

***DESIGN AND CONSTRUCTION OF ANCHORED
BULKHEADS WITH SYNTHETIC SHEET PILES
SEABROOK, NEW HAMPSHIRE***

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DESIGN AND CONSTRUCTION OF ANCHORED BULKHEADS WITH SYNTHETIC SHEET PILES, SEABROOK, NEW HAMPSHIRE

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Authority: Section 227 of the Water Resources and Development Act of 1996 (WRDA 96); Administered by ERDC

- **Research & Development: Advance the state of the art of coastal erosion control technology**
- **Encourage and achieve the development of innovative solutions to the erosion control challenge**
- **Communicate findings to the public, state, and local coastal managers**

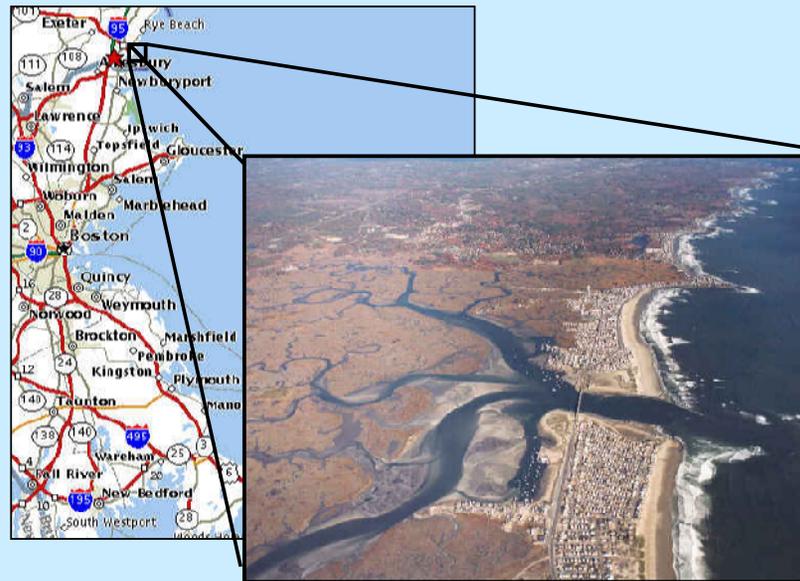


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Hampton-Seabrook Harbor, adjacent to the mouth of the Blackwater River, located in coastal New Hampshire, USA



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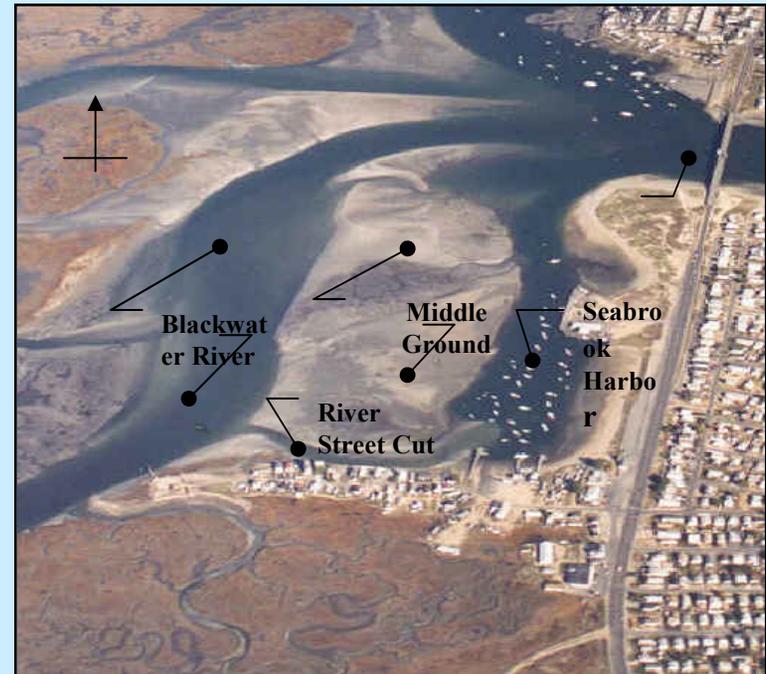
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DESIGN AND CONSTRUCTION OF ANCHORED BULKHEADS WITH SYNTHETIC SHEET PILES, SEABROOK, NEW HAMPSHIRE

- Objectives:
 - Replace lost intertidal sands
 - Reduce sand migration into the Harbor
 - Prevent shoreline erosion
- Constraints
 - Innovative Components
 - Ability to remove
 - Dredging window of time, November through March
 - Cost
 - 50-year design life
- Solutions:
 - Install cofferdams across the eroded channel using synthetic sheeting
 - Dredge sand from the shoaled areas of the River to encourage flow
 - Use the dredged sand to fill between the cofferdams to restore the sand flats

