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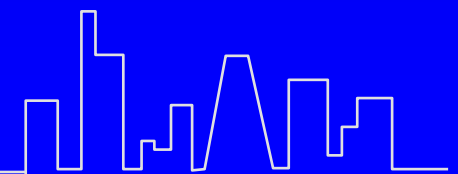
*2005 Tri-Service Infrastructure Conference*

*St. Louis, Mo. August 4, 2005*

## **Design of Concrete Lined Tunnels in Rock**

# **CUP McCook Reservoir – Distribution Tunnels Contract**

**David Force, S.E.**  
David Force, S.E.

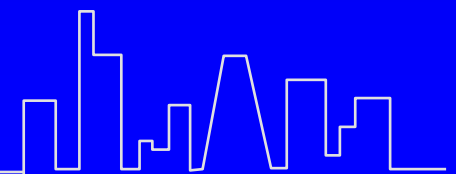




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# Outline of Presentation

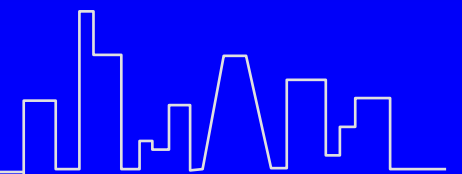
- **General Project overview – McCook Reservoir Project**
- **Overview of Distribution Tunnels Contract**
- **Design of Circular Tunnel Lining on Distribution Tunnels Contract**
- **Design of Concrete Bifurcations on Distribution Tunnels Contract**
- **Overview of Steel Liner Design on Distribution Tunnels Contract**





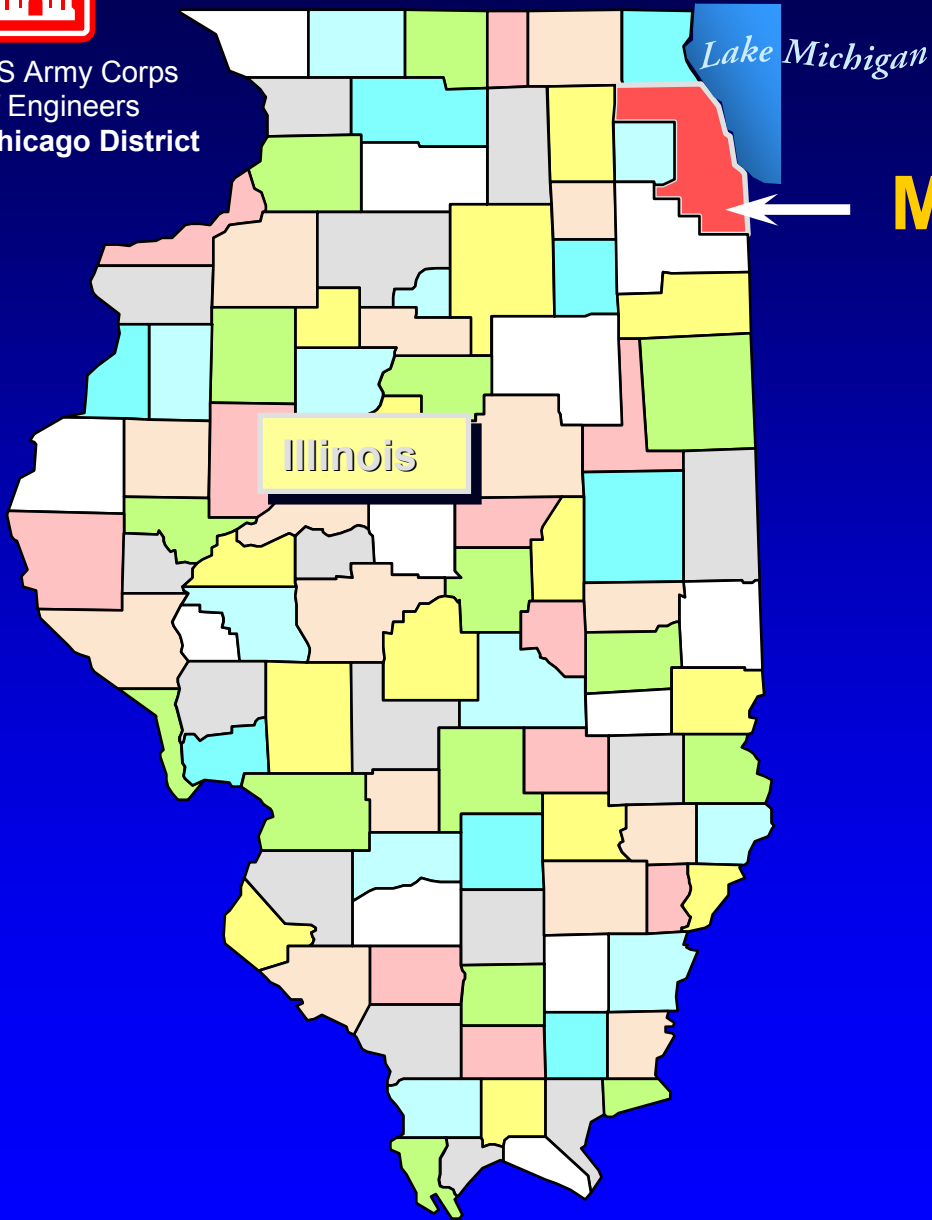
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# McCook Reservoir Project



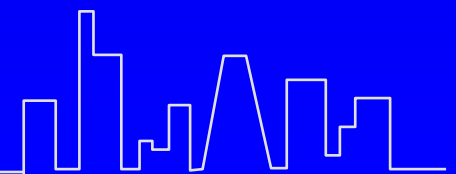


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**MWRDGC**

**Metropolitan  
Water  
Reclamation  
District of  
Greater  
Chicago**







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Overall Goal – Control Flooding and  
Keep CSO Out of Lakes and Rivers !

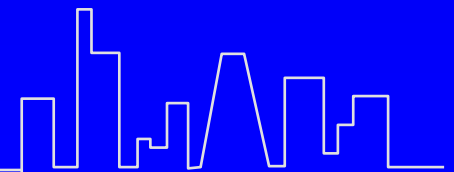




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# McCook Reservoir

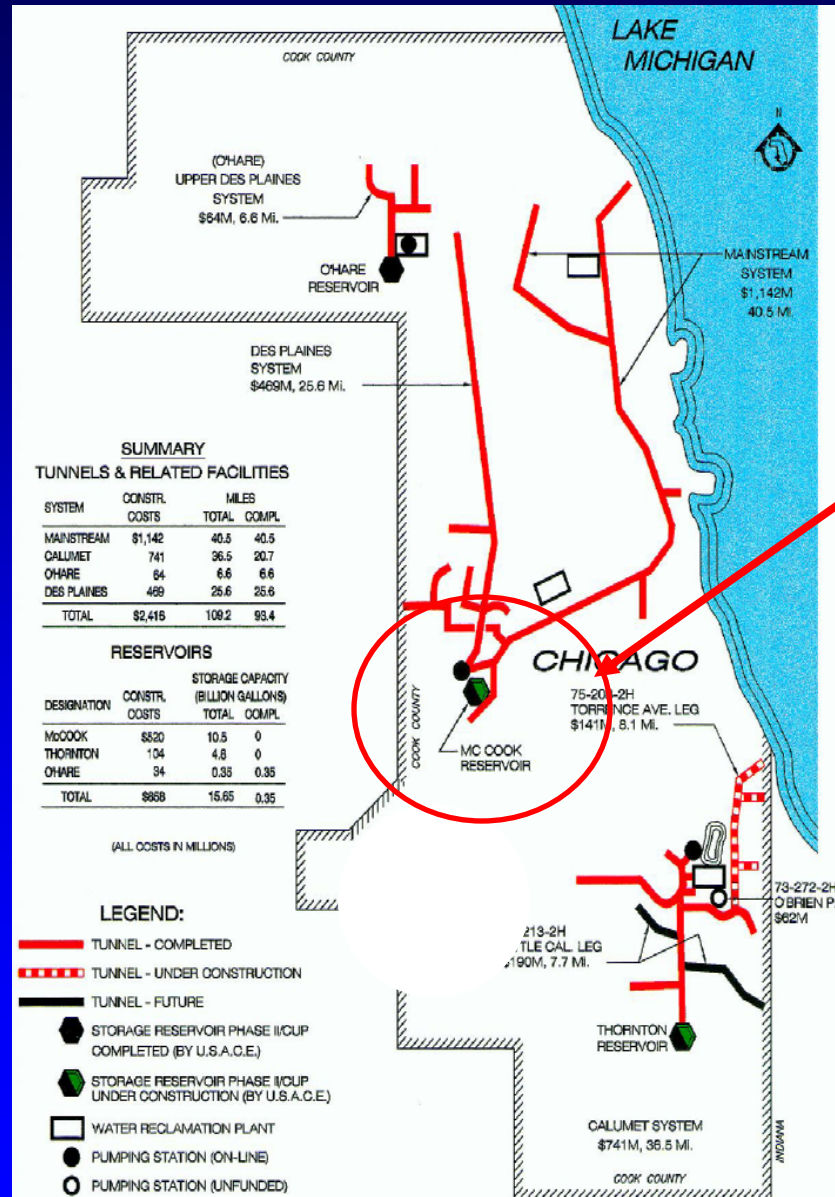
- **Estimated cost \$520 million**
- **Provides flood control between Des Plaines River and Chicago Sanitary and Ship Canal**
- **Excavation of reservoir will be by Drill and Blast (Quarrying)**
- **Captures CSO's from Chicago and 37 suburbs**
- **Provides > 10 billion gallons of storage**
- **Scheduled Project Completion - FY 2012**



