



# M789 LW 30mm HEDP Cartridge In-Bore Detonation Investigation



Presented By

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# Agenda



- 30mm Inbore/Hangfire Investigation
  - Apache M230 Weapon System Basic Information
  - Reported Problems
    - Total Incident Types / #'s & Groupings
    - Resultant Damage Examples
  - Investigation Team
  - Methodology Employed
  - Most Likely Causes & Actions Taken
  - Additional Recommendations
  - Summary



# Apache M230 Weapon System



- Aircraft System
  - Turret Mounted Weapon
  - Closed Loop Linkless Feed System
  - Weapon Mounted Uploader/Downloader; 'D' Model Aircraft have Additional Ammunition Sideloader
  - **First In/Last Out Ladder/Rail Magazine**
- M230 Weapon
  - **Externally Powered w/Electric Drive Motor**
  - Single Barrel, Chain Driven Automatic Cannon
  - 625 ± 25 Shots per Minute Firing Rate
- M789 High Explosive Dual Purpose Cartridge
  - **Aluminum Cartridge Case w/Electric Primer, IB52 Booster System & Double Base WC855 Ball<sup>®</sup> Powder**
  - High Strength 4130 Steel Projectile **w/PBXN-5 Explosive Fill**
  - Spin Compensated Shaped Charge Liner
  - Point Initiating, Base Detonating Nose Mounted Fuze



# Original Incident Classifications



- Hangfire – Ballistic functioning of the cartridge occurs outside of the dwell time of the weapon. Operating group & sometimes receiver damaged.
  - 23 Incidents since Aug 97
- Inbore Detonation – Premature initiation in the barrel under the barrel support shroud. Barrel bulges, sometimes ruptures.
  - 21 Incidents since Aug 97
- Severed Barrel – Premature initiation in the barrel near the muzzle. Muzzle is completely lost.
  - 2 Incidents Since Aug 97



# Typical Damage “Minor Event” - Hangfire





# Typical Damage "Severe Event"- Hangfire





# Typical Damage Inbore Detonation



- Damage Similar to or Identical to Severe Hangfire/High Pressure Plus Barrel Cracking & Muzzle Break Impacts by Fragments



Typical



Extreme



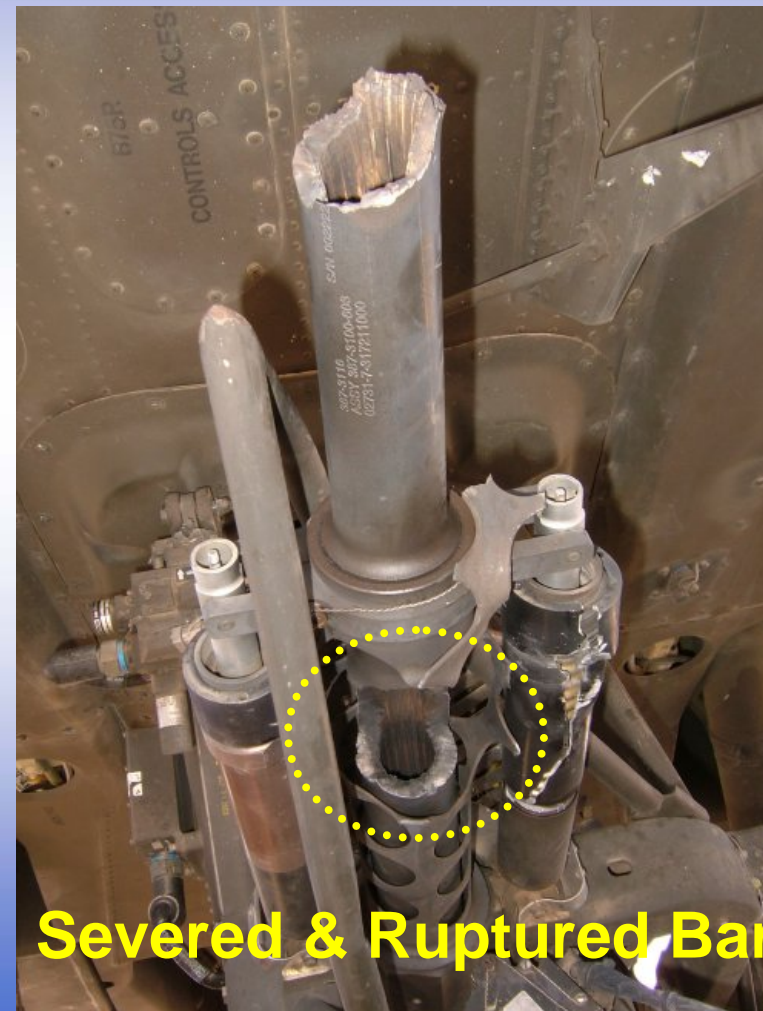


# Typical Damage Bullet on Bullet



Severed Barrel

1/130th



Severed & Ruptured Barrel

2/101st

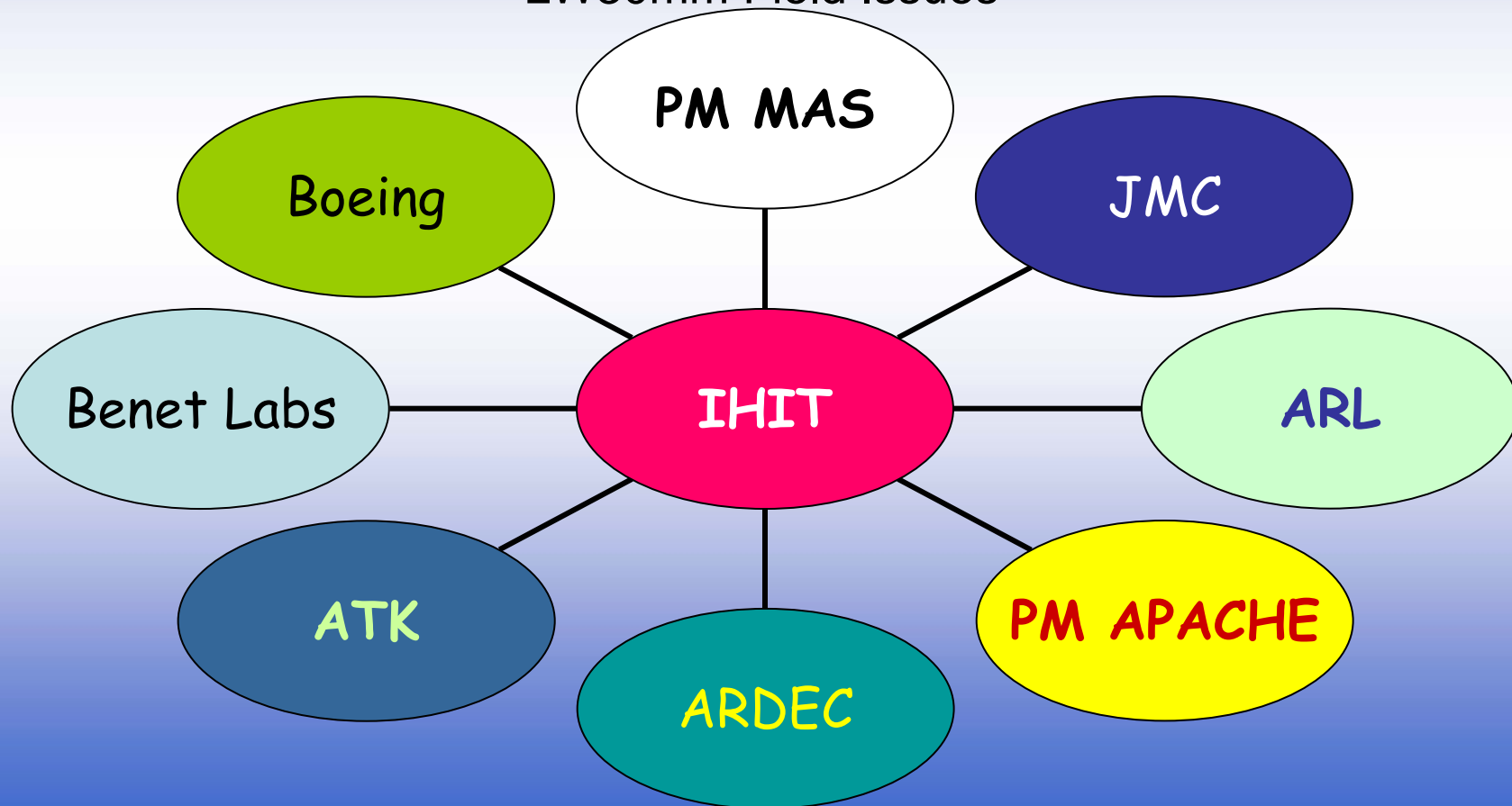




# In-Bore/Hang-fire Investigation Team Participation



In-Bore/Hang-fire Investigation Team Encompasses Elements From Across Area Weapon System, and is a Total System Approach to Solving LW30mm Field Issues