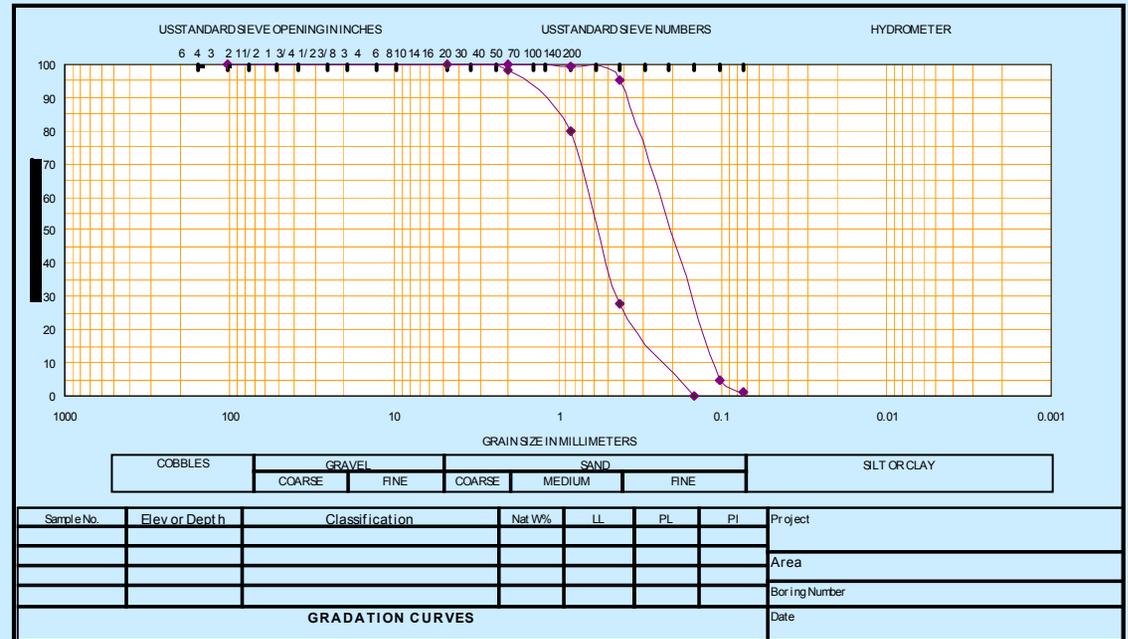


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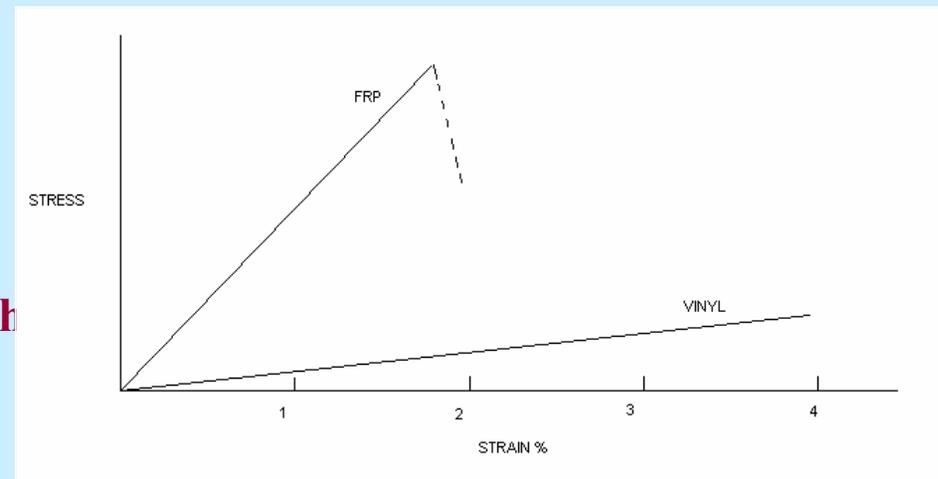
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- **Subsurface Conditions**
 - **Medium dense fine sand**
 - **Field SPT = 20**
 - **No obstructions**



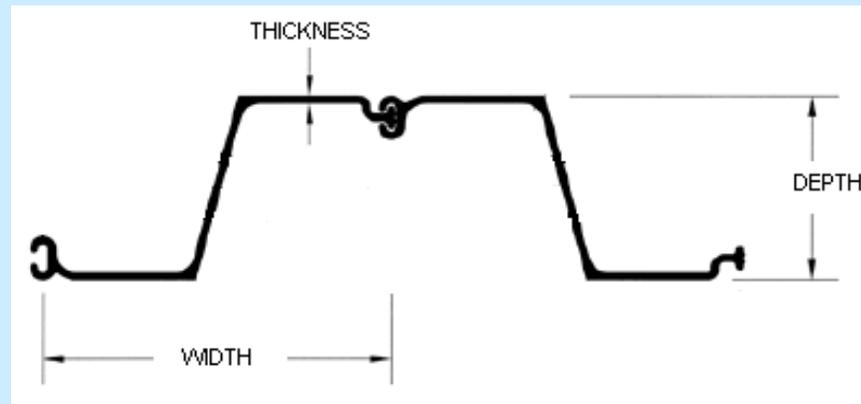
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- **Synthetic Sheeting**
 - **Vinyl: Made of virgin or recycled plastic or combination (recycled, with virgin veneer)**
 - High tensile strength
 - Less brittle
 - 10+ years of case histories of use
 - **Fiber Reinforced Polymer (Fiberglass) Glass fibers embedded in resin matrix such as polyester, polyurethane, or vinyl ester.**
 - High flexural strength
 - More brittle
 - Limited number of projects



DESIGN AND CONSTRUCTION OF ANCHORED BULKHEADS WITH SYNTHETIC SHEET PILES, SEABROOK, NEW HAMPSHIRE

| Property | Test Method | Vinyl | FRP | |
|------------------------|-------------|---------|---------------|-------------|
| | | | Longitudinal* | Transverse* |
| Tensile Strength (psi) | ASTM D638 | 6,300 | 60,000 | 10,000 |
| Tensile Modulus (psi) | ASTM D790 | 380,000 | 4,000,000 | 1,000,000 |
| Width (inch) | | 18 | 18 | |
| Depth (inch) | | 12 | 8 | |
| Thickness (inch) | | 0.65 | 0.25 | |
| Weight (lbs/sf) | | 8 | 4 | |

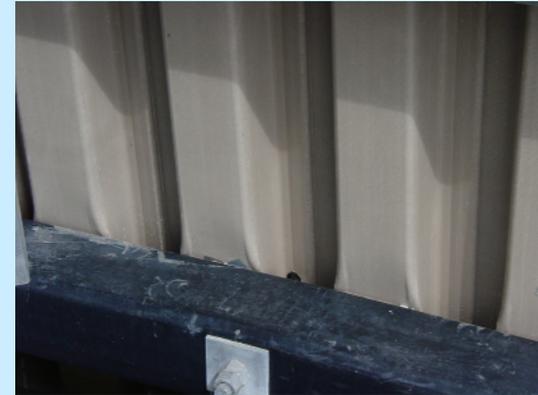


Note: Longitudinal (along) and Transverse (across) refer to fiber direction.



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- **Design Considerations**
 - **Inadequate shear strength or section depth**
 - **Lack of interlock strength**
 - **Limitation on cantilevered length: recent failures during construction**
 - **Longevity: UV resistance, cold**
 - **Lack of standardized tests, data and guide specifications**
 - **USACE Engineering & Construction Bulletin, 2002-31 October 2002:**

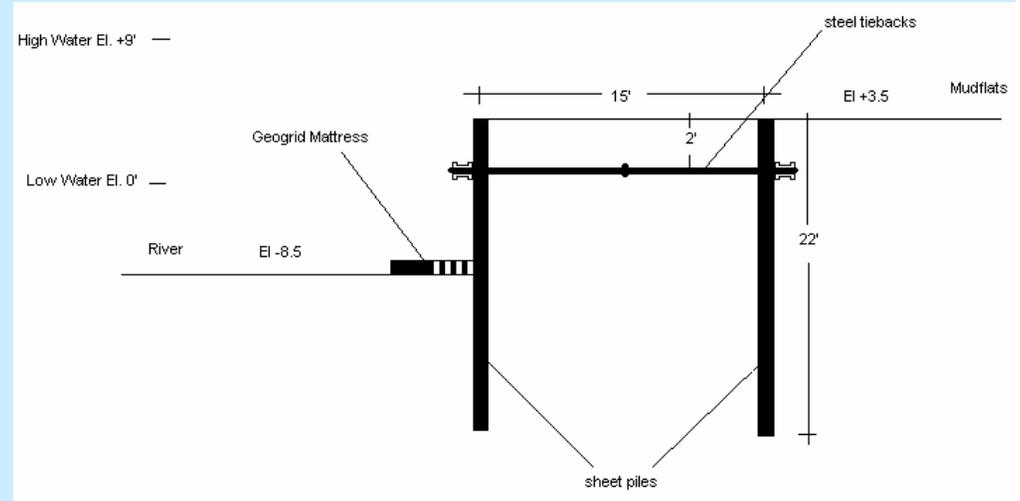


for use. In the meantime, vinyl sheet piling should not be used in applications where life safety and widespread property damage are at stake in the event of failure.