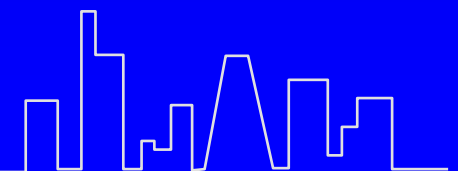


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# TARP / CUP SYSTEM



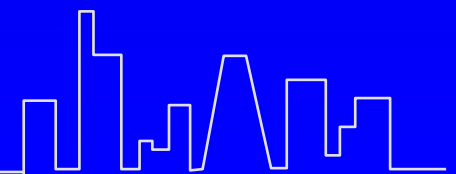
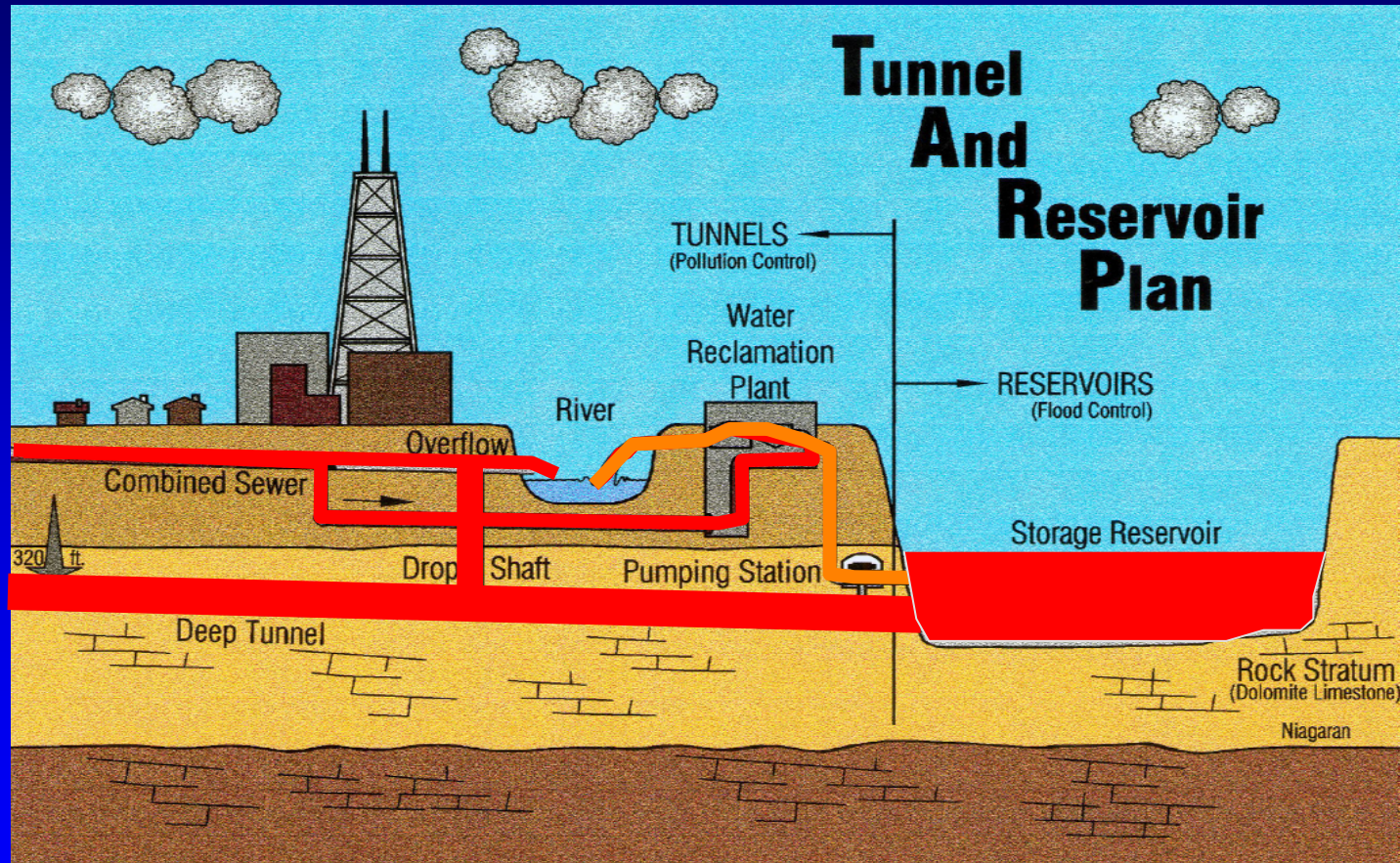
McCook Reservoir







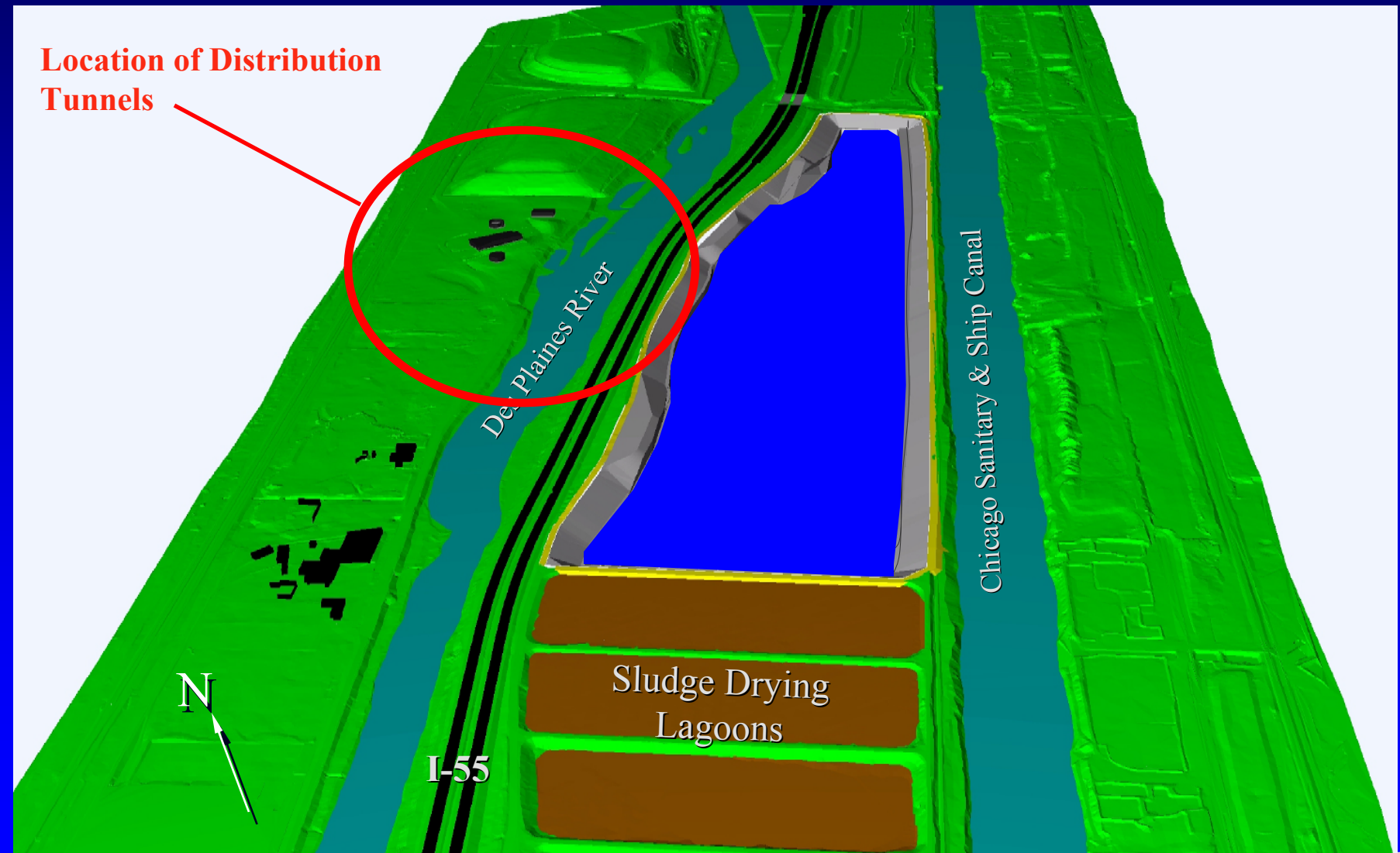
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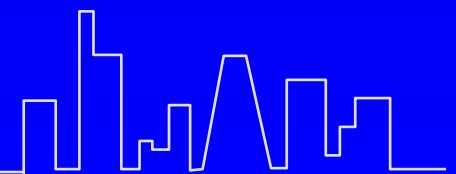
# Reservoir Project





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# Distribution Tunnels Contract

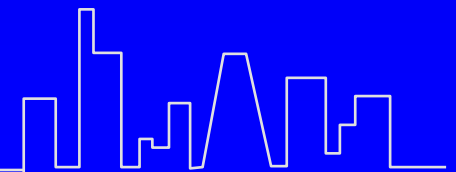




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# Distribution Tunnels Contract

- **LS:** *Metropolitan Water Reclamation District of Chicago (MWRD)*
- **Designer:** *Montgomery Watson Harza*
- **Construction Contractor:** *Kenny Construction*
- **Gate Designer:** *INCA (sub to Kenny)*
- **Steel Liner Fabricator:** *CBI (sub to Kenny)*



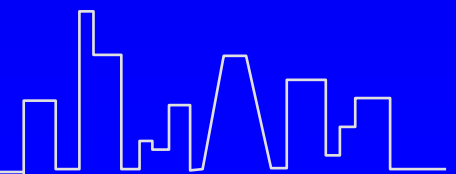




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# Purpose of Distribution Tunnels

- **Convey and Distribute CSO's between the new Reservoir and the existing TARP Pump Stations and Tunnels**