# IHIT Methodology



- Team Used A System Engineering And Six Sigma Approach
  - Interviews w/Field Units (Shooters, Ground Crews, Supply)
  - Re-work Previous Root Cause Analysis for Inbore Detonations
  - Use Failure Mode Effects Analysis (FMEA) Process
  - Collect Data (Modeling, Simulation, Testing) To Fill Data Gaps & Populate Fault Tree For Each Failure Mode
  - Conduct Design Of Experiments (DOE) And Verification Testing
  - Incorporate Changes Into TDP



# UNIT VISIT & INCIDENT KEY INFORMATION



- No Incident Resulted from the 1st Round Fired
- Ammo Usually Stays in A/C Until Scheduled Phase Maintenance - Some Units Reloaded in Reverse Order of Download
- Manual Mode for Sideloaders & Uploader/Downloader are Still Used Infrequently
- Feed System Jams While Uploading are Still Occurring Resulting in Punctured Cartridge Cases



# A Total System Approach



**Cannon, Handling System & Aircraft Systems**  
**121 Potential Causes**

- Cross Functional/Cross Organizational IPT
- Co-Leaders from PM-MAS & PM-Apache
- User Involvement & Feedback
- Systems Engineering

**Ammunition Handling & Storage**  
**3 Potential Causes**



**215 Total Potential Failure Modes Identified**



**Six Sigma Tools:**

- Continuous Black Belt Consultation
- Failure Modes Effect Analysis
- Fault Tree Analysis
- Design of Experiments

**Ammo Metal Parts Manufacture**  
**55 Potential Causes**

**Ammunition LAP**  
**36 Potential Causes**



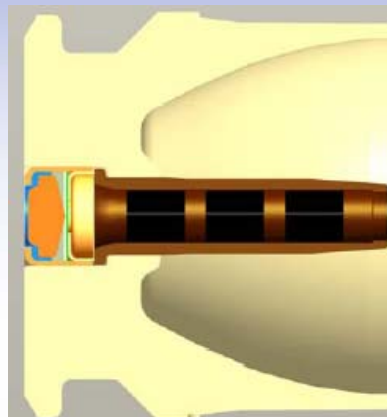
**Identified Three Major Root Causes**



# Hangfire/High Pressure



# Ignition System DOE Phase I

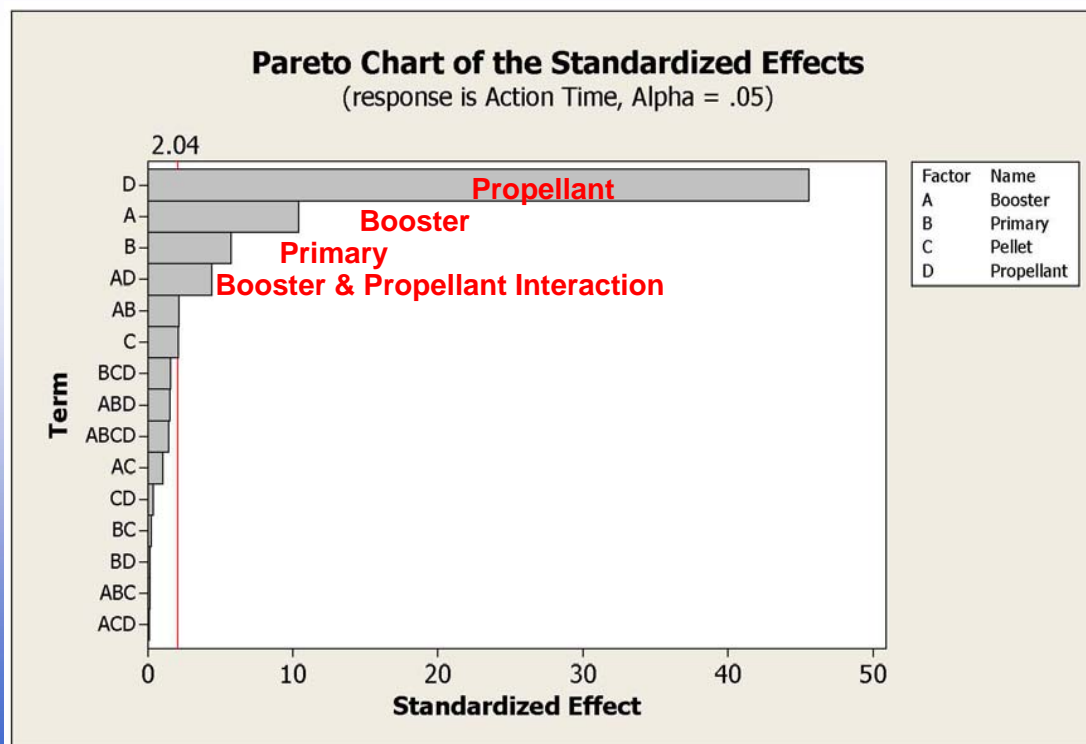


| Control Factors   | Level 1 | Level 2 | Level 3 |
|-------------------|---------|---------|---------|
| Booster Mix       | 100%    | 50%     |         |
| Primary Charge    | With    | Without |         |
| Flashtube Pellets | Pellet  | Powder  |         |
| Propellant Level  | 100%    | 50%     | 25%     |

**MANN BARREL TEST**



**Mann Barrel**





# Damaged IB52 Pellets/Flash Tube



Open Air  
High-Speed  
Video of  
Flash Tube  
Venting

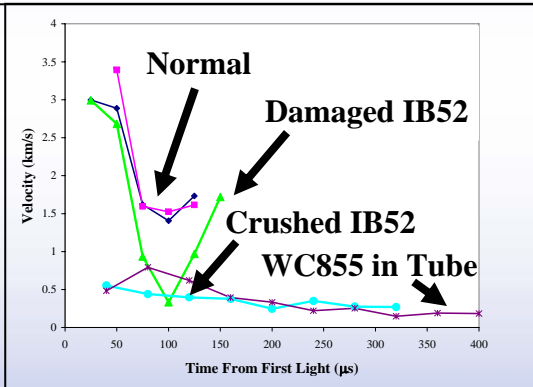
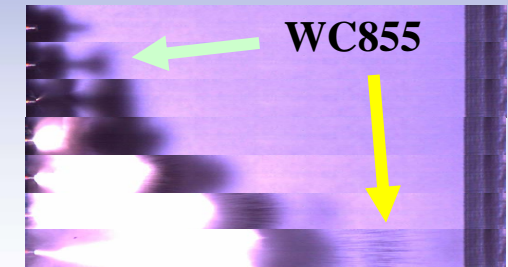
Normal Flash Tube



Damaged IB52

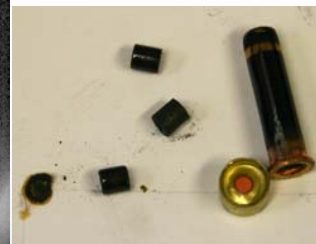
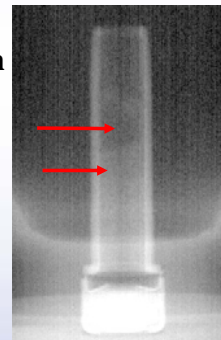


WC855 in Tube

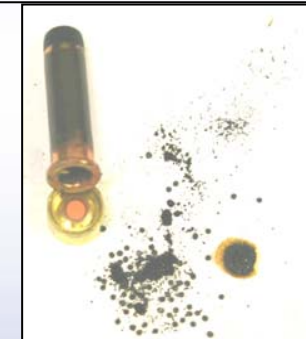


Gas Velocity From Flash Tube

Radiograph  
Damaged  
Flash Tube  
in M789



Some Damage IB52 Pellets

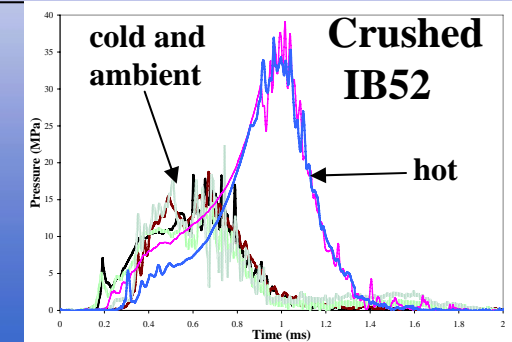
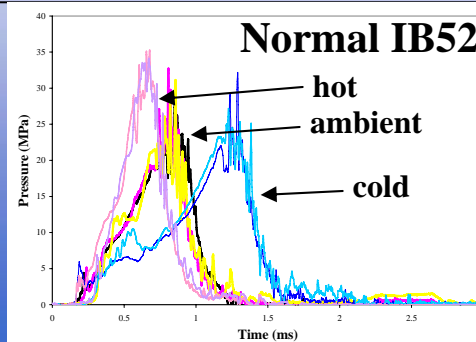