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- Selected Design for each of the two bulkhead
 - Double rows of sheets, FRP or heavy vinyl: No cantilever
 - Galvanized steel tiebacks and waler: Reliability
 - Single Waler: No diving (winter)
 - Scour protection: Protect toe
 - Drain holes: Reduce loads



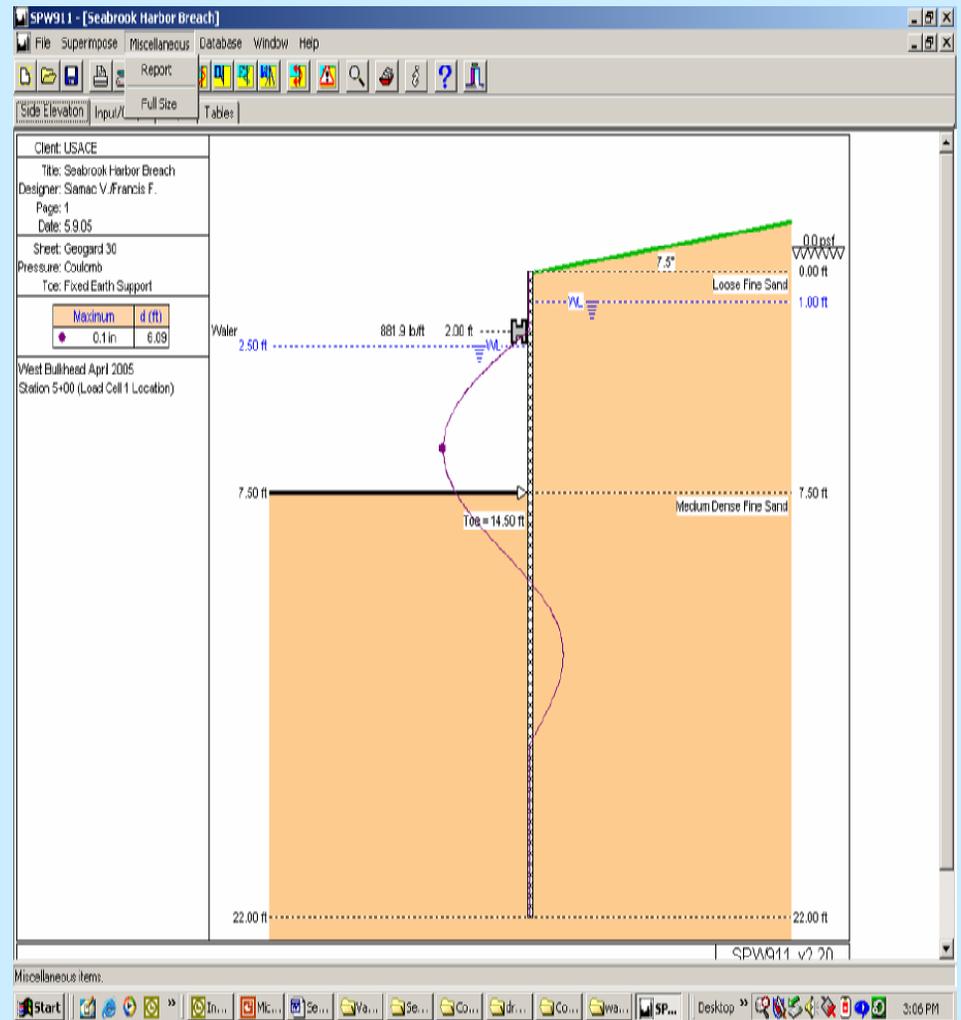
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Design Parameters

- 50-year low tide
- 50% drainage in fill
- 12' depth to mudline (22 feet sheet length)
- 2 tons horizontal load per linear foot
- Tiebacks 6' spacing
- 200 psf surcharge

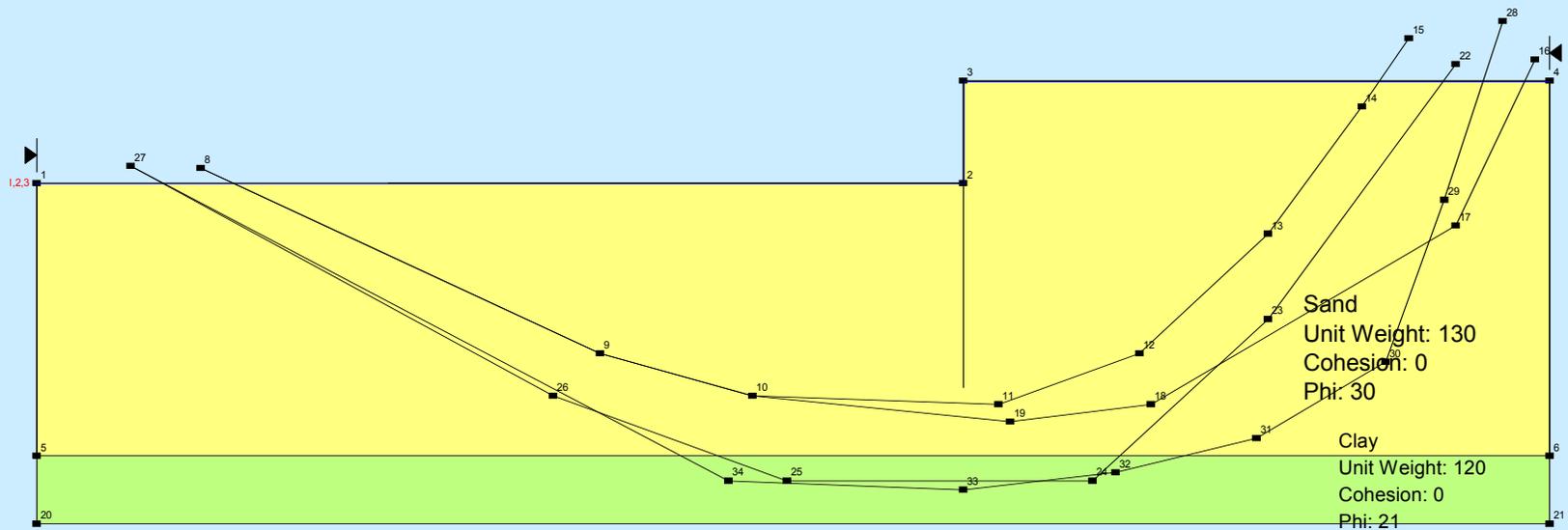


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Seabrook Harbor
Slope Stability Analysis
Analysis Method: Bishop (with Ordinary & Janbu)
Slip Surface Option: Fully Specified



