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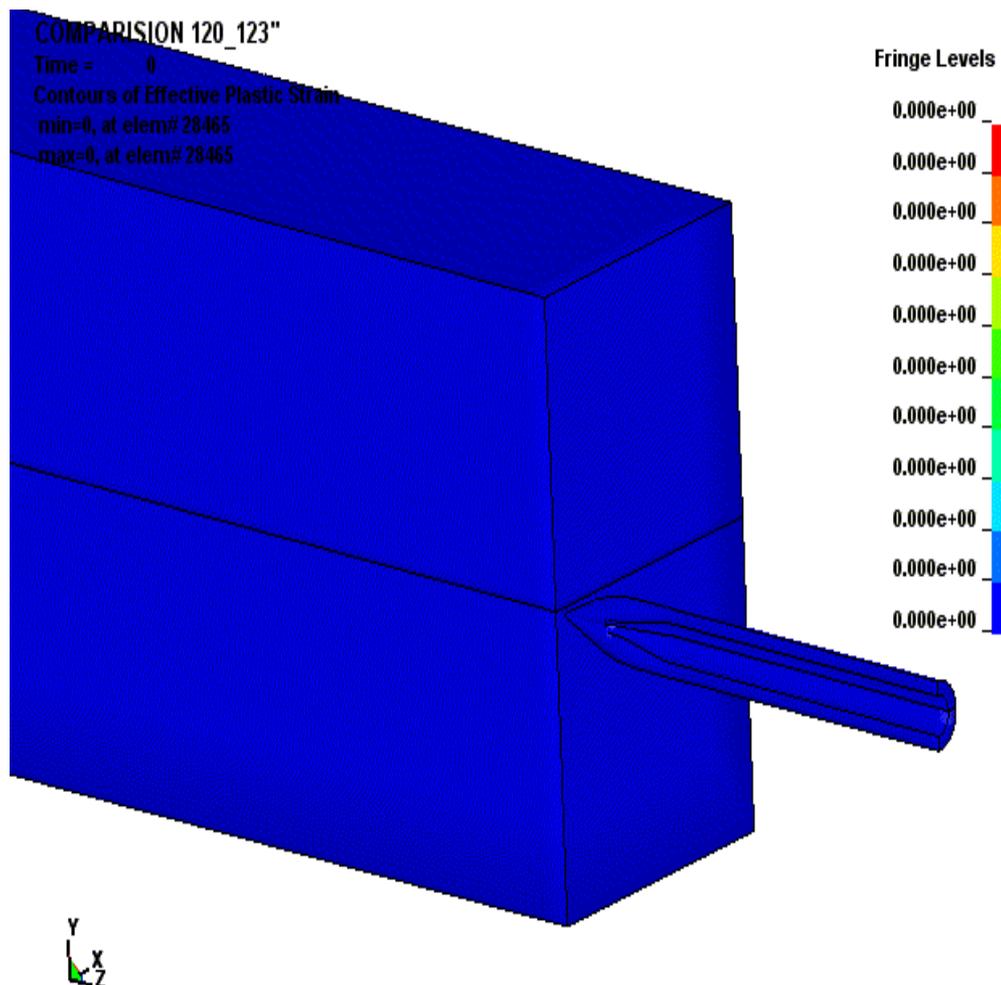
54th Annual NDIA Fuze Conference; May 12, 2010

TITLE

Dynamic impact simulation of "high g hardened fuzes".

AUTHOR

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ME US NAVY
CHINA LAKE





Purpose and goal



- The purpose of this paper is to document the **development of a new simulation tool** which is being employed to simulate deceleration, stress, and strain imposed on penetrators and fuzes during typical cannon and sled tests.
- The secondary goal is to create standard **“LS-DYNA input templates”** which can be employed by the “non-expert user” to simulate cannon and sled tests.