Broken Lacquer Seal with  
WC855 in Tube

Live Propellant 30-mm Gun Simulator



WC855 in Flash  
Tube has Given  
Greater Than  
40 ms Ignition  
Delay

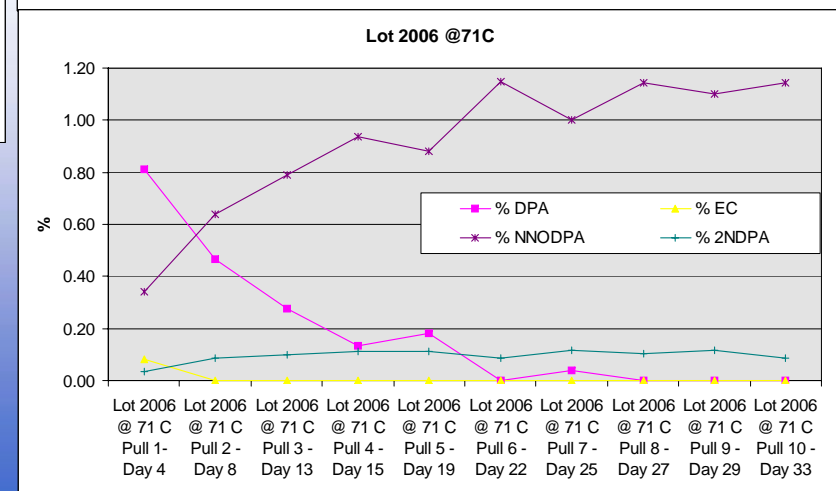
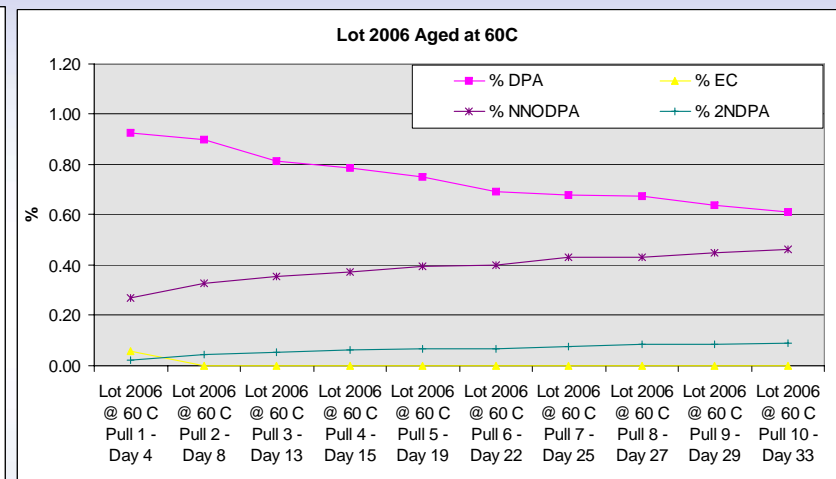
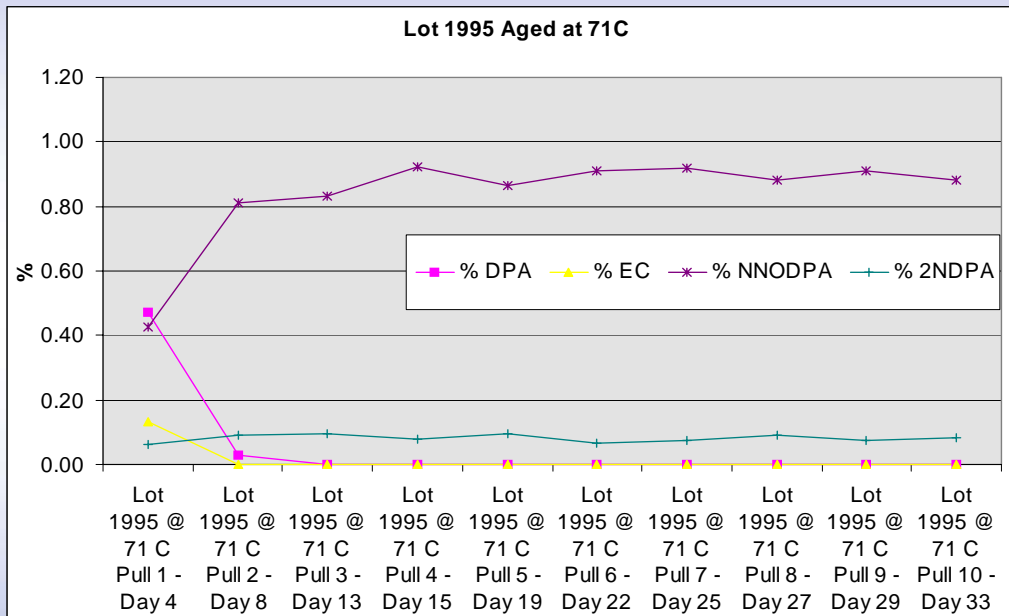




# Hot Temperature Storage Led to DPA Depletion



- Over time, the original stabilizer, DPA, depletes and converts to daughter products – 2NDPA, NNODPA ; DPA reaction rate increases as temperature increases



•DPA concentration of the 1995 Lot had depleted to half the concentration of the 2006 Lot at time = 0

•AT 71°C, DPA concentration depleted to 0 within 22 days of storage

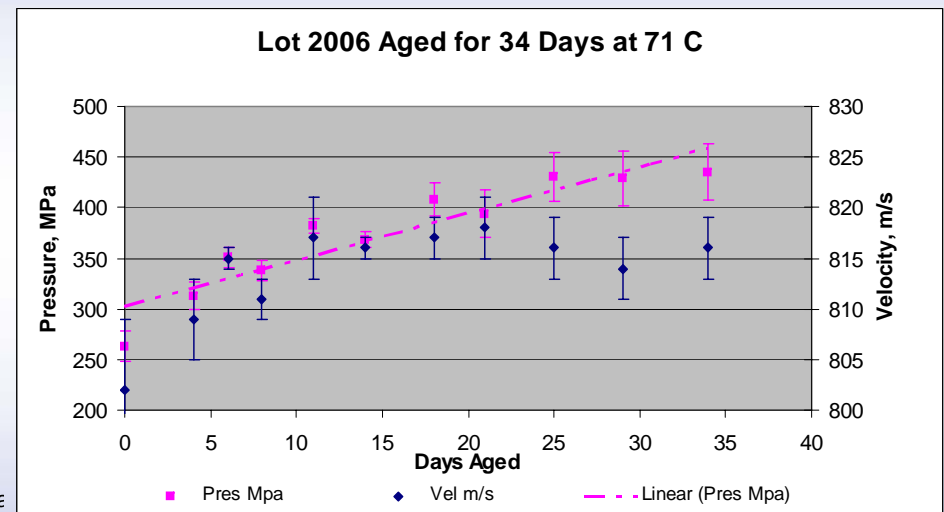
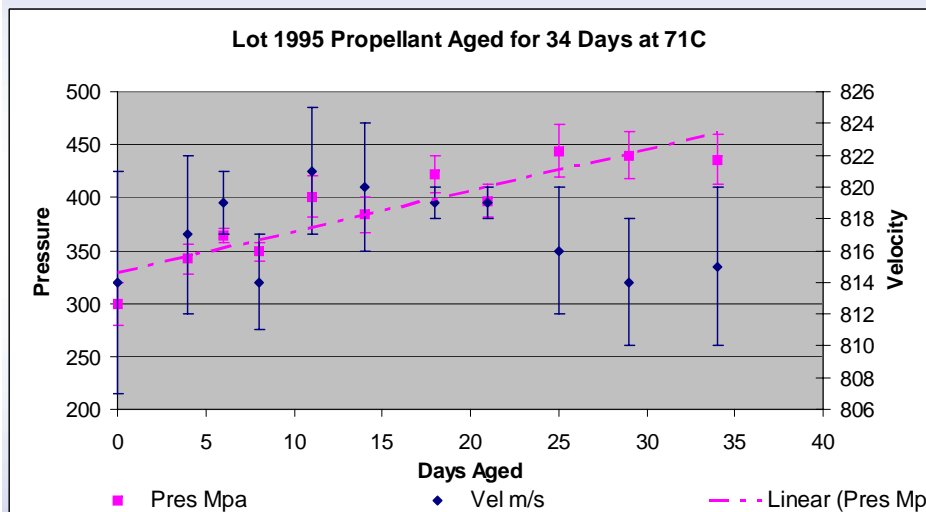




# Ballistic Pressure Increases With Days Aged



- Within 10 days of aging a new propellant lot at 71°C, the measured pressure was in excess of the upper specification limit of 335 MPa



- Ballistic testing conducted at ambient. All data corrected with reference ammunition. Data is the average of 5 shots.