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Component Details

- **Waler: 2 x 10” galvanized steel Channels on the outside**
- **Tiebacks: 18’ long, 2.25” galvanized steel tiebacks with turnbuckle, Oversized to allow for corrosion**
- **Drains: 2 x 2” dia holes with wire mesh/geotextile backing, located under water to prevent freezing**



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- Recent Examples Viewed
- Fiberglass



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- Recent Examples Viewed
- Vinyl



DESIGN AND CONSTRUCTION OF ANCHORED BULKHEADS WITH SYNTHETIC SHEET PILES, SEABROOK, NEW HAMPSHIRE

- **Construction**
 - **October 2004 – April 2005 (within the November-March dredging window)**
 - **Two barges, three cranes, clam shell, dozer, supply boats, Crew of 20**
 - **Hydraulic Dredge**
 - **Hydraulic vibratory hammer**
 - **Design called for vinyl or fiberglass; Contractor Submitted fiberglass sheeting with polyurethane resin (delivery and QC problems resulted in switch to different manufacturer and polyester resin)**
 - **Total length of two bulkheads = 1,700 feet**
 - **Sheet panel length = 27 feet (5 feet cut off to obtain required 22 feet)**
 - **Construction cost = \$3 million**



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| MATERIAL: FRP | | | | | | | | | | | |
|---------------------------|-------------------|-----------------|--------------|-----------------|------------------|------------------|-----------------------|----------------|-----------------|--------------------|------------------|
| WEST BULKHEAD - EAST WALL | | | | | | | | | | | |
| DATE DRIVEN | SHEET LOCATION | GROUND ELEV. | TIP ELEV. | SHEET LENGTH | DRIVEN LENGTH | CUTOFF LENGTH | DRIVING TIME H.M.S | VIBRO MODEL | VIBRO WEIGHT | VIBRO FREQUENCY | CUTOFF LENGTH |
| | 1100 | | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1097 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1094 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1091 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1088 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1085 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1082 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1079 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1076 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1073 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1070 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1067 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1064 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1061 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1058 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1055 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1052 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1049 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1046 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1043 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| | 1040 | 1.5 | -18.5 | 25' | | | 5 80 | 216 ICE | 5350 | | |
| 10/28/2004 | 1037 | 1.5 | -18.5 | 27 | | | 5 80 | 216 ICE | 5350 | | |
| 10/28/2004 | 1034 | 1.5 | -18.5 | 27 | | | 5 80 | 216 ICE | 5350 | | |
| 10/28/2004 | 1031 | 1.5 | -18.5 | 27 | | | 5 80 | 216 ICE | 5350 | | |
| 10/28/2004 | 1028 | 1.5 | -18.5 | 27 | | | 5 80 | 216 ICE | 5350 | | |
| 10/28/2004 | 1025 | 1.5 | -18.5 | 27 | | | 5 80 | 216 ICE | 5350 | | |
| 10/28/2004 | 1022 | 1.5 | -18.5 | 27 | | | 5 80 | 216 ICE | 5350 | | |
| 10/28/2004 | 1019 | 1.5 | -18.5 | 27 | | | 5 80 | 216 ICE | 5350 | | |
| 10/28/2004 | 1016 | 1.5 | -18.5 | 27 | | | 5 80 | 216 ICE | 5350 | | |
| 10/28/2004 | 1013 | 1.5 | -18.5 | 27 | | | 5 80 | 216 ICE | 5350 | | |
| 10/28/2004 | 1010 | 1.5 | -18.5 | 27 | | | 5 80 | 216 ICE | 5350 | | |
| 10/28/2004 | 1007 | 1.5 | -18.5 | 27 | | | 5 80 | 216 ICE | 5350 | | |

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Field Issues & Lessons Learned