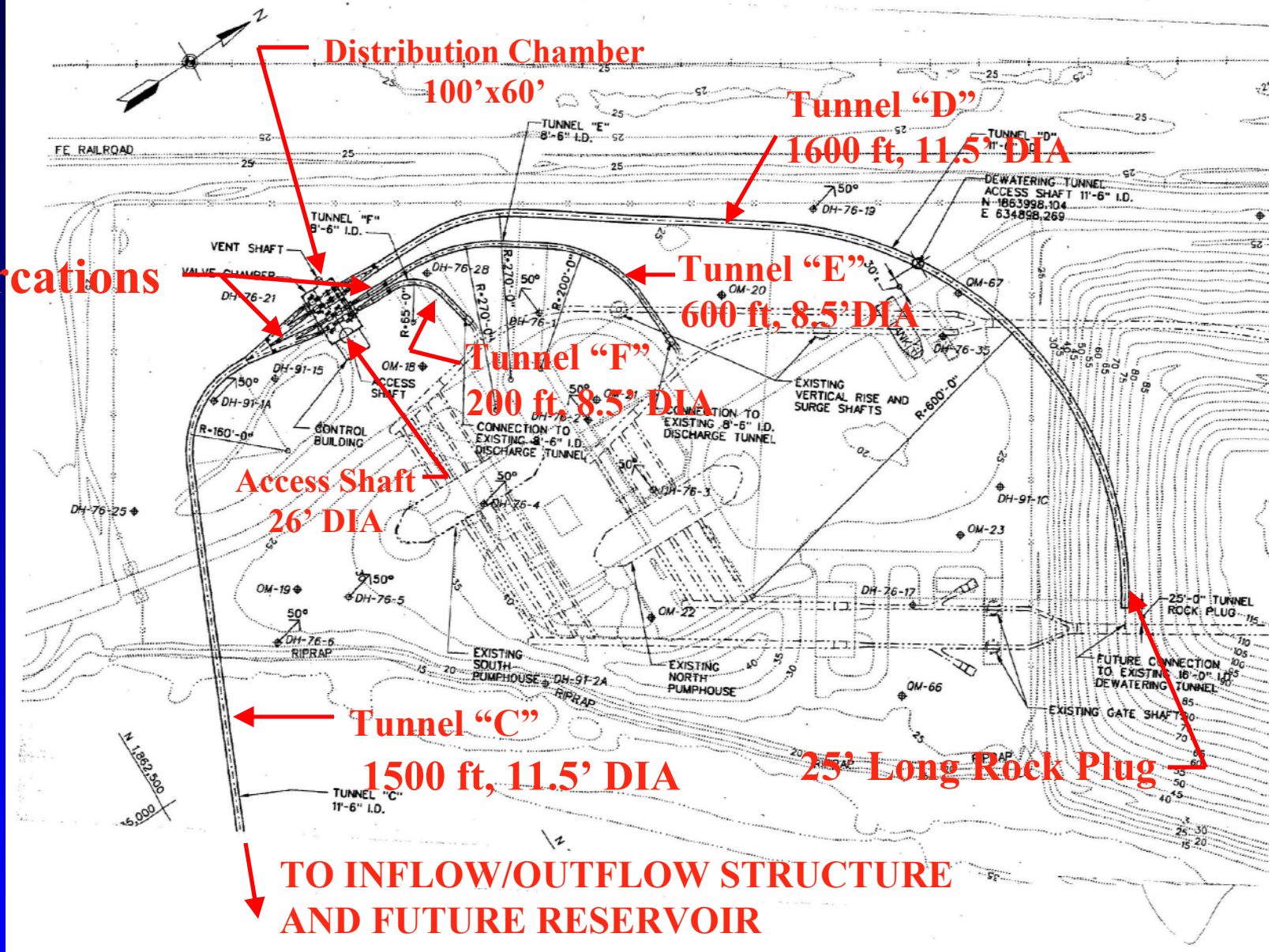




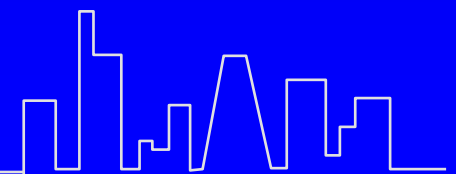


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**Bifurcations**

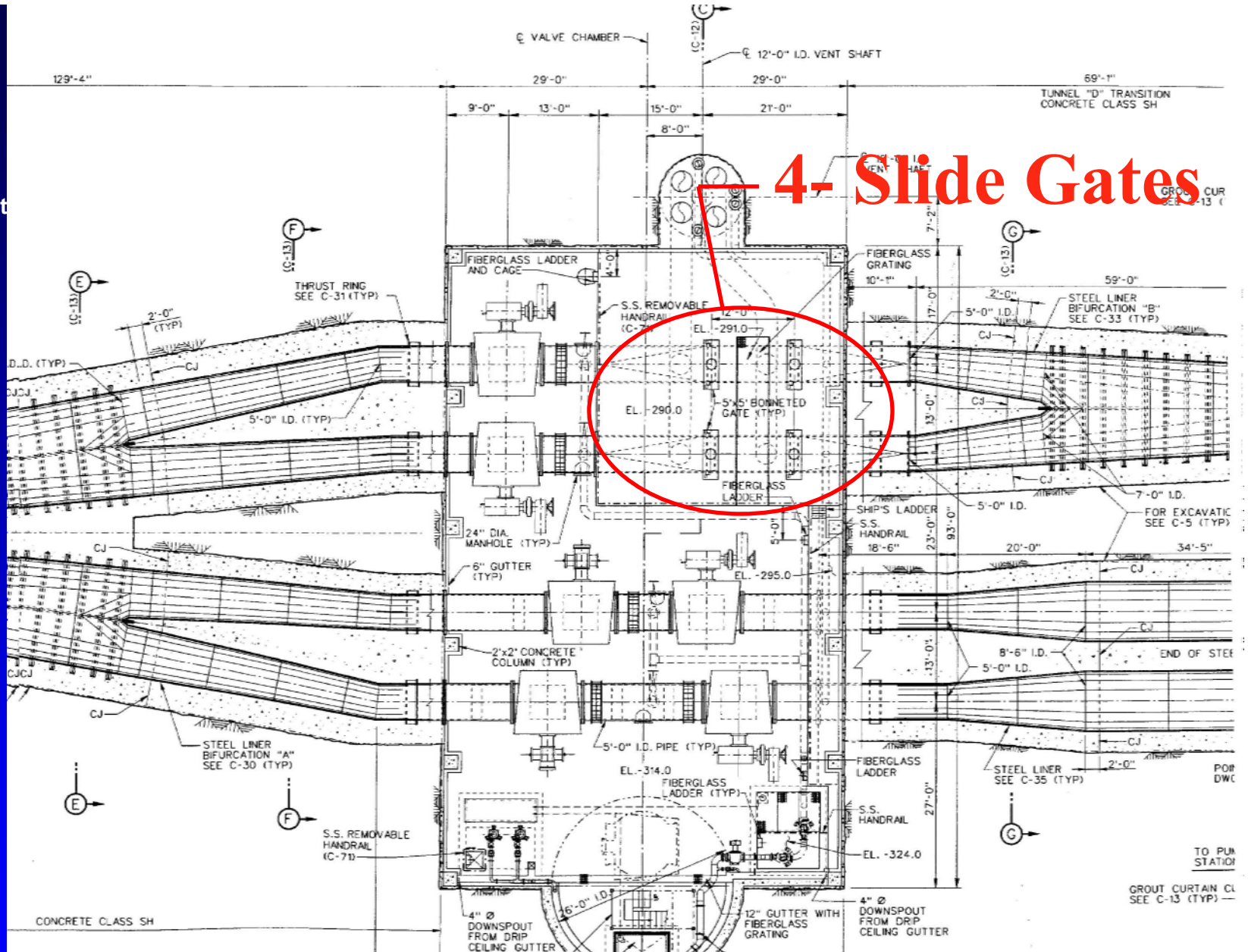


**Plan – Distribution Tunnels**

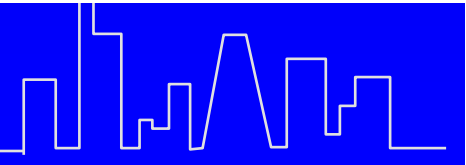




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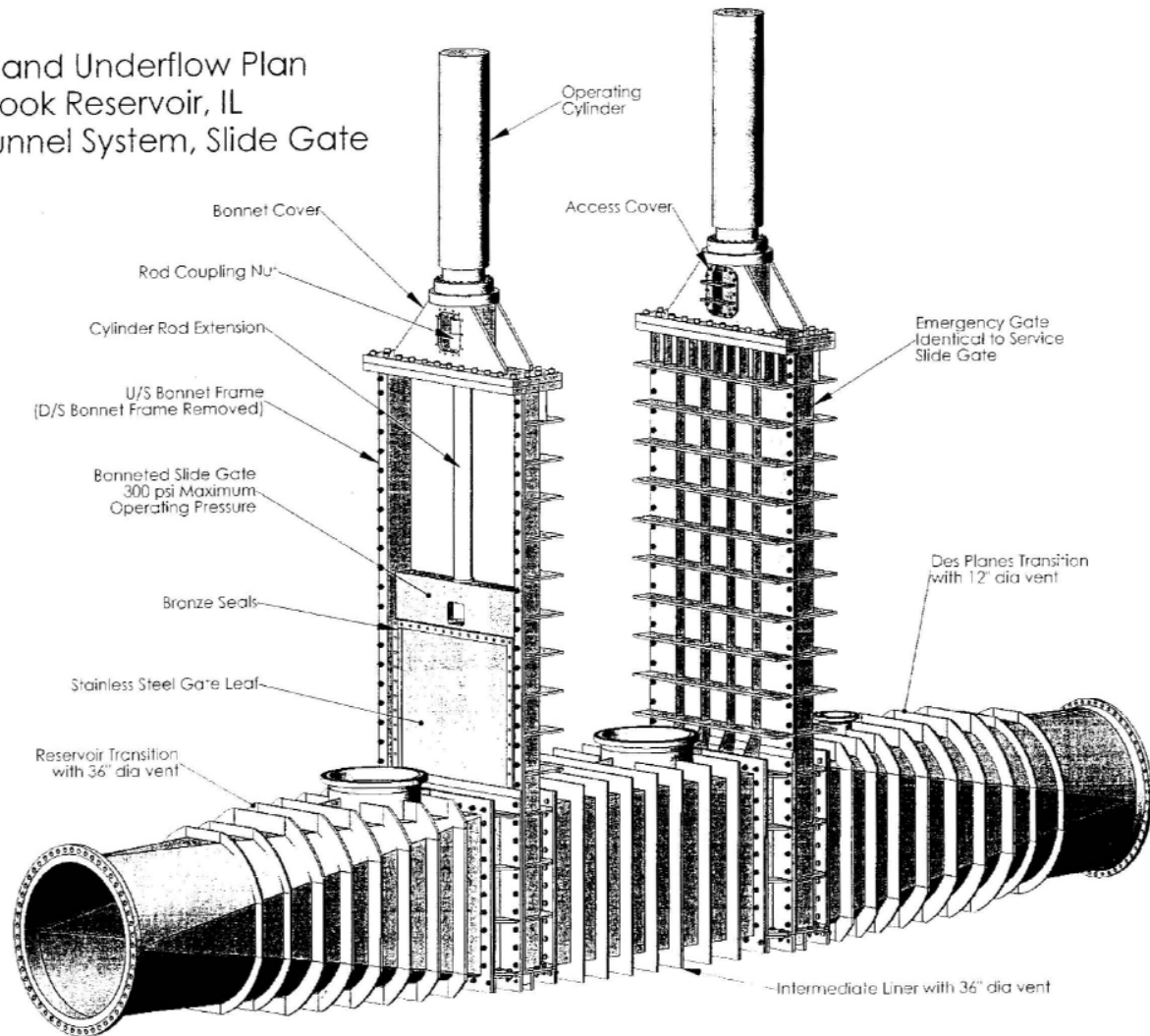
# Distribution Chamber





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## Chicagoland Underflow Plan McCook Reservoir, IL Distribution Tunnel System, Slide Gate



# Bonneted Slide Gates – 5' x 5'





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# CONTRACT COST/SCHEDULE

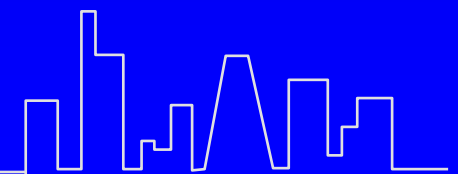
<b>Total contract</b>	\$60 million
Completed	85%
Anticipated Completion Date:	Jan 2006





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# Design of Circular Tunnel Lining





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EM 1110-2-2901  
30 May 1997

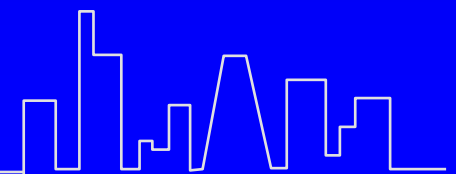
ENGINEERING AND DESIGN

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# Tunnels and Shafts in Rock

LIBRARY COPY

ENGINEER MANUAL

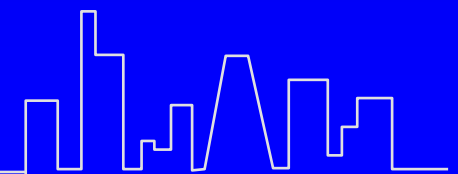




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# Tunnels General

- **3100 Lineal Feet of 11.5' DIA. Tunnel**  
**800 Lineal Feet of 8.5' DIA. Tunnel**
- **Approximately 310' below grade**
- **Excavation by Drill and Blast - Creating a horseshoe shaped excavation**



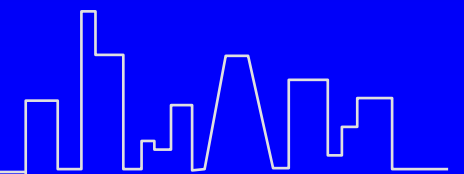


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**Rock Dowels**



**Tunnel Excavation –  
Drill and Blast**



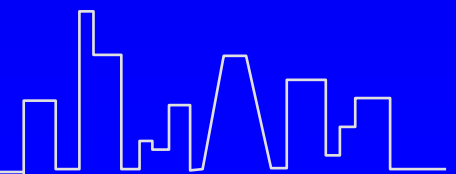




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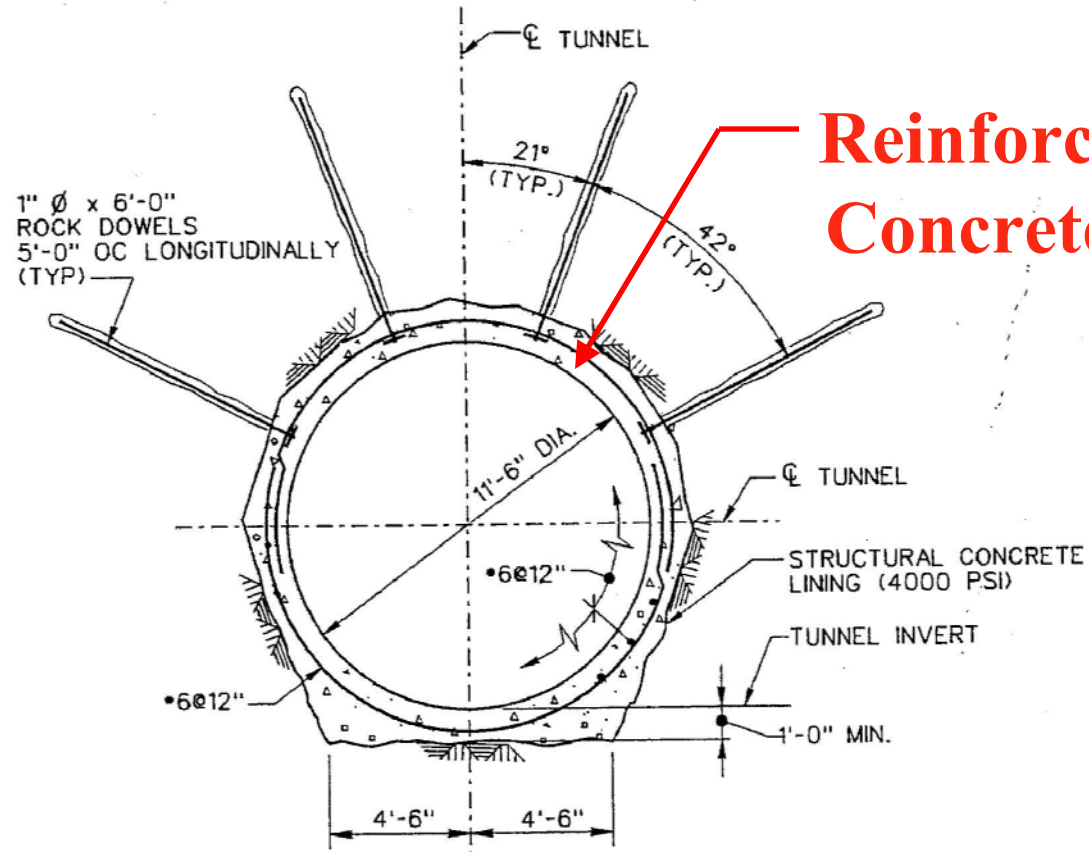
# Tunnels General (con't)