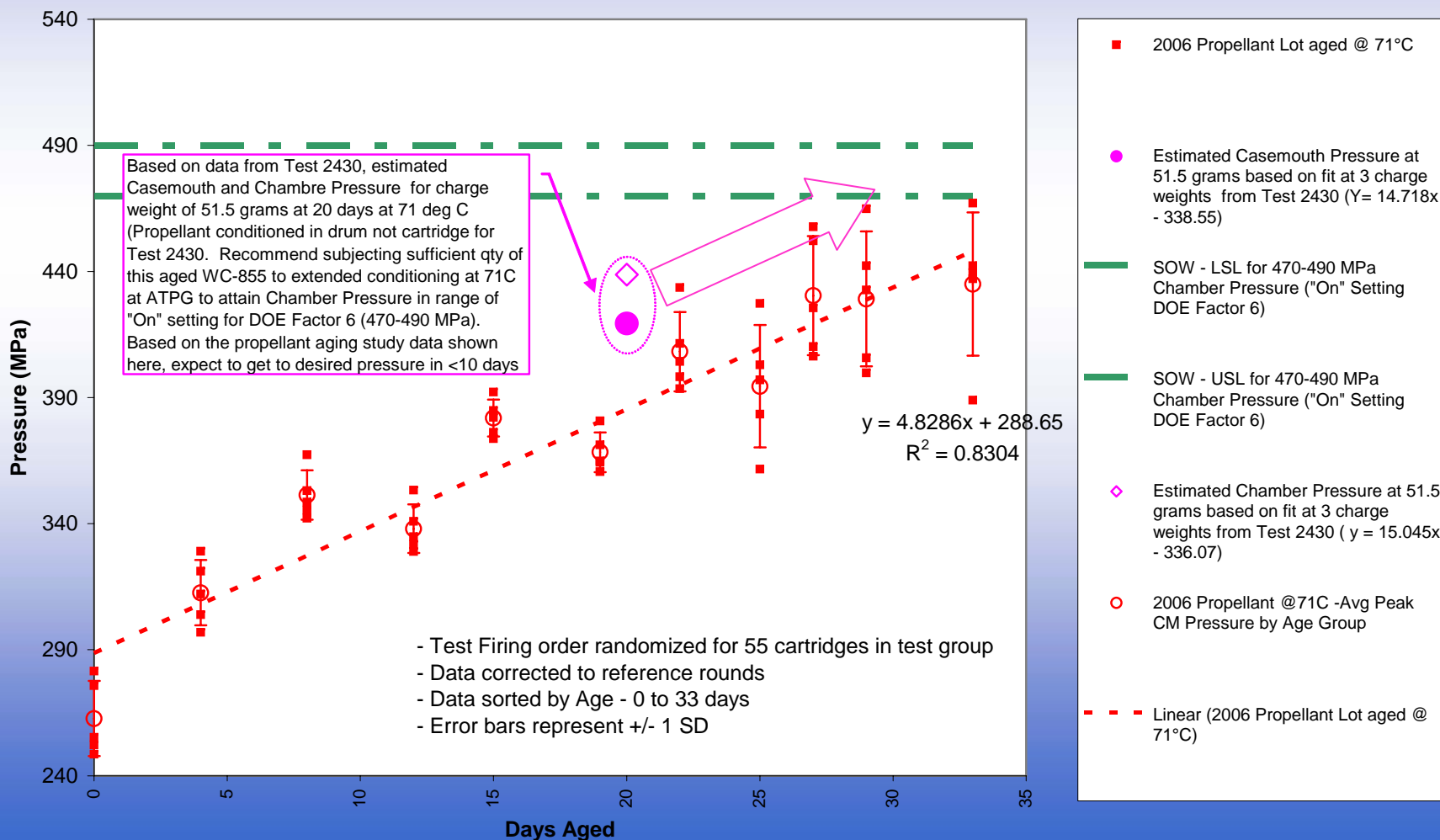
- Variation in pressure performance attributed to migration of DBP deterrent



# Aged WC-855 for DOE Factor 6



Casemouth Pressure vs Days Aged - 2006 Propellant Lots Conditioned at 71 deg C  
 (Test RFAAP 07-004 & 005)  
 IHIT Propellant Aging Study - Ballistic Testing at Radford 4-5 January 2007





# Headspace DOE



## Phase I Test Matrix

| Firing Order of Rounds | No. of Rounds | High Pressure (approx 500 Mpa) | Nominal Pressure | Nominal Headspace | Headspace 0.025" | Headspace 0.031" | Hot Barrel (180°F) | Ambient Barrel |
|------------------------|---------------|--------------------------------|------------------|-------------------|------------------|------------------|--------------------|----------------|
| 1                      | 5             |                                | X                | X                 |                  |                  |                    | X              |
| 2                      | 5             | X                              |                  | X                 |                  |                  |                    | X              |
| 3                      | 5             | X                              |                  |                   | X                |                  |                    | X              |
| 4                      | 5             | X                              |                  |                   |                  | X                |                    | X              |
| 5                      | 5             |                                | X                |                   | X                |                  | X                  |                |
| 6                      | 5             |                                | X                |                   |                  | X                | X                  |                |
| 7                      | 5             | X                              |                  |                   | X                |                  | X                  |                |
| 8                      | 5             | X                              |                  |                   |                  | X                | X                  |                |

Tested ok

Incident 1

Incident 2

## Phase II Test Matrix

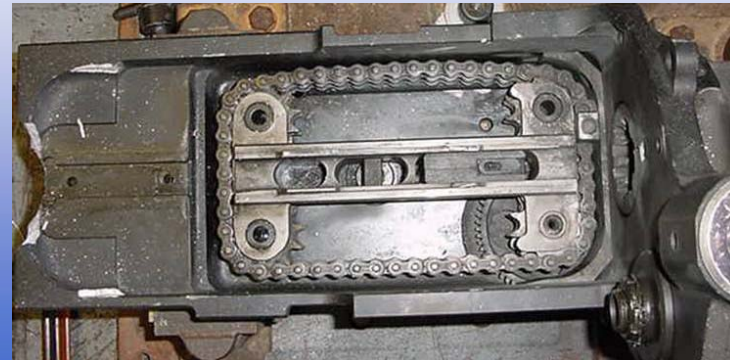
| Firing Order of Rounds | No. of Rounds | High Pressure (approx 415 Mpa) | Nominal Headspace (.022") | Maximum Headspace (0.031") | Ambient Barrel |
|------------------------|---------------|--------------------------------|---------------------------|----------------------------|----------------|
| 1                      | 5             | X                              | X                         |                            | X              |
| 2                      | 5             | X                              |                           | X                          | X              |



# Headspace DOE



- Hangfire signature has been replicated without an actual hangfire event.
    - Excessive headspace
    - Elevated pressure (~ 500 Mpa)
    - Hot barrel
  - Propellant gases vented from the chamber area can damage the operating group and receiver.
  - Damage created similar to that seen in HE-Inbore events, except no barrel bulge and generally no Blast Suppressor damage.
- Not all “hangfires signatures” are necessarily actual hangfires.**





# Hangfire/High Pressure



- Most Likely Causes
  - ★ Extended Vibration Damages Cartridge Ignition System (Replicated)
    - No Rounds Showed Physical Damage After 144 Hours
    - 30% Showed Some Damage After 192 Hours
  - ★ Extended High Temperature Exposure Changes Propellant Characteristics (Replicated)
    - Significant Pressures Measured after 432 Hours @ 71° C (160° F)
  - ★ Cartridge Cases are Punctured and Propellant is Lost or Contaminated (Replicated)
- Actions Taken to Date to Reduce/Eliminate Issues
  - 1980s Production Placed into Condition Code 'N'
    - Removed to Strategic Reserve in Kuwait, Planned for Demilitarization When Stockpile has been Replenished
  - Aviation Safety Action Message (ASAM) and AIN issued
    - Requires Download and Inspection of Ammo at Aircraft Regularly Scheduled Maintenance
    - Requires Rotation of Ammo When Reloaded into Aircraft to Minimize Prolonged Exposure to Vibration and Extreme Temperatures
  - Initiated Design Improvement Program to Improve Robustness of the Ignition Train



# Inbore Detonation



# Explosive Reaction and Response



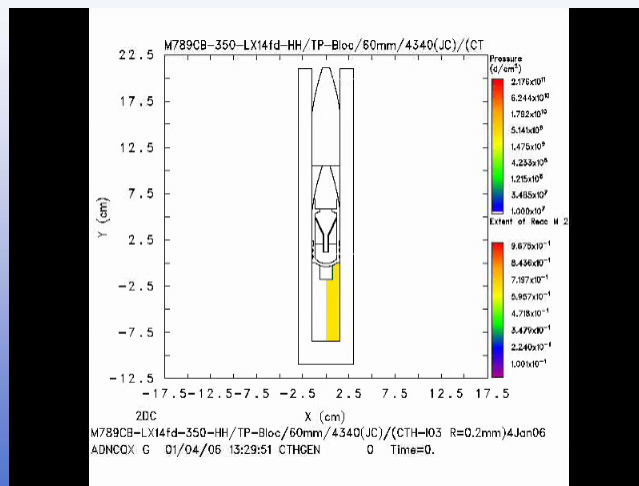
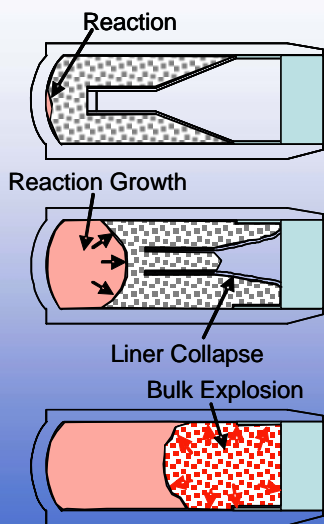
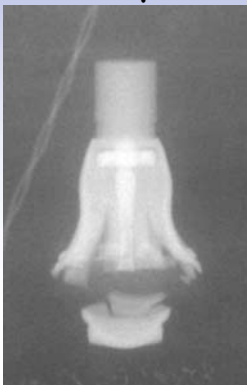
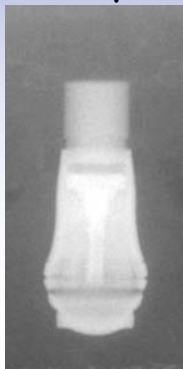
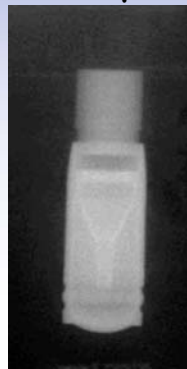
## Low Order Time Lines