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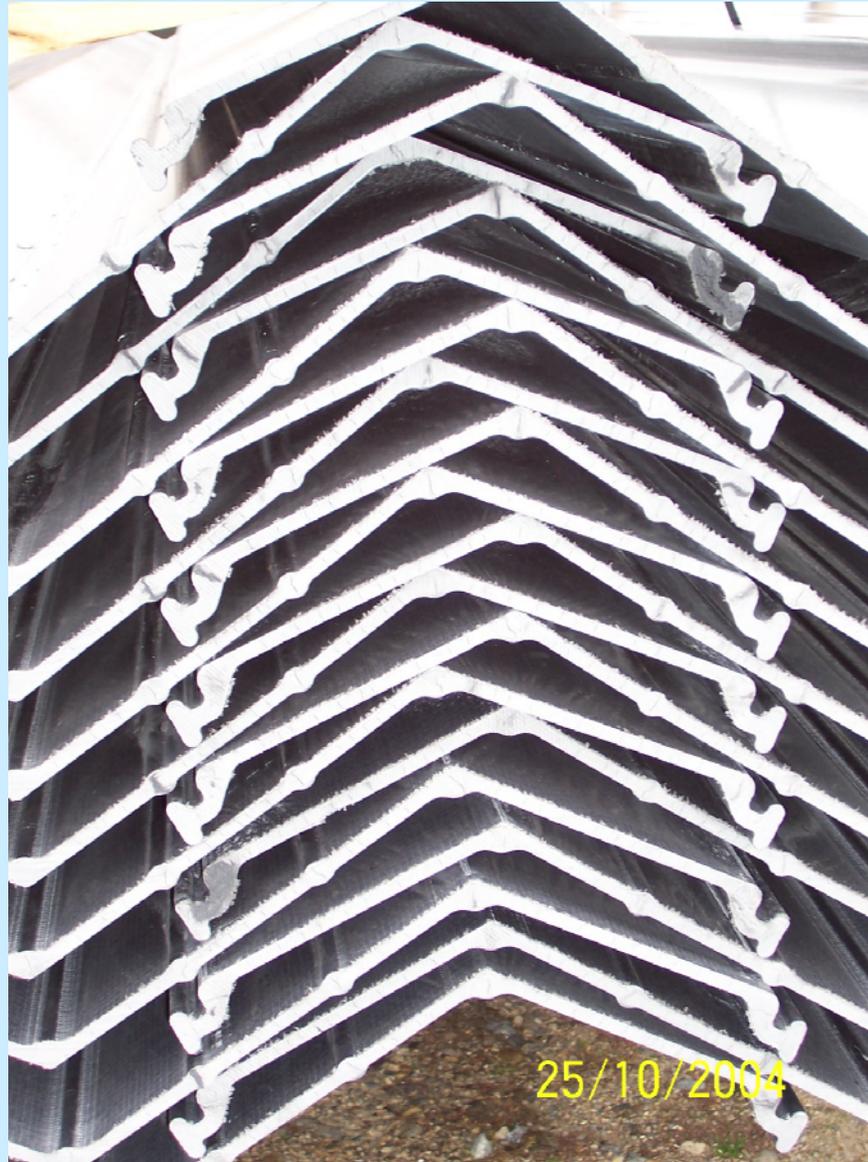
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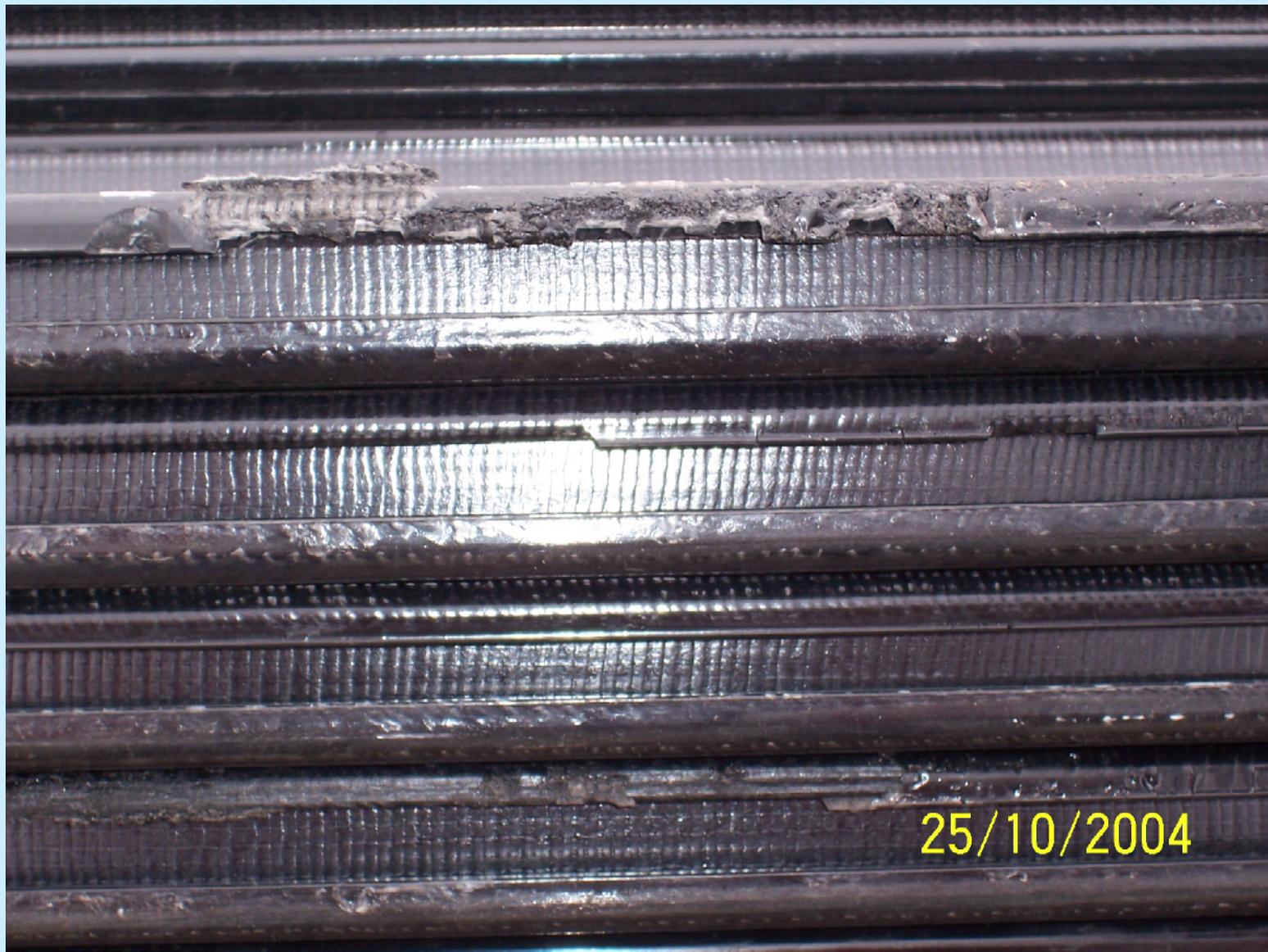
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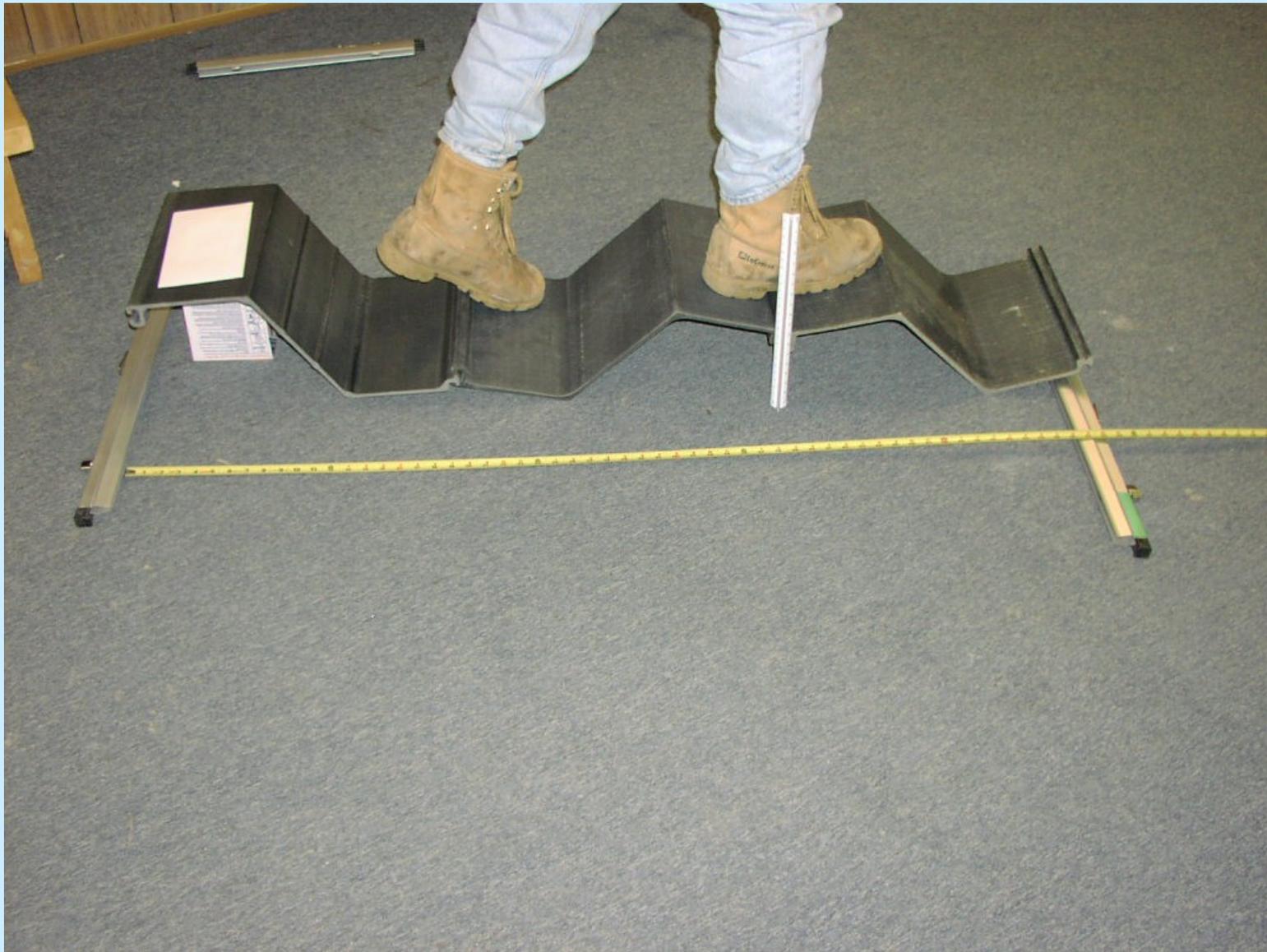
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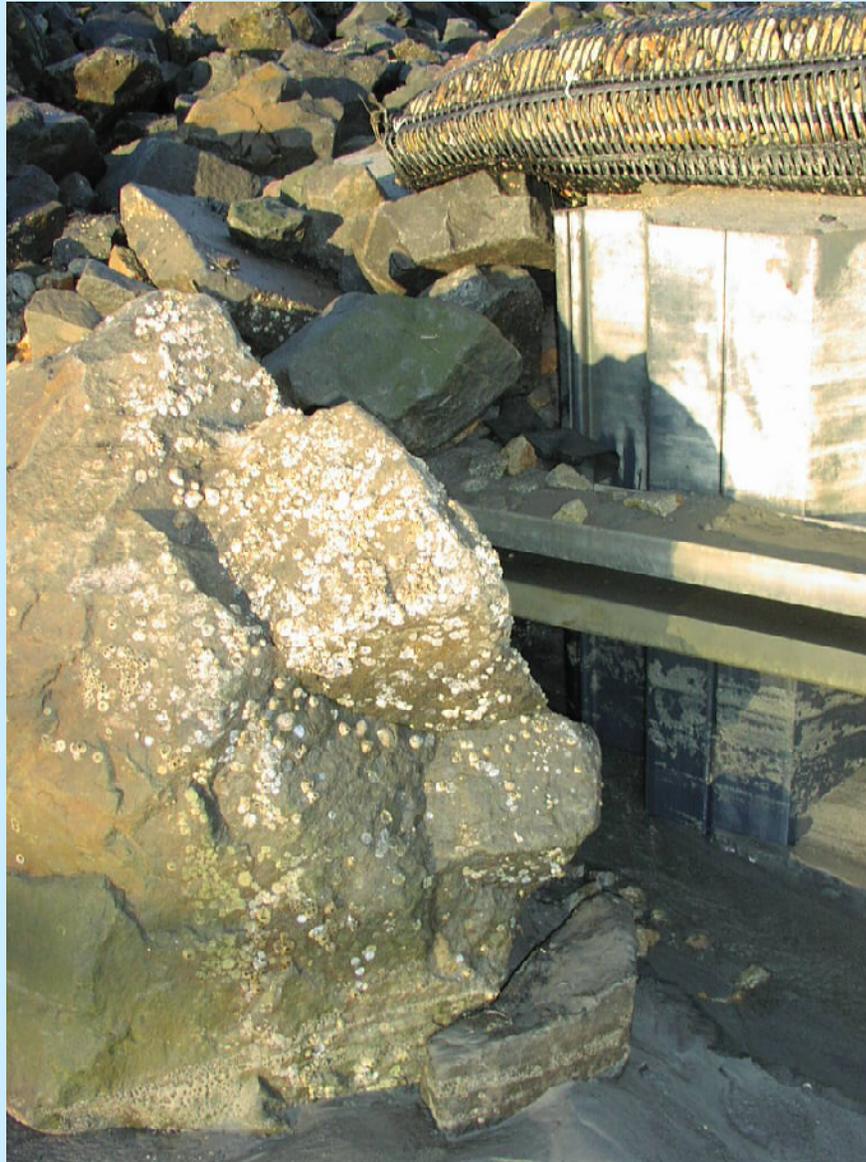
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Instrumentation