- **Final Tunnel cross sections are Circular except at bifurcations.**
- **At bifurcations cross sections are oblong or vary between circular and oblong**





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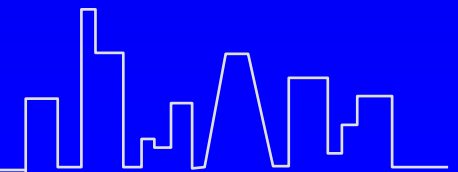


**Reinforced and  
Concrete Lined**

B - B  
TUNNEL CROSS SECTION

SCALE: 1/4" = 1'-0"

**Typical Tunnel Cross Section**

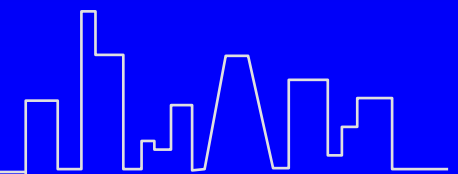




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# Why Reinforced?

- **Most of the Chicago TARP tunnels are not reinforced because;**
  - **Exfiltration is not a concern since external pressures from ground water exceed internal pressures**



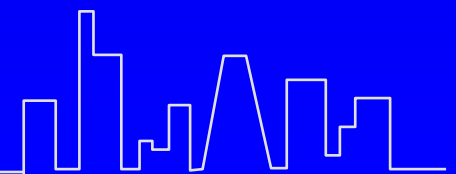


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# Why Reinforced? (con't)

**On Distribution tunnels reinforcement is provided because;**

- **The proximity of the reservoir draws groundwater down allowing exfiltration**

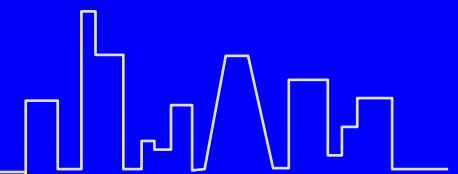




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# Hydraulic Design Considerations

- **Velocities  $> 100$  fps can occur around gates and valves in tunnels – those areas are steel lined and backed with 6000 psi concrete**
- **Tunnel C and D are low velocity gravity – 4000 psi concrete**





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# Design Loads

## Circular Tunnel Liners

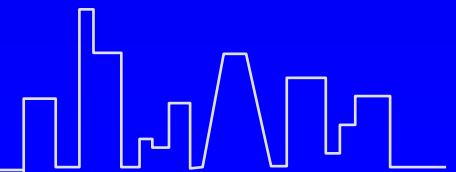
- **Internal Pressures**

Max Hydraulic Dynamic Pressure of 160 psi

- **External Pressure**

Hydrostatic Load from Ground Water

head = 310 ft or 132 to 134 psi

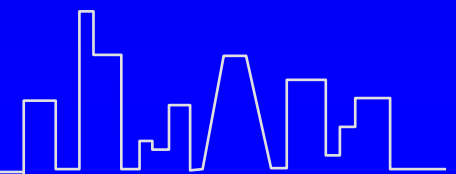




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# Key Design Assumptions

- **All rock loads are assumed to be fully supported by permanent rock dowels. No rock loads to the liner.**
- **Relaxation of the rock and stress redistribution is assumed to occur prior to installation of the lining**

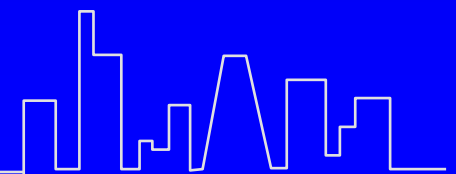




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# Crack Width Limitation (Internal Pressure Design)

- Crack Width Limited to .008" for water tightness
- Tensile stresses in the reinforcing are limited to limit the crack width.







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# Materials

- **Concrete strength:**

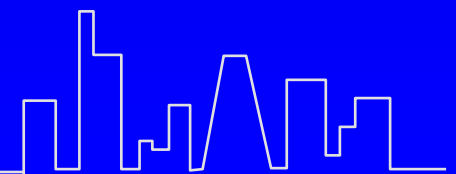
4000 psi in tunnels

6000 psi around steel liners

10,000 psi at concrete bifurcation

- **Reinforcing:**

ASTM A615, GR 60

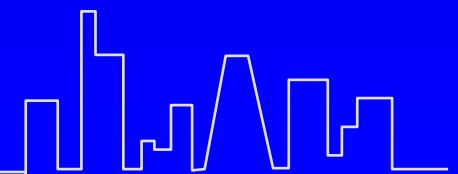




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# Analyses Procedure

**Tunnel Lining is analyzed for Internal  
External pressure**





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# External Pressure Design Procedure

**1. Determine and apply external pressures:**

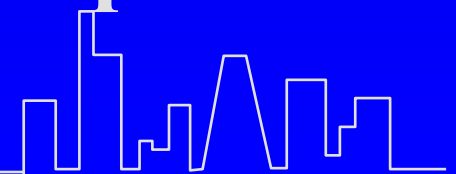
132 psi for 11.5' diameter tunnels

**2. Determine Load Case(s):**

1.1 D + 1.4 H (EM 2901, Table 9-1)

**3. Model tunnel Lining using STAAD**

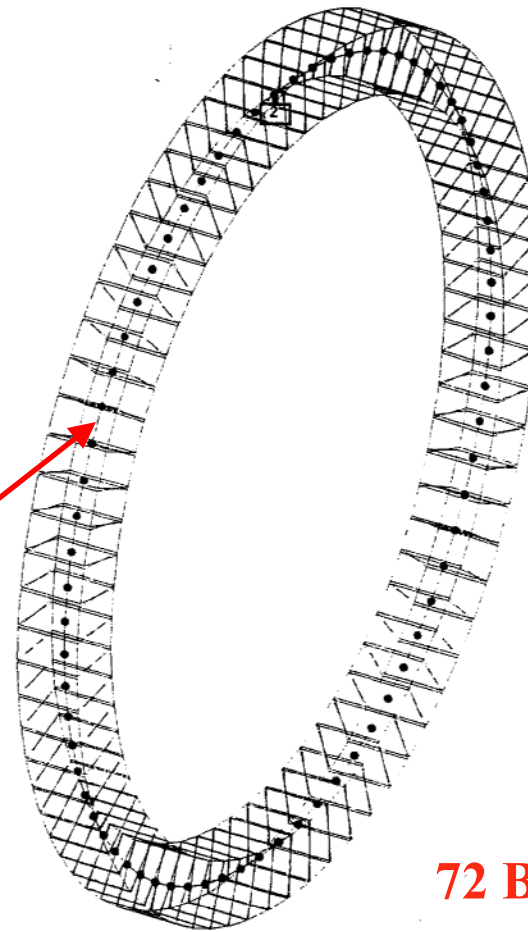
**4. Design Concrete for Hoop Compression**





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**Tunnel Lining modeled  
with beam elements**

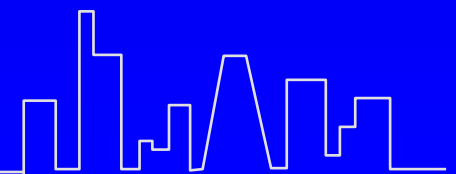


**72 Beam Elements**



11.5 ft I.D. Tunnel

**STAAD FE Model**

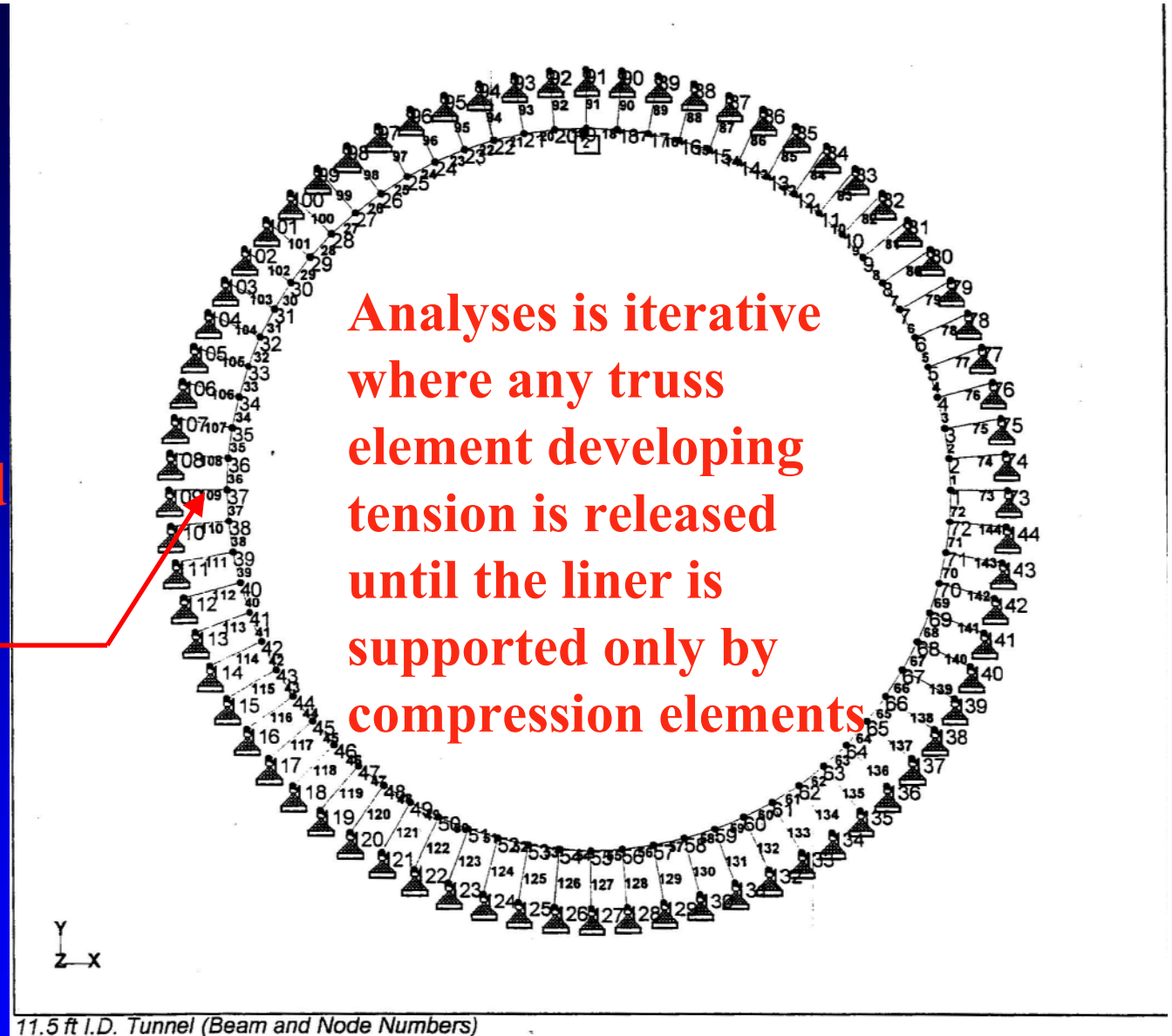




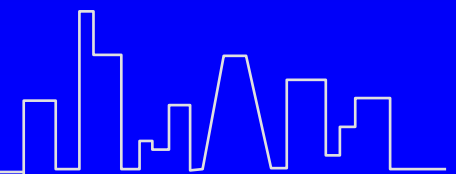
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Rock Modeled  
With truss  
elements

Radial spring  
Stiffness assigned  
Per Equation 9-18,  
EM 2901.