35  $\mu$ s

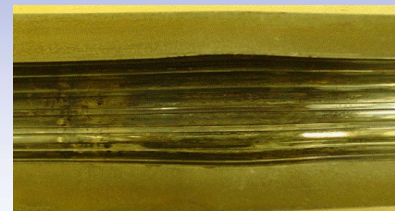
55  $\mu$ s

75  $\mu$ s

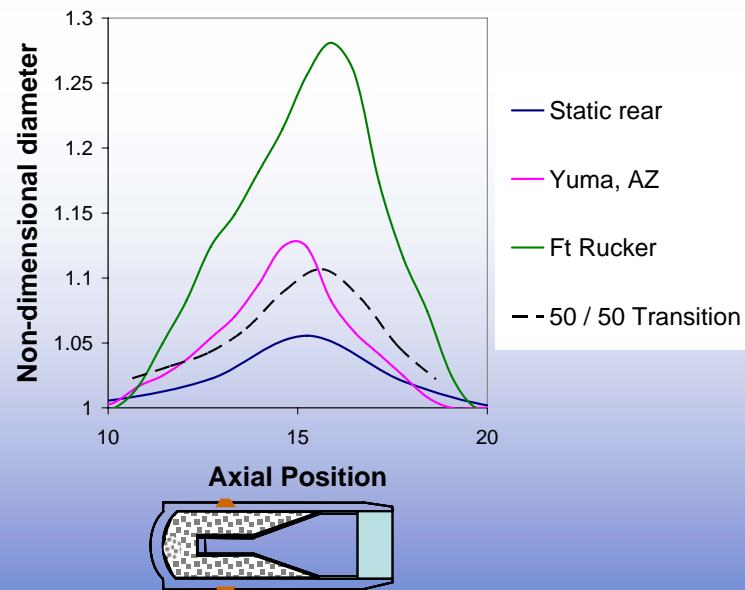
100  $\mu$ s



Barrel from Arizona Incident



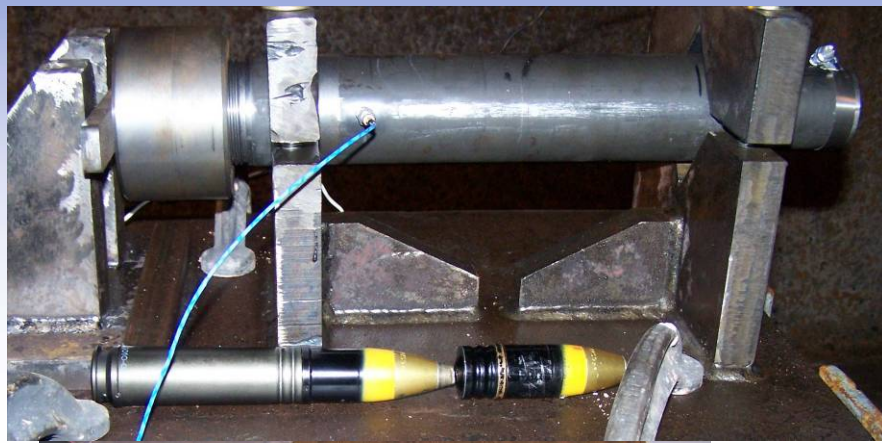
Data from Incidents, Experiment and Modeling



Signature matches an initiation at rear of warhead



# Dynamic Signature Replication Bullet-on-Bullet

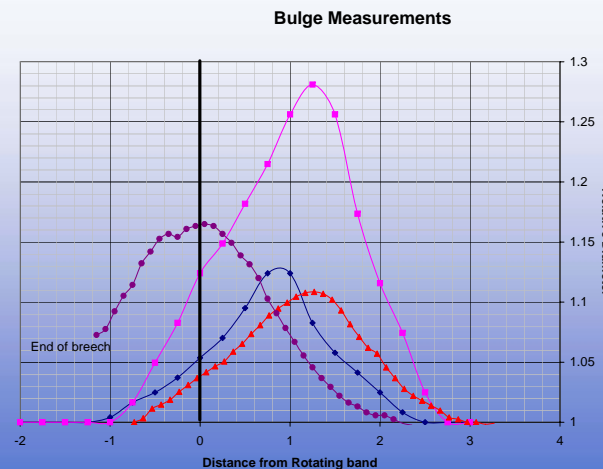


Violence and location reveal that bullet on bullet scenario not likely scenario for bulge...

Tests conducted:

- HE round → HE round (3 times)
- HE round → HE round (dummy fuze)
- HE round → TP round

Implies rear bullet initiation

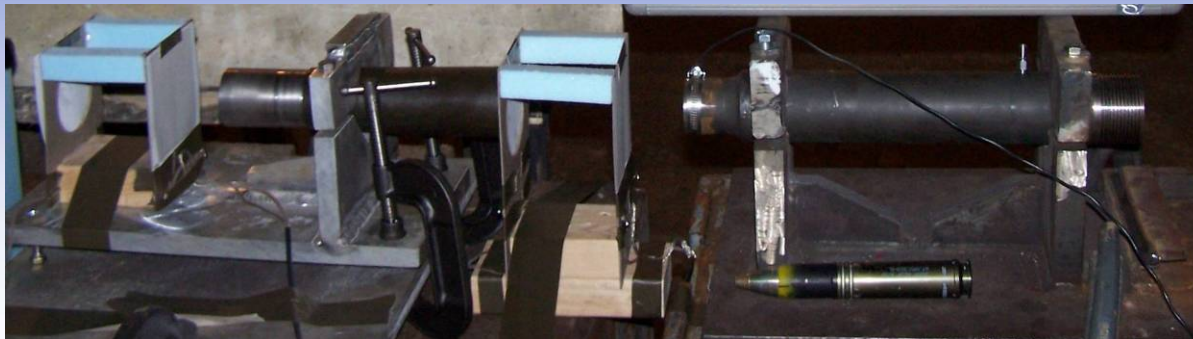


Follow-on shot with solid fuze result was an in-bore with incorrect signature

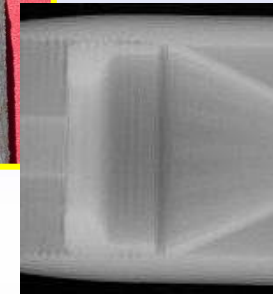




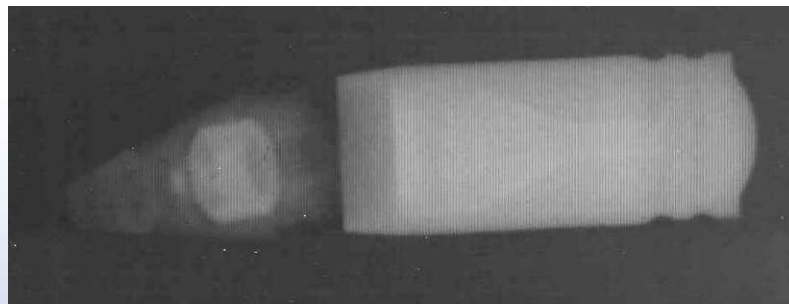
# Dynamic Signature Replication Set Forward



Exuded explosive in threads



Gap between retainer and liner



Result is g-load on order of  $10^3$ - $10^5$  with no reaction of projectile (Fuze ripped off body)

## Liner / Retainer gaps

- Gap > 0.032 in (from x-ray)
- Defuzed
- 8 shots, no in-bores

## Fuzed

- No defects as determined from x-ray
- Standard, fuzed rounds
- 5 shots, no in-bores



