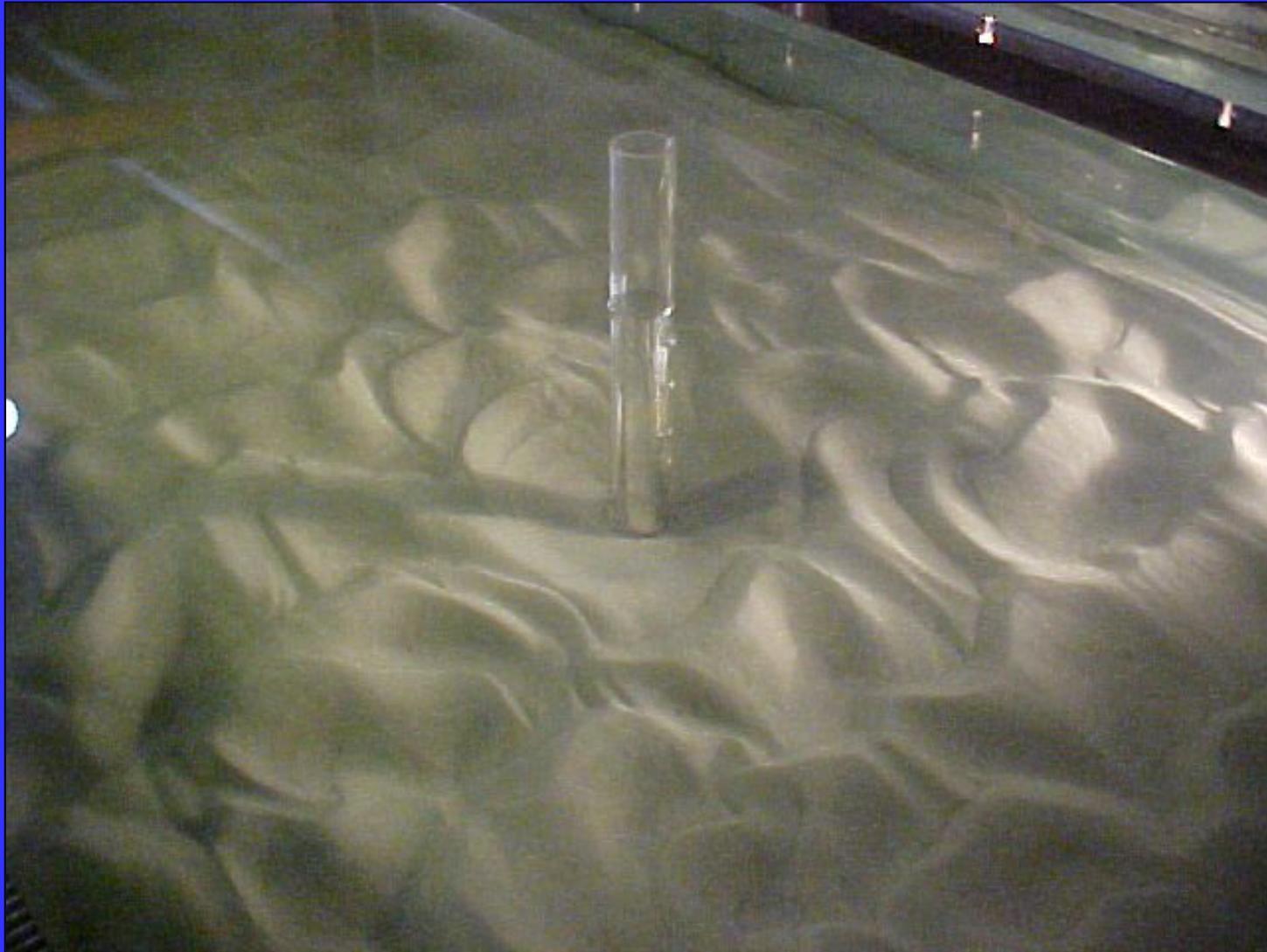
Sample Scour Hole- Test C5



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Sample Scour Hole- Test XR2



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Conclusions

Ice Effects on Bed Erosion

- Ice cover can be a major factor in sediment transport and stability of contaminated sediment.
- Pressurized flow due to ice significantly increases mean velocity and the scour potential.
- Ice cover roughness increases turbulence, distorts the vertical velocity profile and increases bed shear.
- Existing theory and models do not adequately explain these field observations and flume experiments.





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Summary Results Grouped by V_{avg}

Test	Avg V [fps]	Ya [in]	Duration [h:mm]	Scour Depth [in]	Scour Depth [cm]	Notes
0.650 fps; $V_{avg}/V_c = 0.7222$						
A5	0.650	9	16:12	2.6875	6.826	
B3	0.650	9	18:10	2.7500	6.985	
0.700 fps; $V_{avg}/V_c = 0.7777$						
A6	0.700	8.5	13:13	2.8750	7.303	
B5	0.700	8.5	15:29	3.2500	8.255	
0.735 fps; $V_{avg}/V_c = 0.8167$						
A3	0.735	10	9:05	2.6875	6.826	
B1	0.735	10	19:49	3.2500	8.255	
C1	0.735	3	18:35	3.1250	7.938	
C4	0.735	6	18:55	3.1250	7.938	



Summary Results Grouped by V_{avg}

Test	Avg V [fps]	Ya [in]	Duration [h:mm]	Scour Depth [in]	Scour Depth [cm]	Notes
0.773 fps; $V_{avg}/V_c = 0.8589$						
A2	0.773	8	17:57	3.1875	8.096	
B2	0.773	8	22:08	3.2500	8.255	
R1	0.773	8	18:13	3.0000	7.620	Live Bed Scour
C5	0.773	3	15:39	3.2500	8.255	
C6	0.773	6	15:39	3.1875	8.096	
XR1	0.773	3	17:17	2.8750	7.303	Live Bed Scour
XR2	0.773	6	16:06	3.3125	8.414	Live Bed Scour
0.835 fps; $V_{avg}/V_c = 0.9278$						
A4	0.836	9	14:27	3.3125	8.414	
B4	0.836	9	17:46	3.3750	8.573	
C2	0.836	3	16:22	3.2500	8.255	Live Bed Scour
C3	0.836	6	20:16	2.8750	7.303	Live Bed Scour



Velocity Profile Comparisons- Summary

- **Open water**- logarithmic as expected
- **Covered flows**-
 - Zero velocity at boundaries (no slip condition)
 - Maximum velocity location is a function of-
 - Flow depth
 - Roughness of boundaries
 - Viscosity of fluid
 - Maximum velocity located near the middle for floating smooth cover → similar boundary roughness
 - Larger maximum velocity for rough cover → live-bed
- **Pressurized flows**- velocity shifts toward smoother boundary
 - Less scour for pressurized smooth cover → shifts toward cover
 - More scour for pressurized rough cover → shifts toward bed
 - Shifts more pronounced for larger V_{avg}/V_c and larger pressure head
 - Pressurized flows- V_{avg} not acceptable indicator for live-bed scour
- **Combined effect of roughness and pressure flow**