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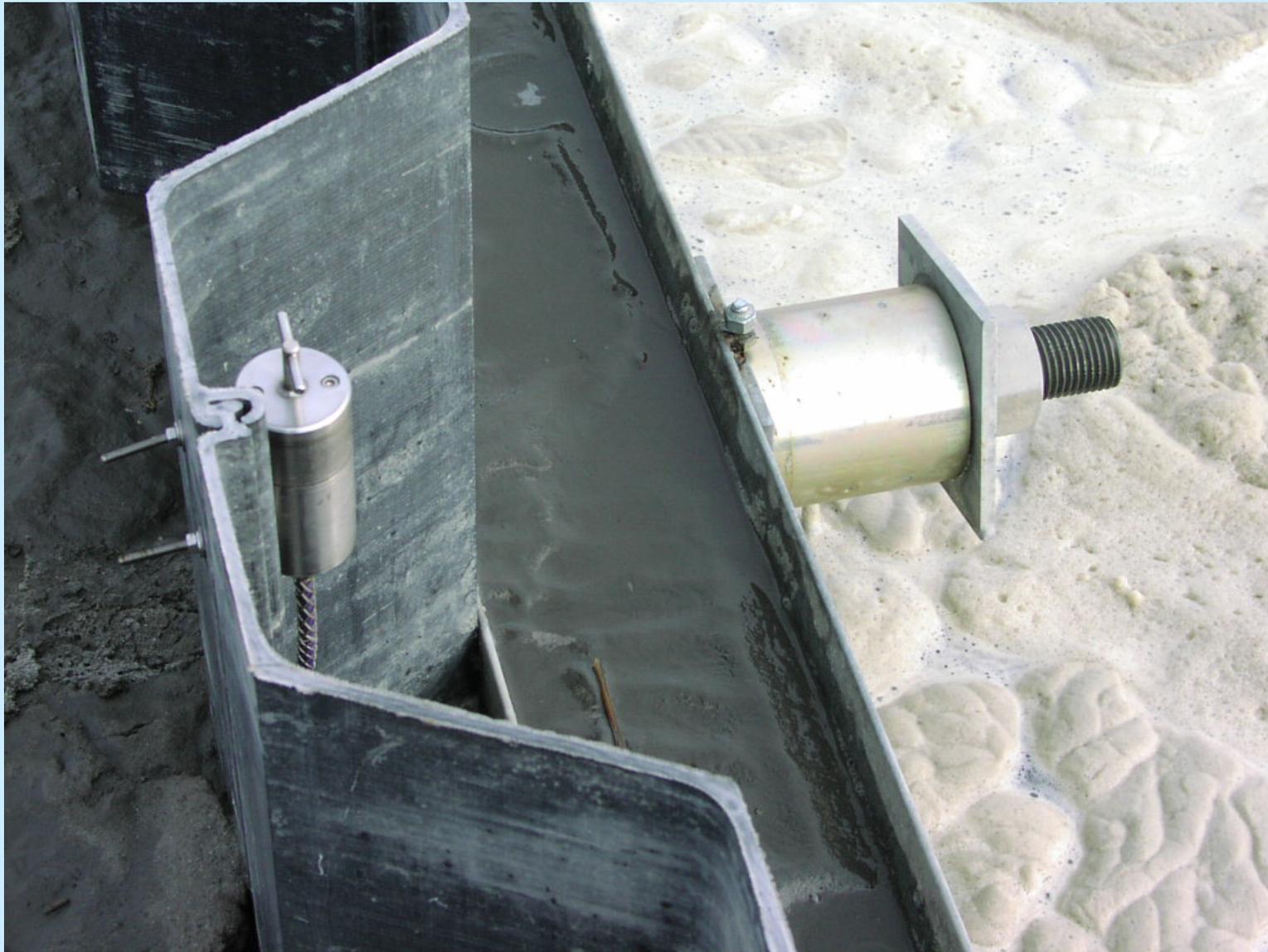
| Location Station | Date | Time | Well Reading | Well Level MLW | Tide Reading | Tide Level MLW | Delta (Well - Tide) |
|------------------|---------|------|--------------|----------------|--------------|----------------|---------------------|
| W4+00... | | | | | | | |
| 1 | 4/14/05 | 1049 | 42" | +1' 11" | 36" | +0' 6" | +1' 5" |
| 2 | 4/15/05 | 1000 | 30" | +2' 11" | 26.5" | +1' 3.5" | +1' 7.5" |
| 3 | 4/18/05 | 1317 | 34" | +2' 7" | 29.5" | +1' 0.5" | +1' 6.5" |
| 4A | 4/19/05 | 1335 | 29.5" | +2' 11.5" | 24.5" | +1' 5.5" | +1' 6" |
| 4B | 4/19/05 | 1440 | 36.5" | +2' 4.5" | 31.5" | +0' 10.5" | +1' 6" |
| 5 | 4/20/05 | 1451 | 33" | +2' 8" | 31.5" | +0' 10.5" | +1' 10.5" |
| 6 | 4/25/05 | 0659 | 38.5" | +2' 3" | 40.5" | +0' 1.5" | +2' 1.5" |