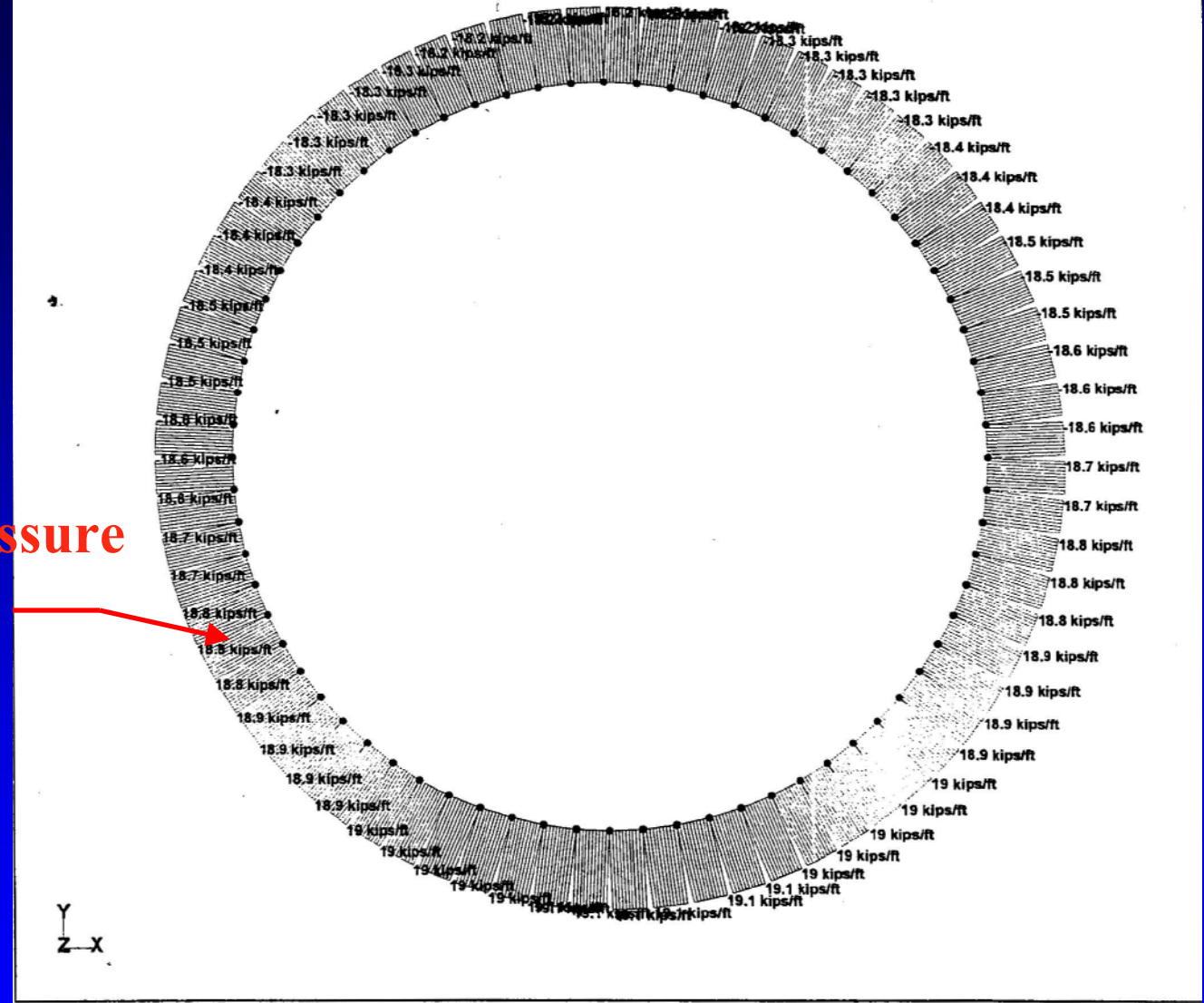
STAAD Model





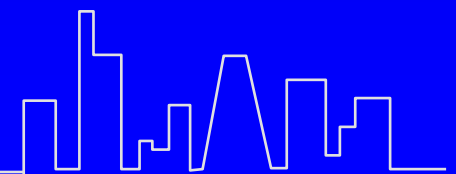
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External Pressure  
Load 132 psi



11.5 ft I.D. Tunnel (Pressure Loads)

STAAD Model





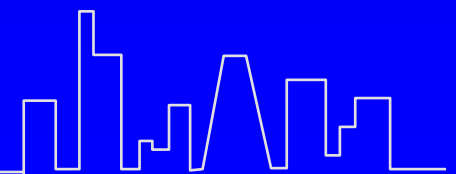
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# Results – External Pressure Design

- **Primary Load is hoop compression**

**$P_u = 164 \text{ K/FT}$  for 11.5' Tunnels**

- **Moments and Shears are negligible**





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# Internal Pressure Design Procedure

## 1. Determine and apply internal pressures:

160 psi .....11.5' diameter tunnels

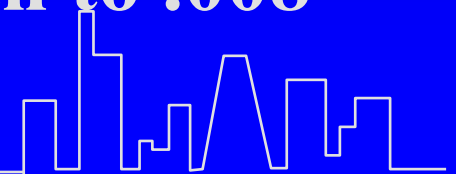
## 2. Determine Load Case(s):

1.1 D + 1.4 H (EM 2901)

## 3. Model the tunnel using Program

“TUNNEL” developed by MWH.

## 4. Design Reinf. to Limit crack width to .008”



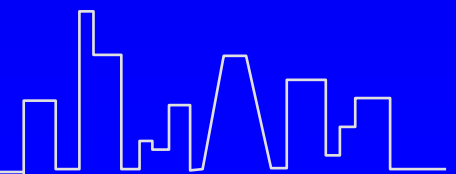




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# Model Features (Internal Pressure Design)

- 1. Surrounding Rock Mass was modeled as a thick walled cylinder**
- 2. Deformation properties of the concrete lining and sound and fissured rock were modeled.**
- 3. Strain compatibility was performed to determine % of load carried by the rock and the lining.**





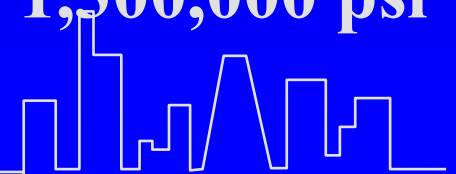
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# Rock Properties (Internal Pressure Design)

- A 40” ring of fissured rock was modeled – due to drill and blast excavations.
- Then, sound rock was modeled beyond the fissured zone

**Fissured Rock (grouted) .....Erock = 480,000 psi**

**Sound Rock .....Erock = 1,300,000 psi**



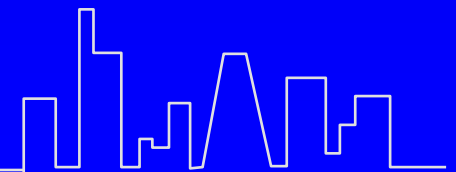


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# Results

## (Internal Pressure Design)

- **Primary Load was tensile stress in the Concrete.**
- Maximum Tensile Stress = 600 psi**
- **Reinforcement was sized to limit crack width to .008 inches**
  - **Resulted in #6 @12 inches**



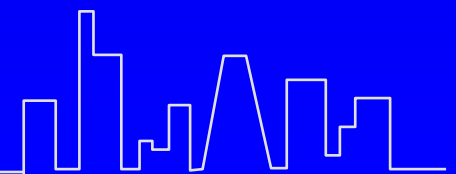


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**Rock Dowels**



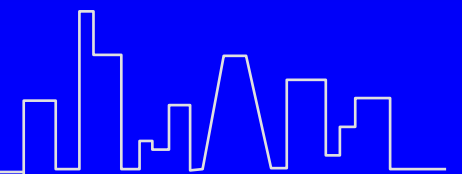
**Setting Forms**







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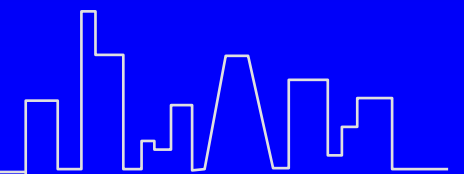




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## Window in Forms for Concrete Placement

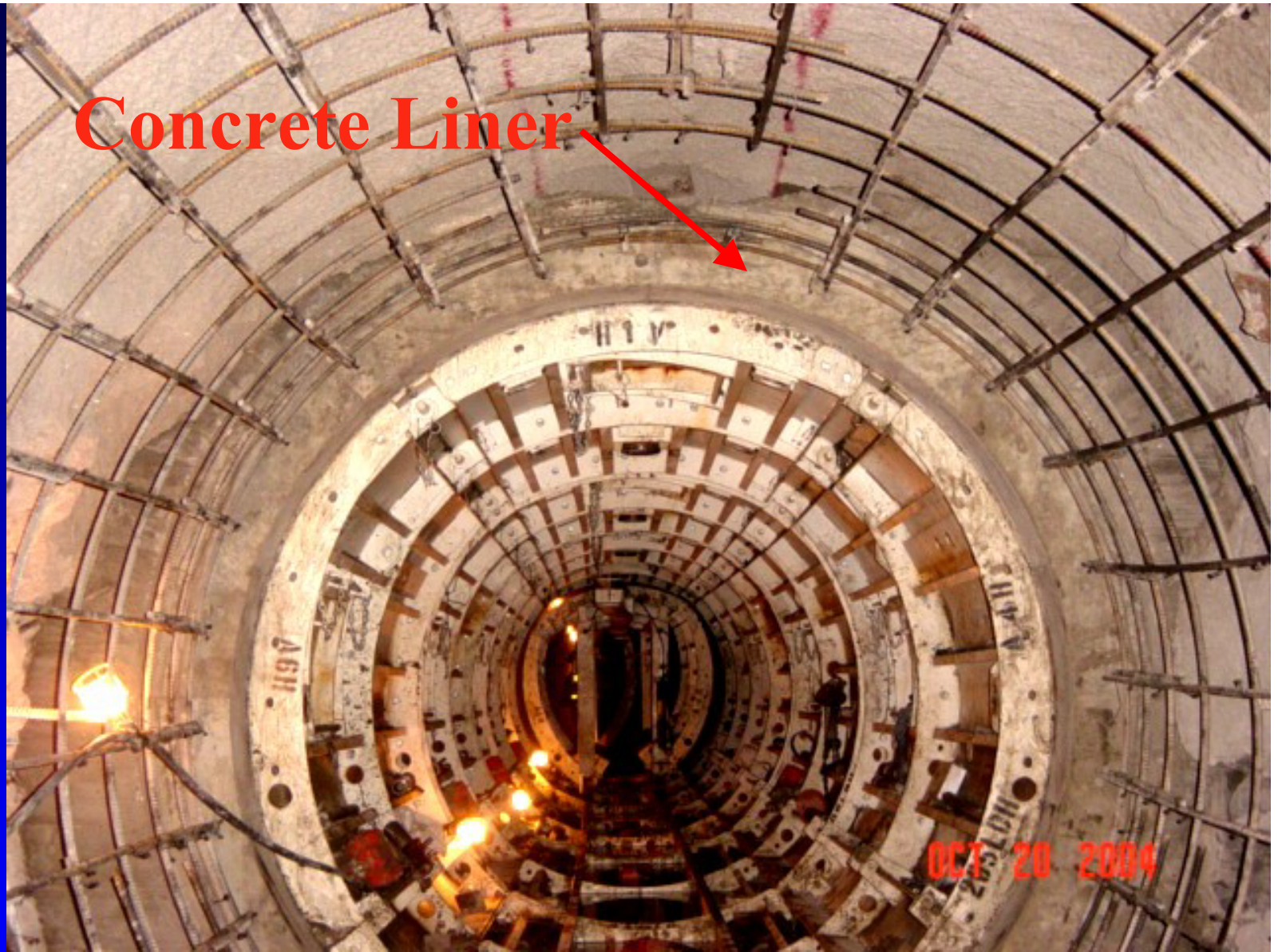






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Concrete Liner



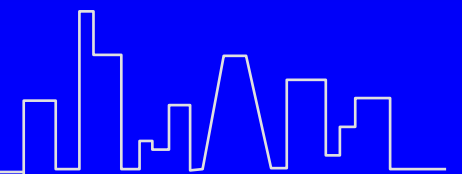
Tunnel Lining Formwork





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# Design of Concrete Bifurcations