# Dynamic Signature Replication High Pressure (Body Failure)



2.00 x

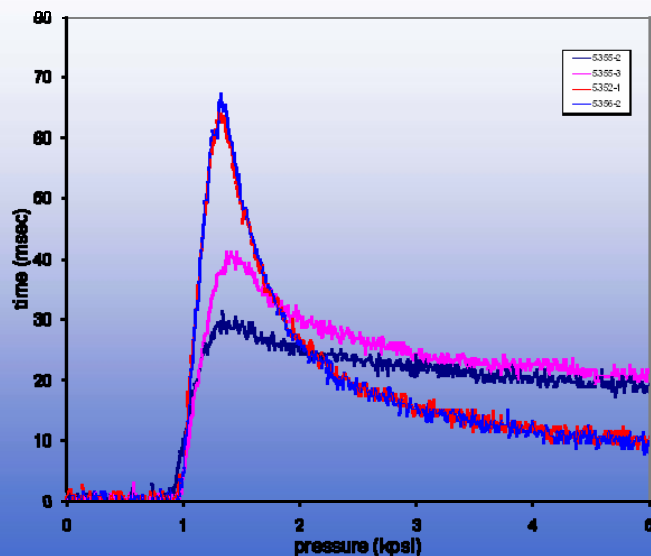


## Rationale

- Structural analysis found weak area in rear
- Bullet-on-bullet tests at APG:
  - 4 out of 4 shots went low order
  - Initiation from rear of projectile

## Procedure

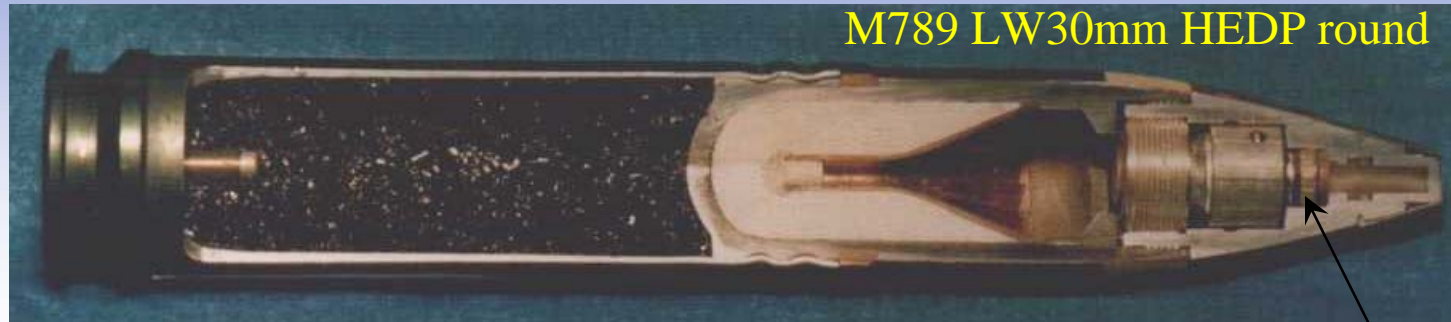
- Single projectile of increased mass
- Replace fuse with tungsten weight
- Provide data for fracture model



**Mass taken to over double (2.25x) of  
projectile with subsequent increase of  
base pressure – NO initiation of  
explosive**



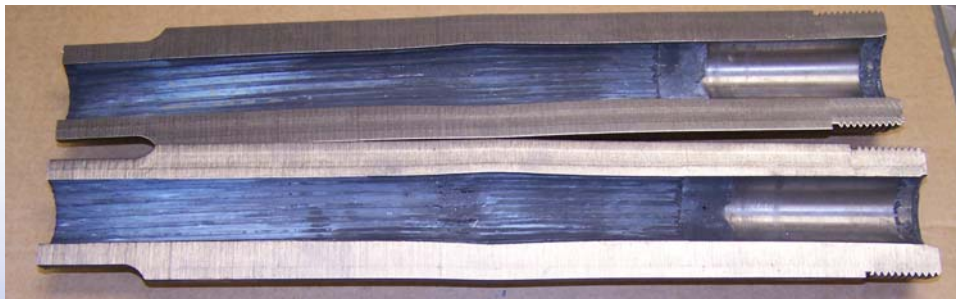
# Dynamic Signature Replication Foreign Material (aka Putty)



M789 LW30mm HEDP round

Shot 1

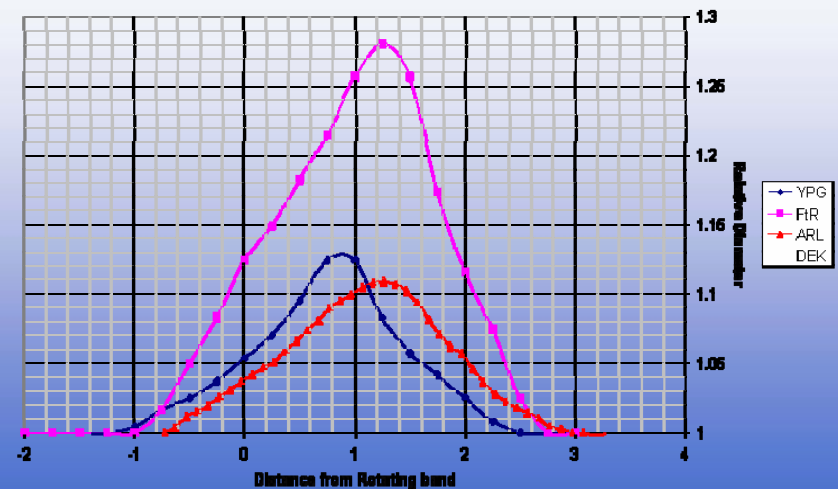
Dummy fuze replaces live fuze (with putty to match mass)



Bulged barrel centered at < 8 inches from breech

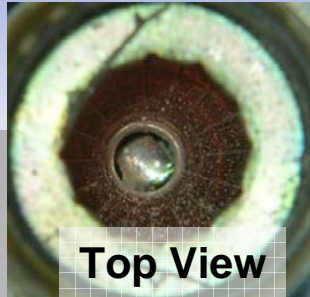


Bulge Measurements

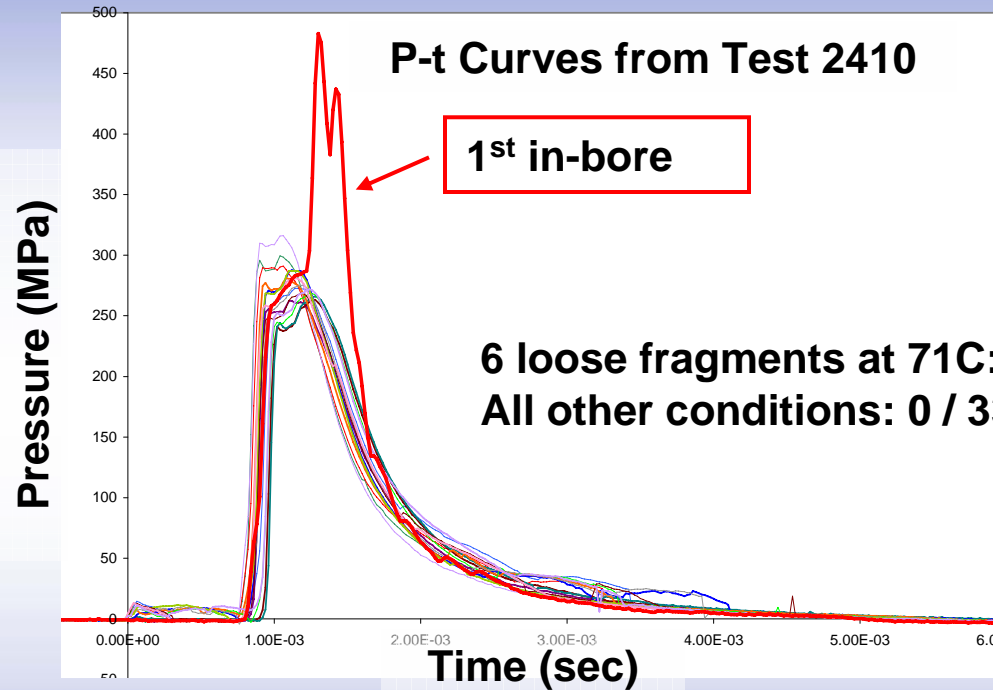
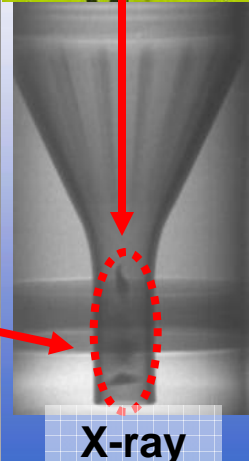




# Foreign Material in Liner Cavity

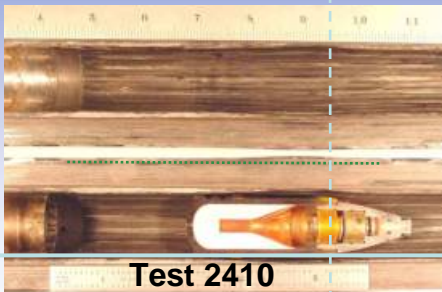


| Sample AA |           |
|-----------|-----------|
| Fragment  | Mass (mg) |
| 1         | 48        |
| 2         | 51        |
| 3         | 53        |
| 4         | 54        |
| 5         | 53        |
| 6         | 52        |
| Average   | 51.8      |
| Total     | 311       |