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Deformation Monitoring Log

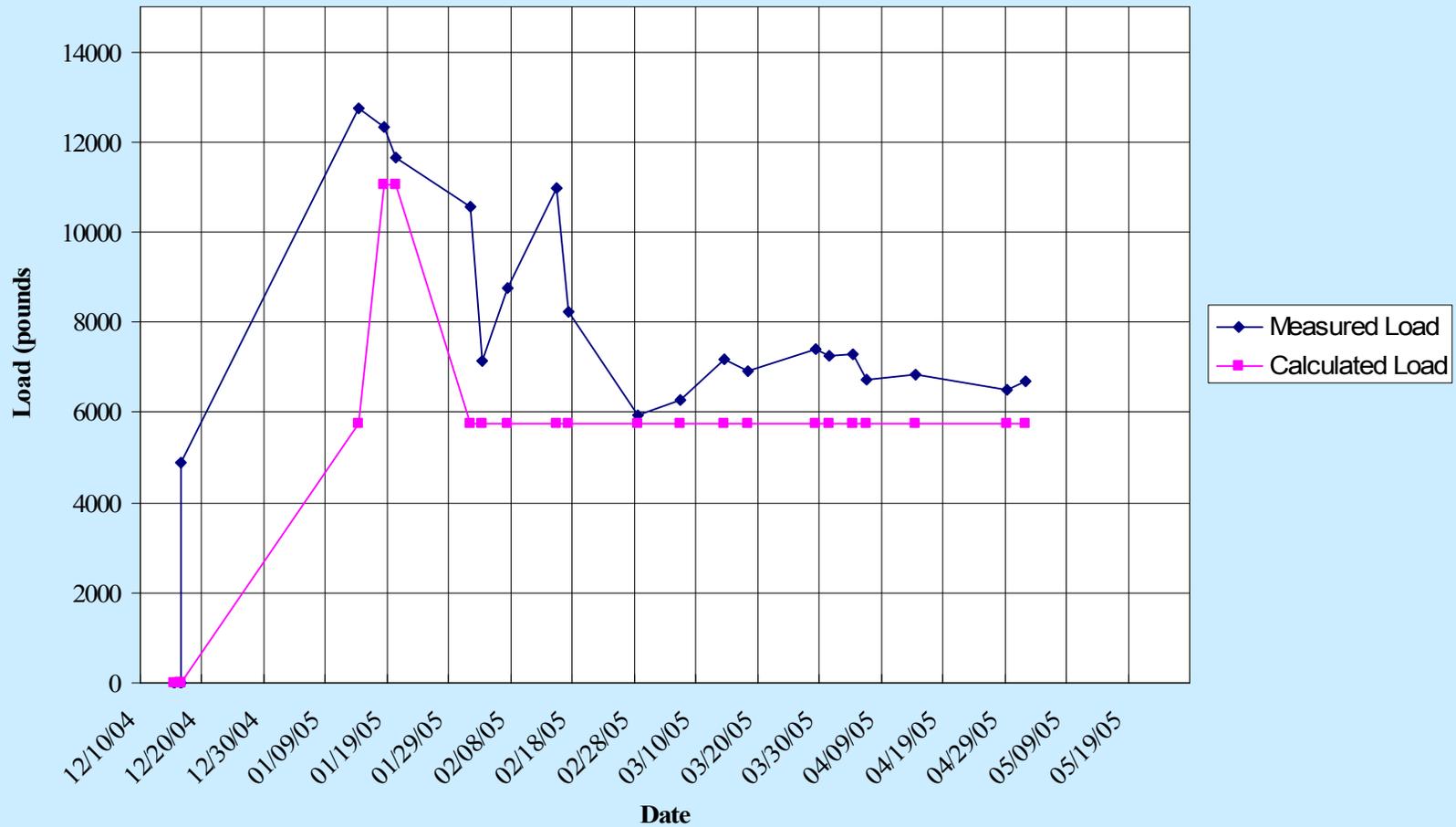
| Reading Number | Location | Direct Angle | Inverse Angle | Average Angle | Direct Distance | Inverse Distance | Average Distance | Elevation | Deformation From Initial Reading |
|---|----------|--------------|---------------|---------------|------------------------------|------------------|------------------|--------------|----------------------------------|
| | | | | | | | | Date: | 4/6/2005 |
| | | | | | | | | Time: | 2:30 PM |
| Project: Seabrook Harbor Section 227 Project | | | | | | | | Temp: | 58°F BP 30.24 |
| Contract No.: W912WJ-04-C-0009 | | | | | | | | Weather: | FAIR |
| | | | | | | | | Surveyed By: | W. Saucier |
| 1 | 1+38 E | 39°39'35" | 39°39'39" | 39°39'37" | 88.24 | 88.245 | 88.24 | 1.77 | E 0.069/N 0.00 |
| 2 | 1+38 E | 39°39'36" | 39°39'42" | 39°39'39" | 88.235 | 88.24 | 88.24 | 1.77 | E 0.068/N 0.00 |
| 3 | 1+38 E | 39°39'39" | 39°39'41" | 39°39'40" | 88.245 | 88.235 | 88.24 | 1.77 | E 0.068/N 0.00 |
| | | | | | | | | 0.02 | |
| | | | | | Change from initial (inches) | | | | 0.83 |
| 1 | 1+60 E | 39°34'54" | 39°35'00" | 39°34'57" | 110.025 | 110.035 | 110.03 | 1.82 | E 0.044/N 0.00 |
| 2 | 1+60 E | 39°34'55" | 39°34'57" | 39°34'56" | 110.03 | 110.03 | 110.03 | 1.82 | E 0.044/N 0.00 |
| 3 | 1+60 E | 39°35'00" | 39°34'54" | 39°34'57" | 110.035 | 110.03 | 110.03 | 1.82 | E 0.044/N 0.00 |
| | | | | | | | | 0 | |
| Comments | | | | | | | | | |
| Note: Initial Readings (1+38E 39°42'19" - 88.24 / 1+60E 39°36'19" - 110.03) | | | | | | | | | |
| Third reading on completed wall | | | | | | | | | |