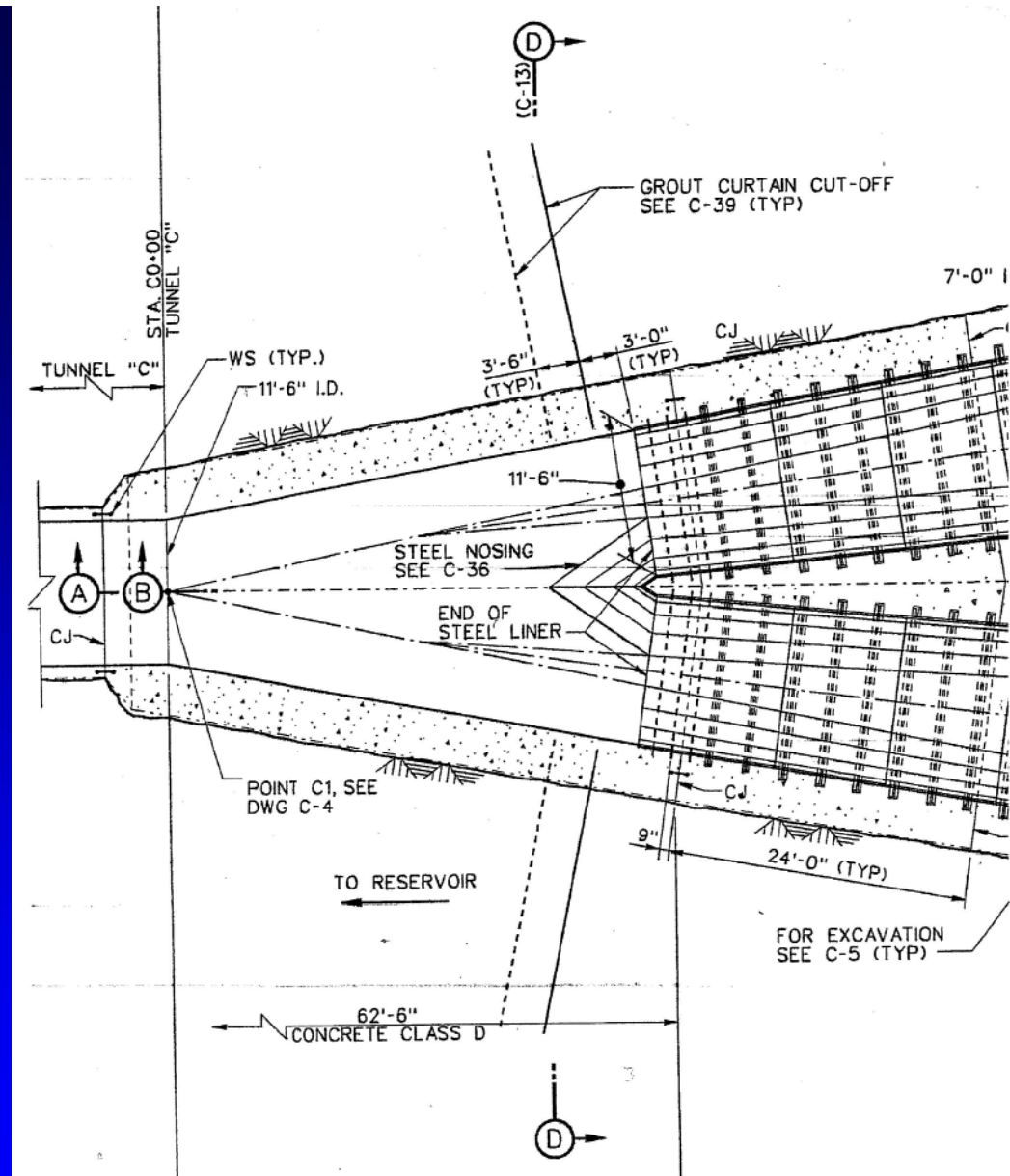




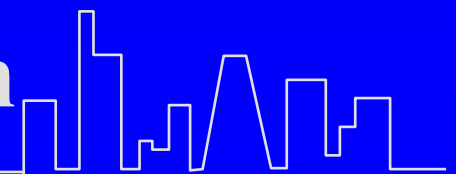




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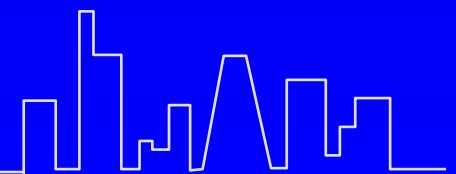
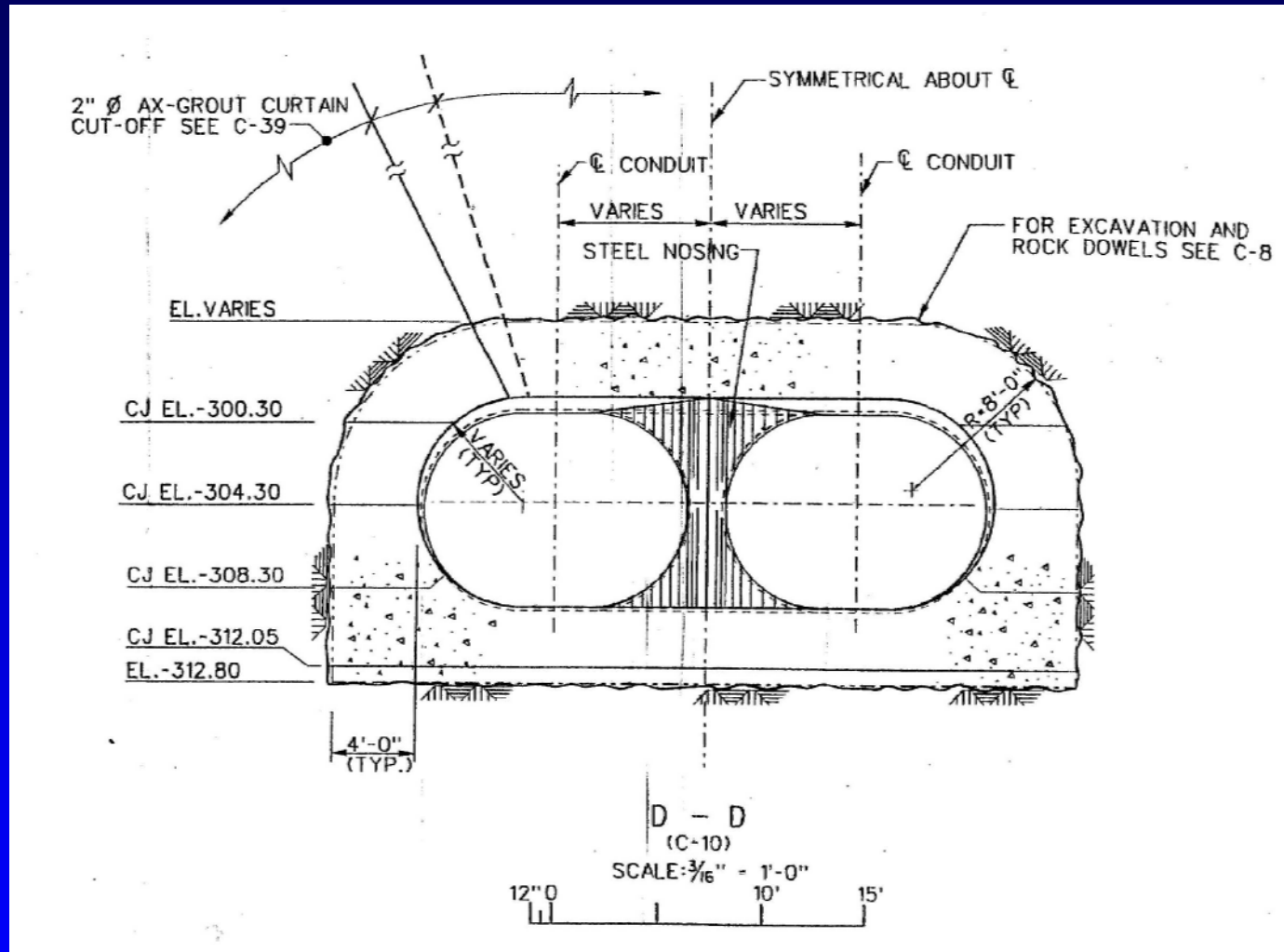


# Plan of Concrete Bifurcation





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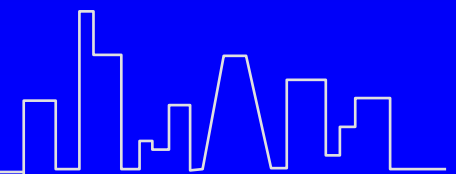




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# Hydraulic Design Consideration

- **Concrete Bifurcation is subjected to moderate turbulence - 10,000 psi concrete**





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# External Pressure Design

- **Designed for external pressure of 136 psi**
- **External Pressures are resisted by the use of rock anchors on all sides**
  - **necessary due to non-circular shape**
- **Concrete sections are designed per ACI 318.**

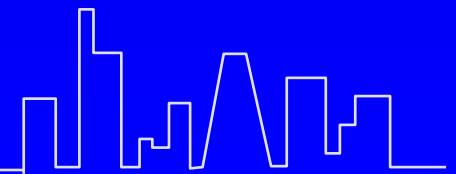




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# Internal Pressure Design

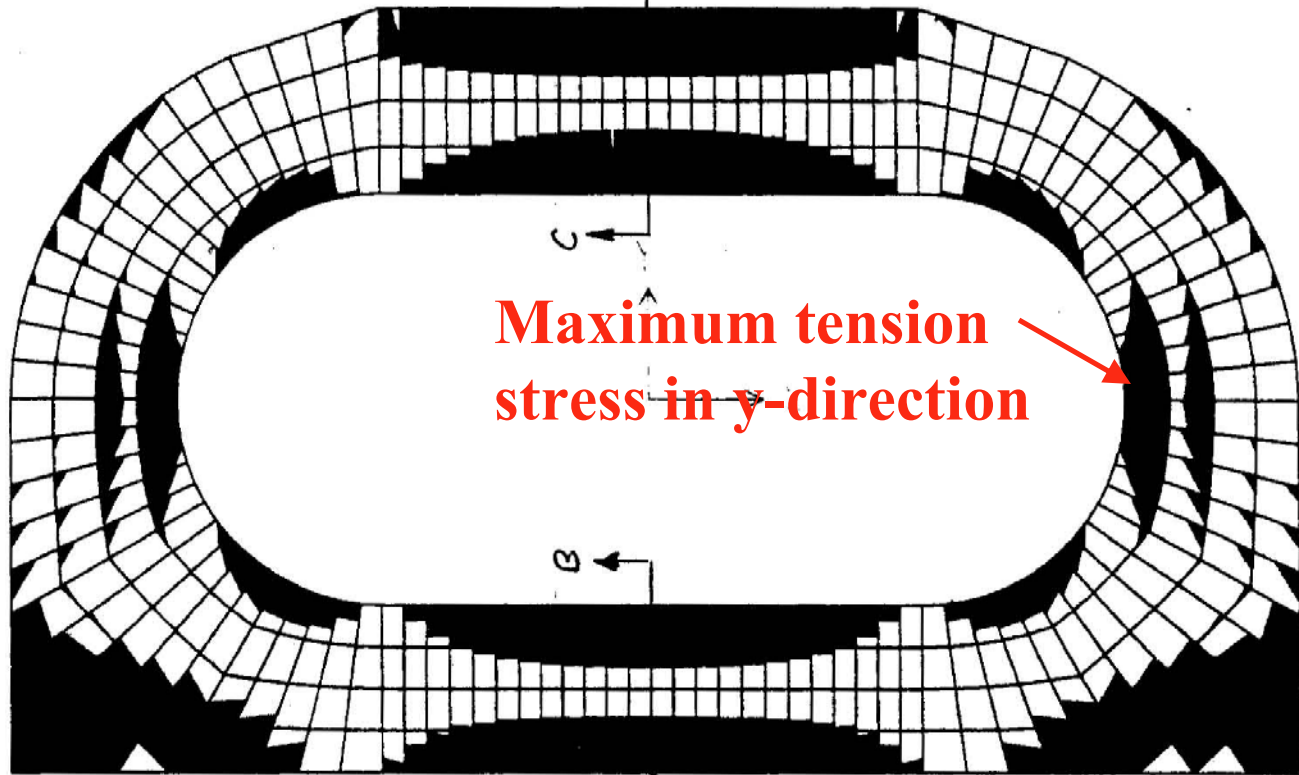
- **Designed for internal pressure of 160 psi**
- **SAP 2000 was used for the Analyses to include the effects of the surrounding rock mass. Similar to tunnel design.**
- **Concrete designed for watertightness and allowable crack width of .008 inches**