# Test vs. Field Incidents - Profile



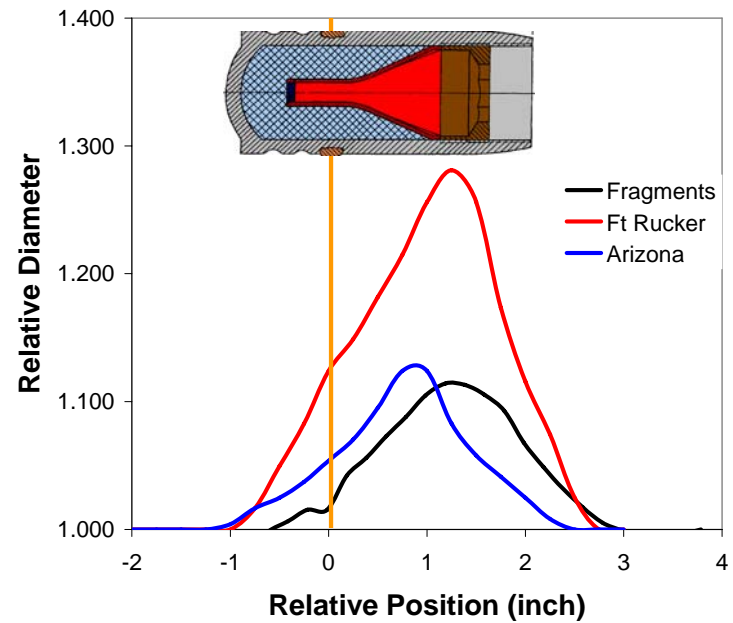
Test 2410



Ft. Rucker Barrel



Arizona Barrel



Reference Line approx. 9.5" from end of barrel



# Fault Tree Probabilities for In-Bore DOE Factors



| Block   | Reliability | Prob. of Failure |       | Final Probability | Priority Ranking |                                      |
|---|-------------|------------------|-------|-------------------|------------------|--------------------------------------|
| #504 Setback initiation due to debris in cavity               | 1           | 1.0005E-05       | A1.11 | 1.0005E-05        |                  | In-bore demonstrated in Test 2410    |
| #65 Thin sidewall body fails on setback                       | 1           | 7.8400E-07       | A1.12 | 7.8399E-07        | 1                | Factor 4                             |
| #502 Particles embedded in HE cause HE to initiate at setback | 1           | 5.0000E-07       | A1.15 | 4.9999E-07        | 2                | Cu shaving test at High P in DOE SOW |
| Normal projectile ?   | 0.9914      | 9.9137E-01       | A2.1  | 4.5107E-08        | 3                |                                      |
| #504 Setback initiation due to debris in cavity               | 0.9999      | 1.0000E-04       | A2.11 | 1.6300E-09        | 4                |                                      |
| #1 Thin BCP flange fails on setback                           | 1           | 1.1000E-09       | A1.17 | 1.1000E-09        | 5                | Factor 2                             |
| #307 Projectile Base deformed by propulsion gases             | 1           | 6.6700E-10       | A1.9  | 6.6699E-10        | 6                | Factor 3                             |
| #303 baseplug Vibrates loose                                  | 1           | 3.3400E-10       | A1.2  | 3.3399E-10        | 7                | Factor 1                             |
| #80 Cut Cartridge Case  | 1           | 1.0000E-10       | A1.3  | 9.9998E-11        | 8                | Factor 5                             |
| #502 Particles embedded in HE cause HE to initiate at setback | 1           | 5.0000E-06       | A2.15 | 8.1500E-11        | 9                |                                      |
| Improperly secured HE moves back and detonates at setback     | 1           | 2.0000E-11       | A1.16 | 2.0000E-11        | 10               |                                      |
| #65 Thin sidewall body fails on setback                       | 1           | 6.4000E-07       | A2.12 | 1.0432E-11        | 11               |                                      |
| PBXN-5 Develops cracks in storage #51                         | 1           | 1.0001E-11       | C1.1  | 1.0001E-11        | 12               |                                      |
| Voids in explosive pellet #52                                 | 1           | 1.0000E-11       | C1.3  | 1.0000E-11        | 13               |                                      |

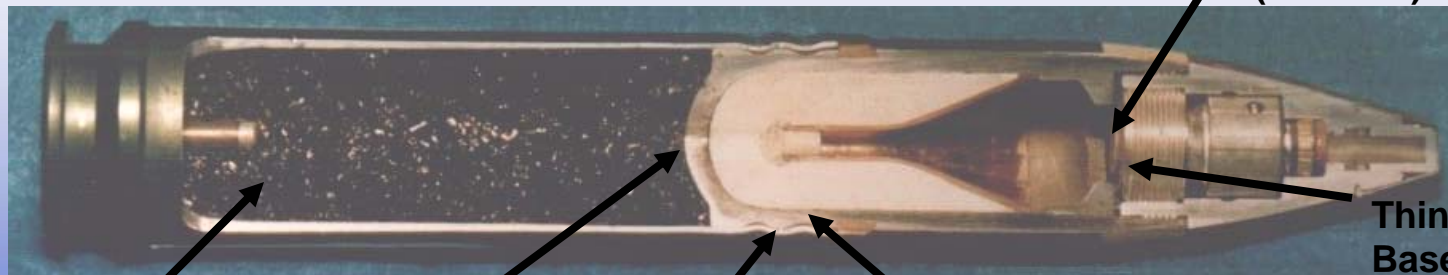
Factor 6 – Chamber Pressure G1 and G2

DOE Factor  
 Special Purpose Test  
 Redundant with a Prior Element Being Testing



|                             |            |             |      |
|-----------------------------|------------|-------------|------|
| In spec Ballistic Event     | 1.6345E-05 | 9.9998E-01  | A1.1 |
| #503 High pressure event    | 0.9227     | 1.63000E-05 | G2   |
| #503 Maximum pressure event | 0.9985     | 4.55000E-08 | G1   |

Loose Base Closing Plug in Fuze (Factor 1)



Propellant High Pressure (Factor 6)

Thin Dome (Factor 3)

Cut Case (Factor 5)









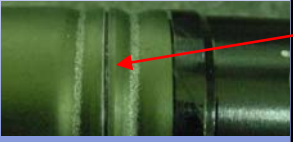

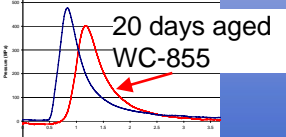
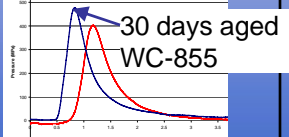
Thin Sidewall due to Eccentric Cavity at Crimp Grooves (Factor 4)

Thin Flange on Fuze Base Closing Plug (Factor 2)