DESIGN AND CONSTRUCTION OF ANCHORED BULKHEADS WITH SYNTHETIC SHEET PILES, SEABROOK, NEW HAMPSHIRE

SECTION

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Load Cell 2



DESIGN AND CONSTRUCTION OF ANCHORED BULKHEADS WITH SYNTHETIC SHEET PILES, SEABROOK, NEW HAMPSHIRE

- **Conclusions**
 - **Pick the right application. Despite some manufacturers' claims, steel it is not!**
 - **Synthetic sheeting can be very cost effective (50% of cost of steel is possible)**
 - **Conservatism in design is recommended because of scarcity of test data.**
 - **Construction sequence is crucial to avoid overstressing the material**
 - **Synthetic sheeting is here to stay**
- **Current Needs**
 - **Standard (full scale panel) test methods & corresponding data**
 - **Standard guide specifications**
 - **Long term performance data (longevity)**
 - **Greater number of quality manufacturers**
 - **Information exchange among designers (USACE, NAVY, Others)**
 - **A committee to facilitate the exchange and develop standards**



***DESIGN AND CONSTRUCTION OF ANCHORED BULKHEADS WITH
SYNTHETIC SHEET PILES, SEABROOK, NEW HAMPSHIRE***

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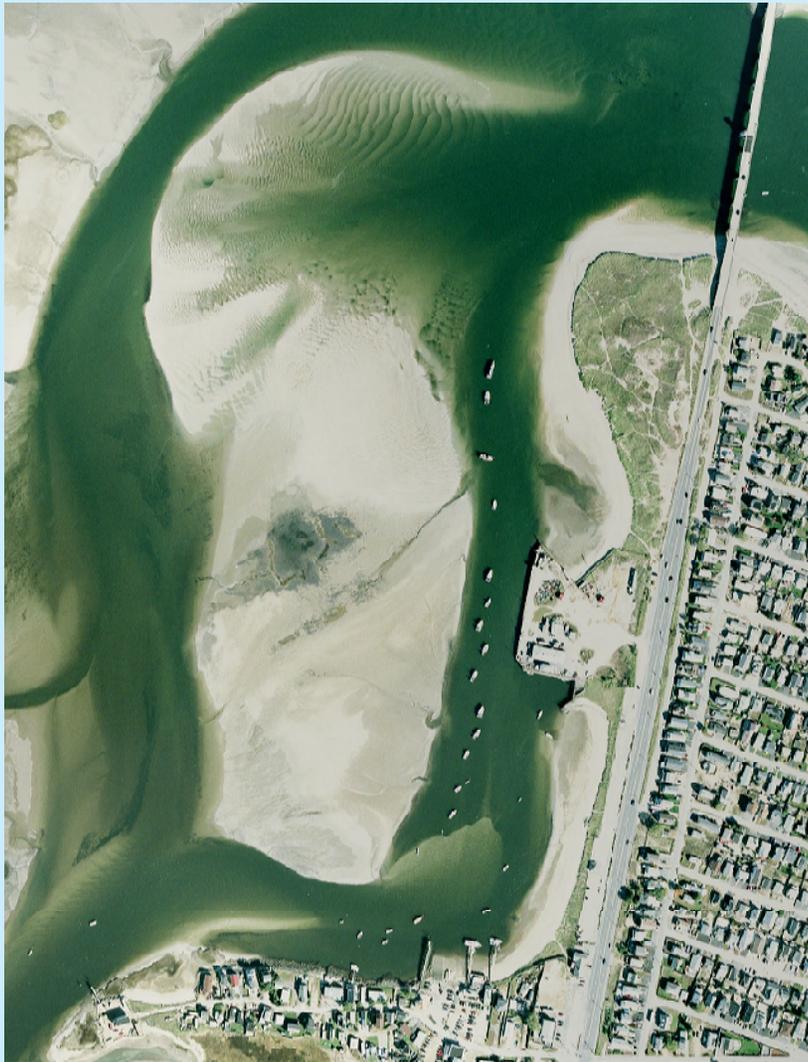
& our final product....



**DESIGN AND CONSTRUCTION OF ANCHORED BULKHEADS WITH
SYNTHETIC SHEET PILES, SEABROOK, NEW HAMPSHIRE**

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October 2004



April 2005



***DESIGN AND CONSTRUCTION OF ANCHORED
BULKHEADS WITH SYNTHETIC SHEET PILES
SEABROOK, NEW HAMPSHIRE***



Thank you

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