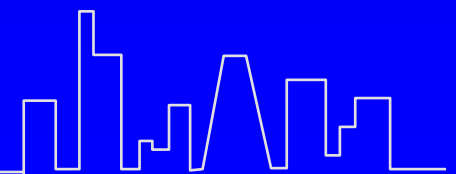
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**Maximum tension  
stress in x-direction**



**Maximum tension  
stress in y-direction**

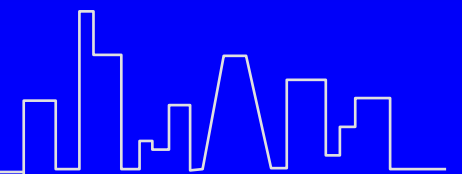
**Maximum Stresses –  
(Internal Pressure)**







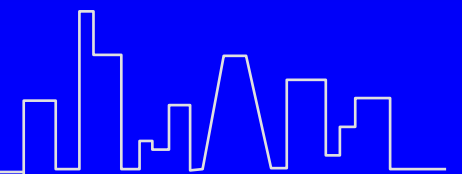
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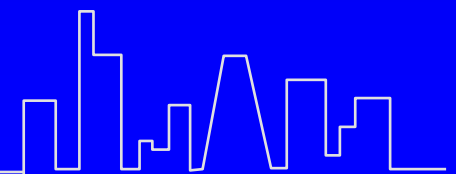
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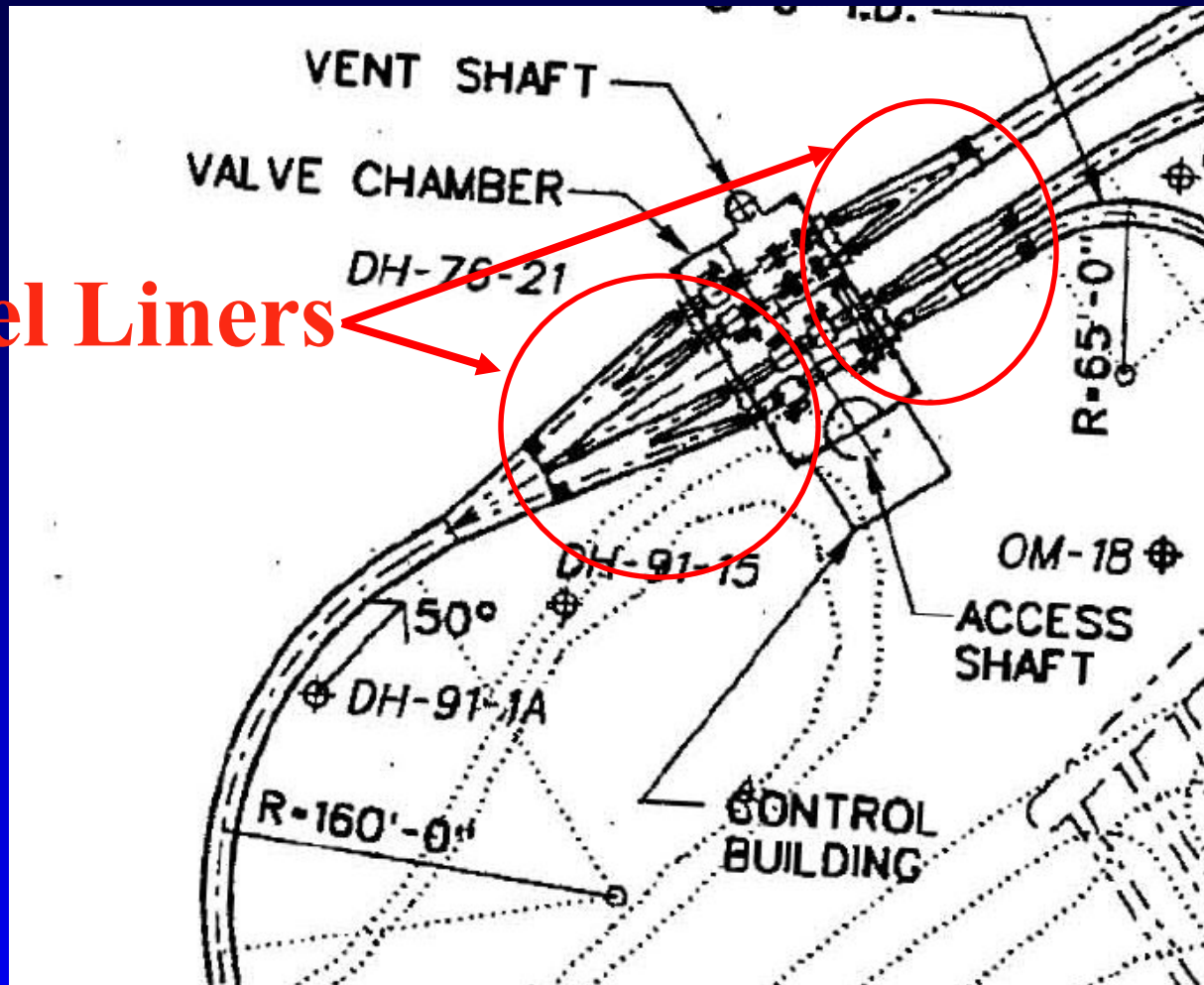
# Overview of Steel Liner Design



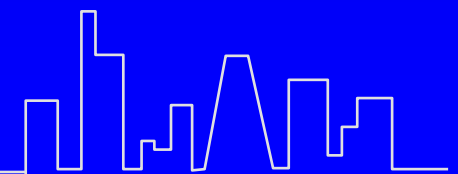


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**Steel Liners**



**Steel Liners Located at  
Distribution Chamber**

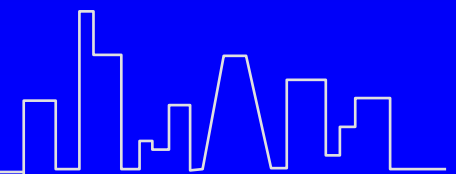




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# Purpose of Steel Liners

- Provide erosion protection in areas around Distribution Chamber
  - Velocities  $> 100$  fps
- Form the bifurcation geometry

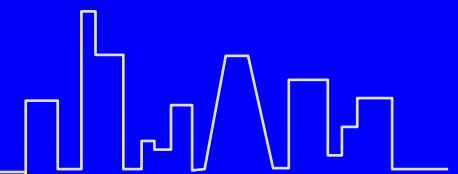




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# Design of Steel Liners

- **Designed for internal and external pressures**
- **Circular Section designed per EM 2901 Section 9-5d.**
- **ASME Pressure Vessel Code, Section VIII used for design of noncircular sections**
- **Stiffeners are provided on obround liner sections to resist buckling**
- **In areas of geometric discontinuities, 3-D STAAD Model used to design the cross sections.**