# Main In-bore DOE

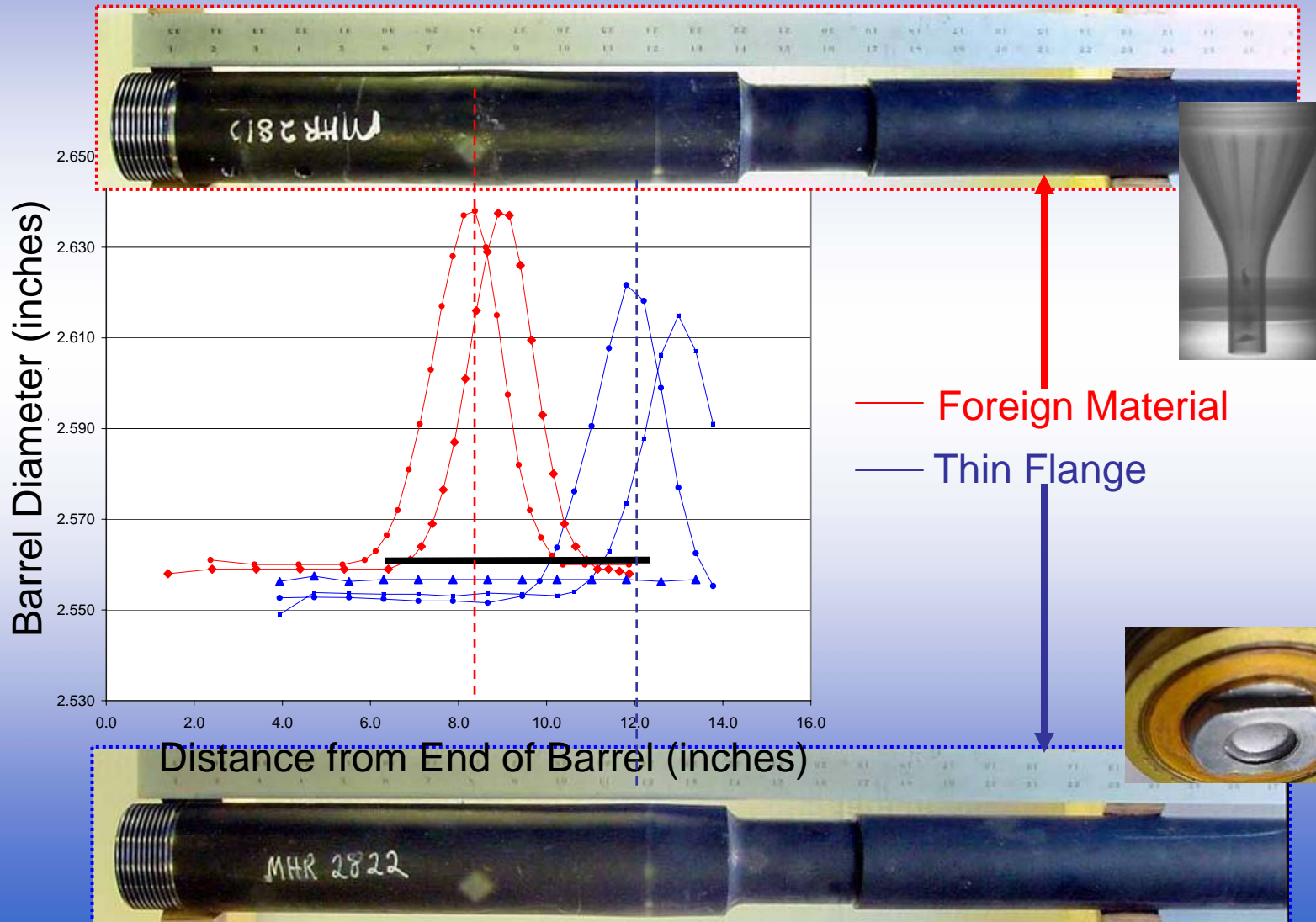


| Factor           | Example of "On" Factor Setting  |                                | Example of "Off" Factor Setting   |                               | Test Results |          |
|------------------|---|--------------------------------|---|-------------------------------|--------------|----------|
|                  |   |                                |   |                               | Shots "on"   | In-bores |
| Loose BCP        |    | ~1/2 Thread Engagement         |                                     | Full Thread Engagement        | 80           | 0        |
| Thin BCP Flange  |    | ~ .015" Flange Thickness       |  | ~ .044" Flange Thickness      | 5            | 3        |
| Thin Dome        |   | ~.05" Dome Thickness           |  | ~.125" Dome Thickness         | 80           | 0        |
| Eccentric Cavity |  | Max Eccentricity (~.020")      |                                  | Nominal Eccentricity (~.008") | 80           | 0        |
| Cut Cart. Case   |  | Cut through case to proj. body |                                   | No Cut                        | 80           | 0        |
| High Pressure    |  | ~405 MPa Chamber               |                                  | ~480 MPa Chamber              | 81*          | 1        |

\* 1 shot included thin BCP Flange



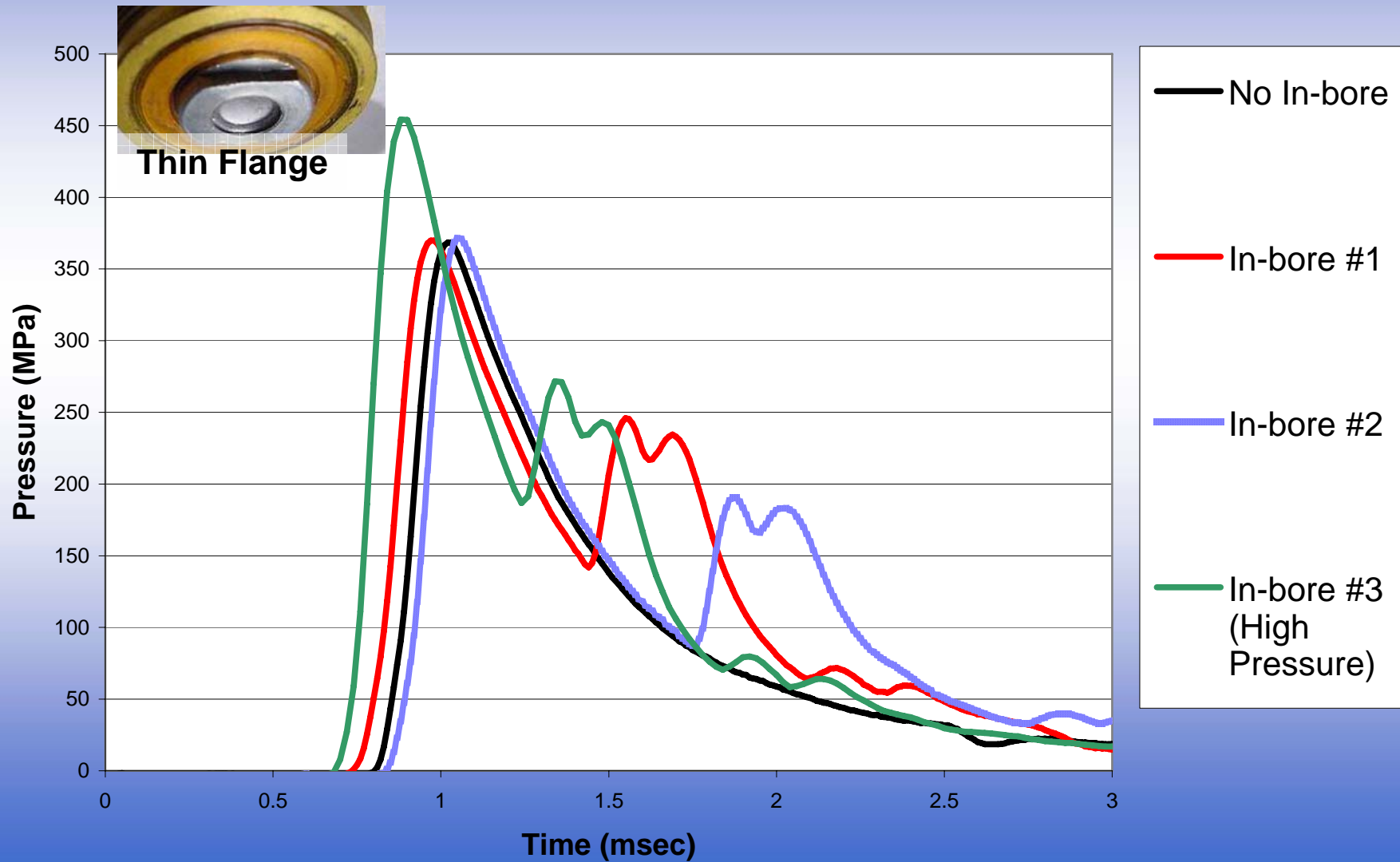
# Test In-bore Comparisons







# P-t Curves from DOE In-bores (Thin Flange)





# Inbore Detonation



- Most Likely Causes
  - ★ Foreign Material from Manufacturing Process in Liner Cavity (Replicated)
  - ★ Thin Flange/Spitback Crimp (Replicated)
- Actions Taken to Date to Reduce/Eliminate Issue
  - 1980s Production Placed into Condition Code 'N'
    - Removed to Strategic Reserve in Kuwait Planned for Demilitarization When Stockpile has been Replenished
  - 1990+ Production
    - Thin Flange on Base Closing Plug Identified as a Critical Defect
      - **Additional Testing Added to Verify Design Margin**
      - **Double Automated Inspections Added to Manufacturing Line**
    - Affected Lots (Prior Inbore Detonations) Restricted from Use Until Screened
    - X-Ray Screening to Remove Defective Rounds Being Initiated
    - Manufacturing Process has been Modified to Eliminate Source of Foreign Material
  - AIN & ASAM Issued to Minimize Ammo Exposure to Extreme Temperatures



# Bullet on Bullet



# Bullet on Bullet



- A loss of propellant due to punctured case caused:
- 1 Increased Action Time (5 to 24 ms)
  - 2 Decreased Range
  - 3 Projectiles stuck beyond origin of rifling at ~15% propellant load
  - 4 Projectiles stuck at origin of rifling or failed to debullet at 5-10% propellant load.



**Field Incident**



**Stuck Projectile Test**



# Bullet on Bullet



- Most Likely Causes
  - ★ Cartridge Cases are Punctured and Propellant is Lost
    - Efficiency Loss to a Level of 10-15% (Replicated)
- Actions Taken to Reduce/Eliminate Issue
  - ASAM #AH-64-07-ASAM-13 Issued
    - Emphasizes Use of “Auto” Mode for D Model Apache Sideloader which Minimizes Risk of Creating and Firing Punctured Cases
    - Requires Download and Inspection of Ammunition at Aircraft Regularly Scheduled Maintenance
    - Re-emphasizes the Need for Caution Uploading/Downloading the Aircraft to Avoid Punctured Cartridge Cases

# Summary



- Investigation is Completed
- Final Reports are Being Written for Individual as well as Combined Efforts
- Investigation Results are Being Formulated into:
  - Design Changes
  - Manufacturing Process Changes
  - Stockpile, Manual and/or Procedural Changes, as Applicable