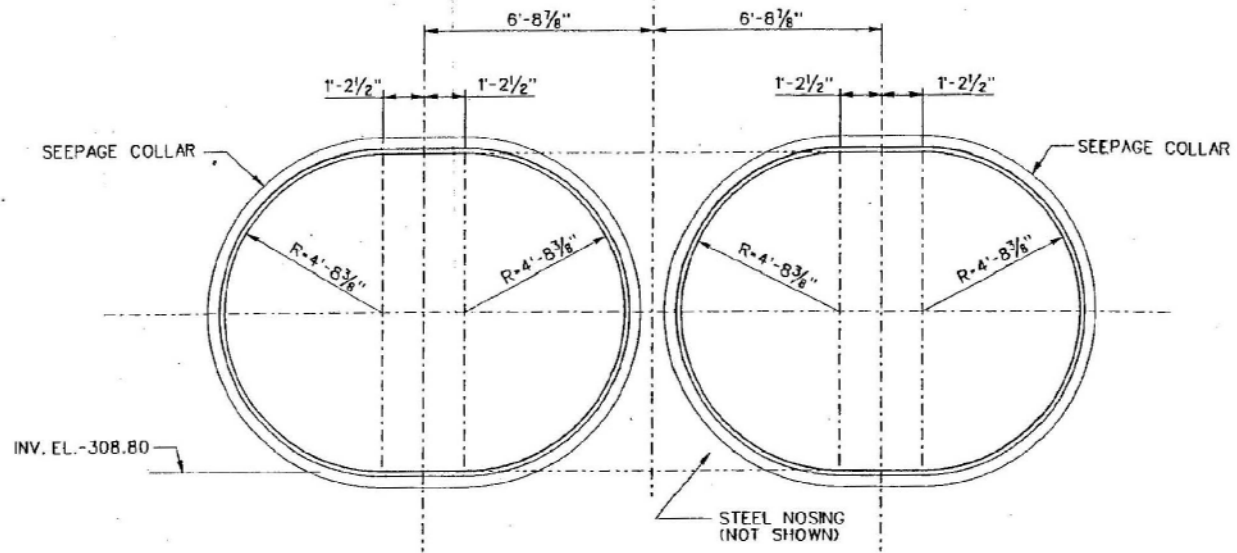




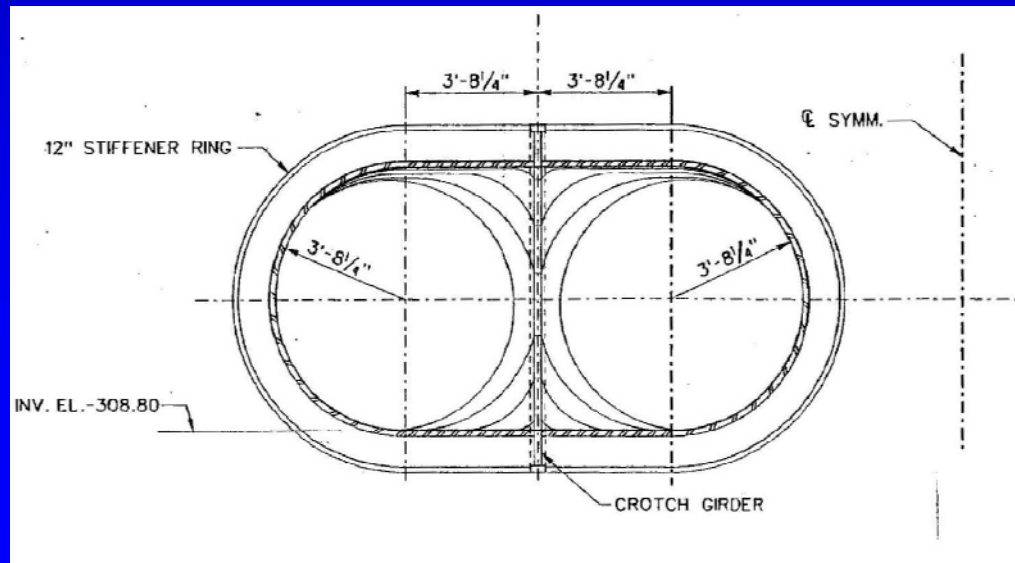




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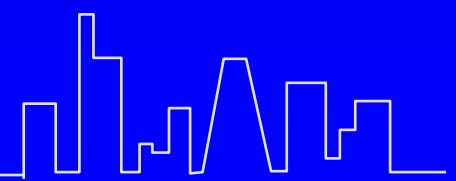
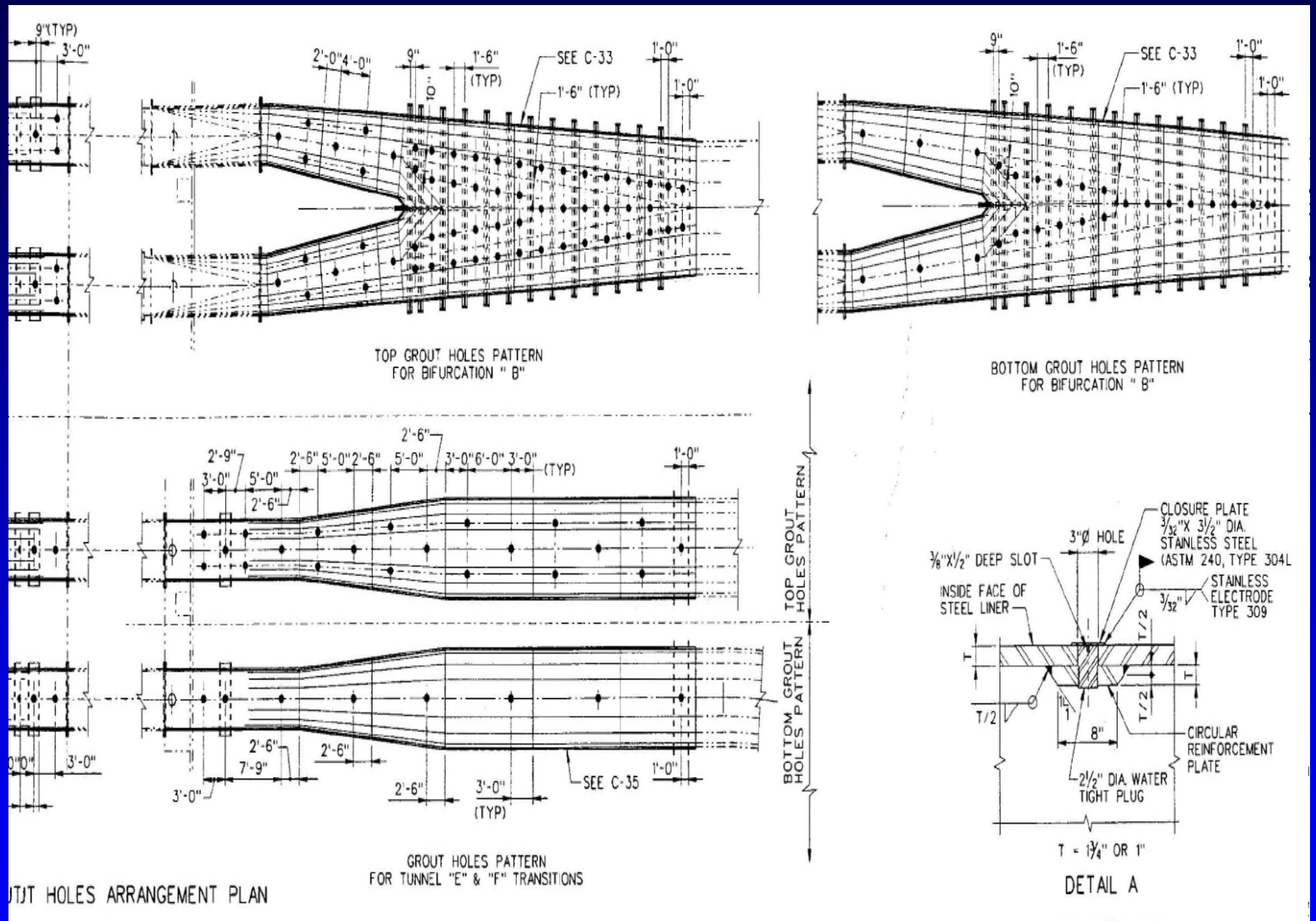


C - C  
(C-30)  
(NOTE 1)  
SCALE:  $\frac{3}{8}" = 1'-0"$   
12" 0' 2' 4' 6'





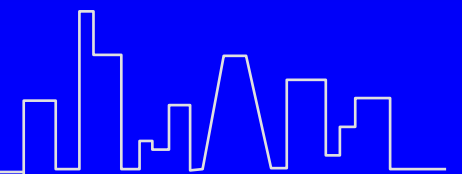
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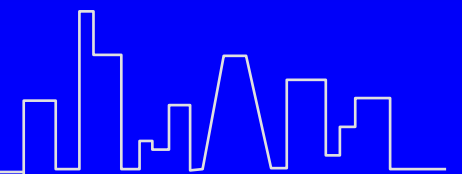


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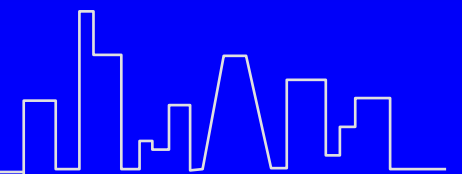
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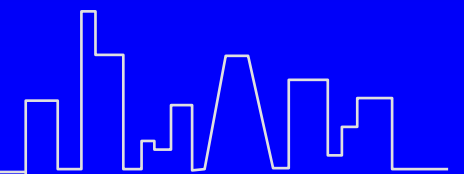




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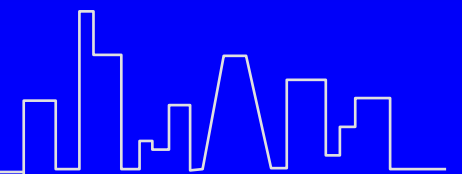
**Steel Nosing being lowered into  
26' dia. Access shaft**







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**View From Inside Steel Liner**







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**Steel Liner Being Welded – Oblong Section**







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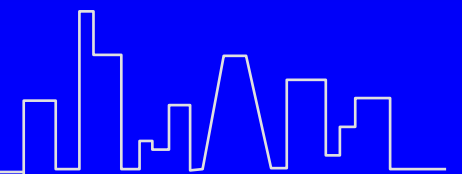


## Positioning Steel Nosing





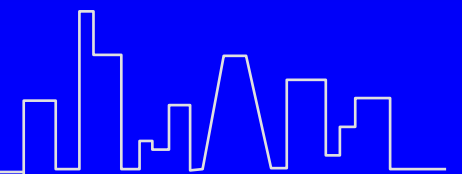
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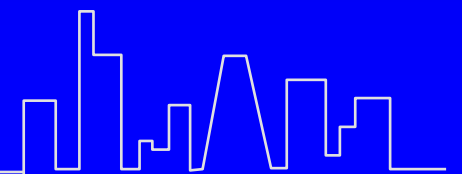
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# Thank You



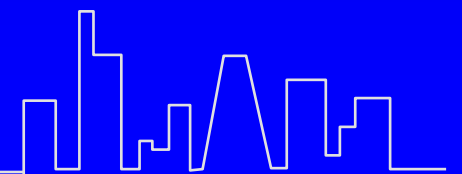


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# Machine-bored Tunnel (the new way)

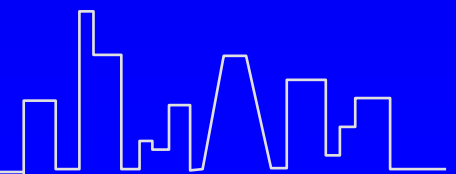






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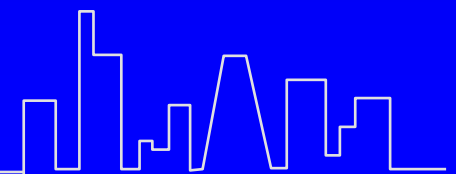
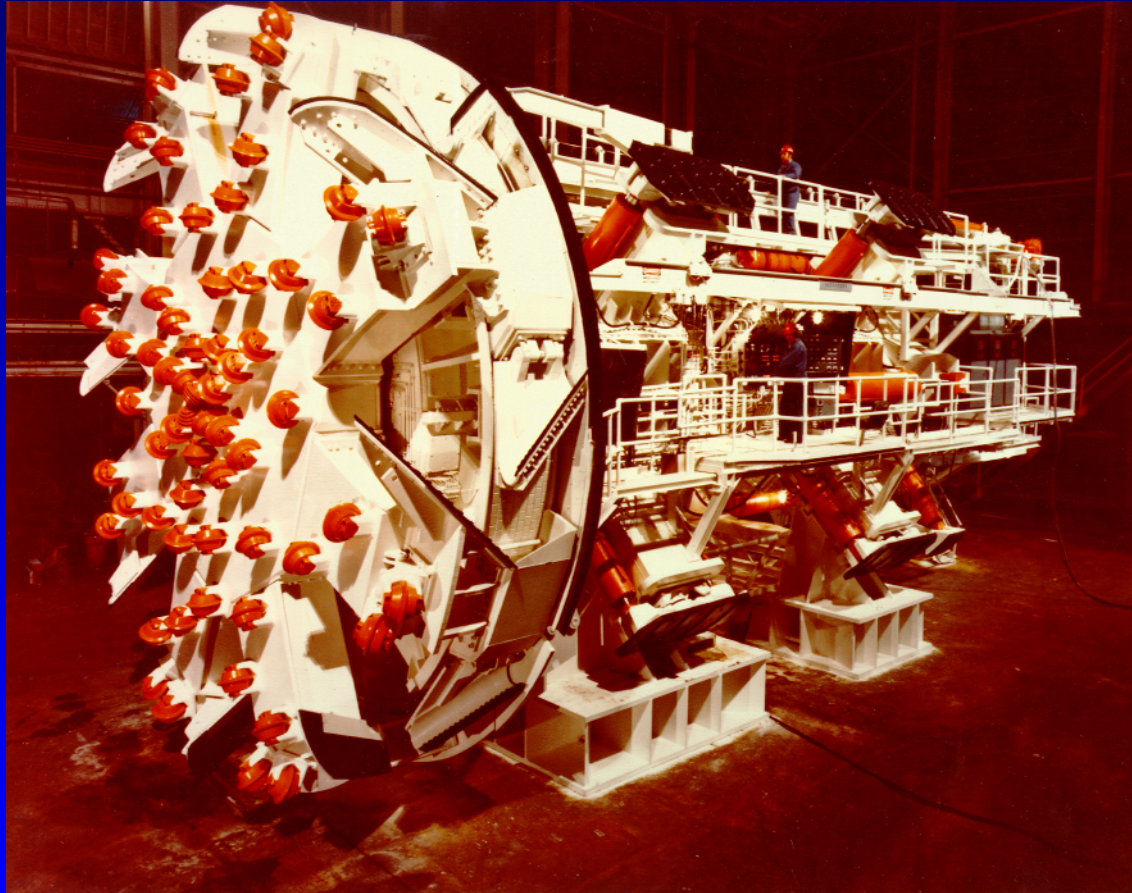
## Intersection of Machine-bored Tunnels





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# TUNNEL BORING MACHINE

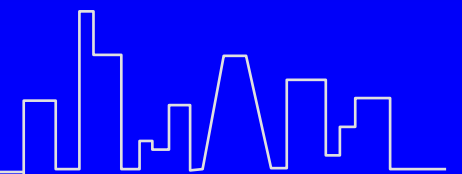






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## 27-ft Diameter Machine-bored Tunnel – Before Lining





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# Placing Concrete for Tunnel Lining







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# LINED TUNNEL