New Simulation method

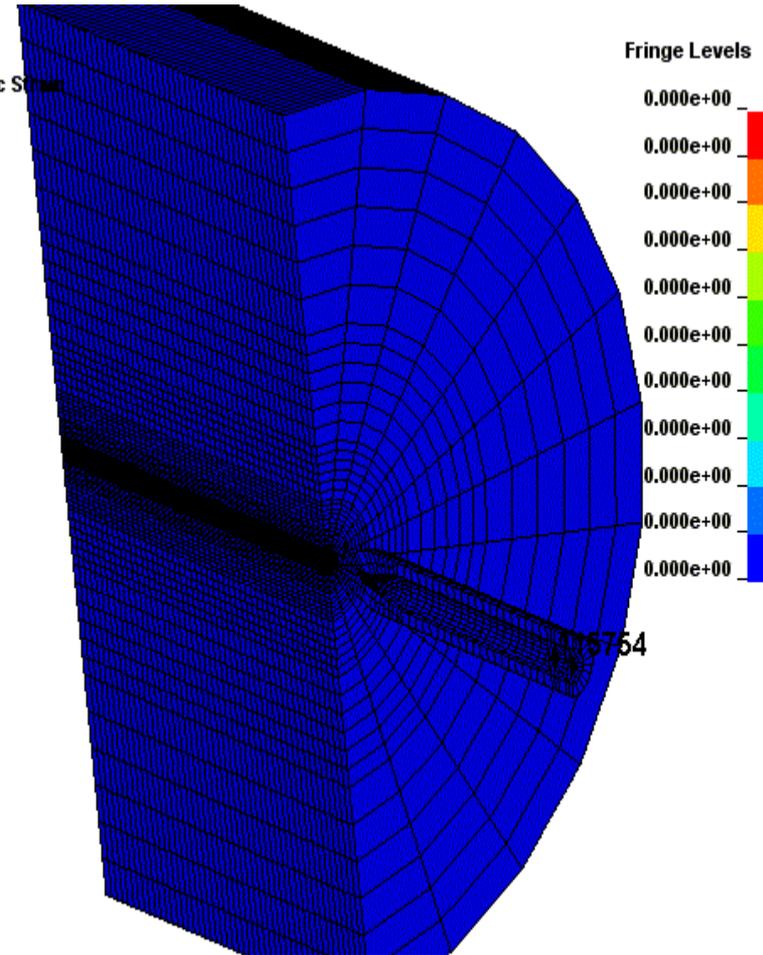


Concrete model
*MAT_159
Failure damage
User friendly
Fast / Robust

Lower stiffness material
dominates performance
e.g. concrete
10 times lower mod
10 times lower yield

Concrete model is critical
Penetrator is secondary

Time = 0
Contours of Effective Plastic Strain
min=0, at elem# 28465
max=0, at elem# 28465



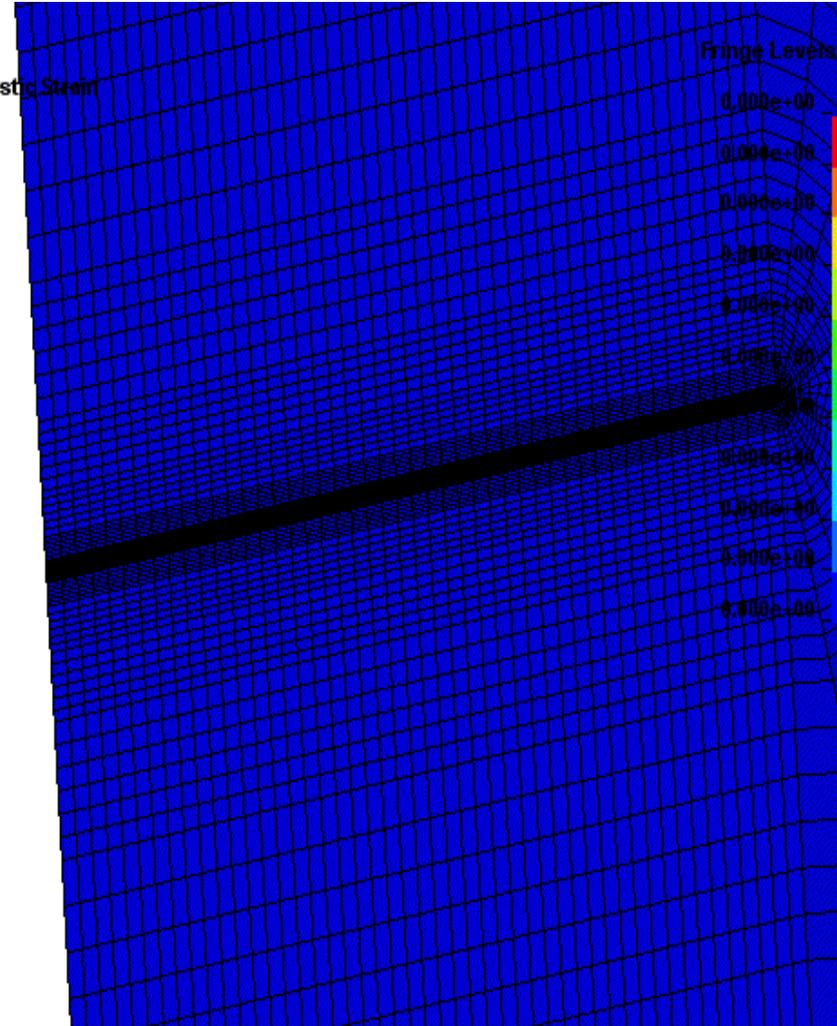


Down load written paper



- UNCLASSIFIED LS_DYNA input template can be down loaded DTIC website
- UNCLASSIFIED written paper version of presentation may be down loaded DTIC website
- paul.glance@navy.mil
- 760-939-7358

LS-DYNA user input
Time = 0
Contours of Effective Plastic Strain
min=0, at elem# 28465
max=0, at elem# 28465





BACKGROUND

- Cannon tests and rocket propelled sled tests are the standard test methods employed to “proof test” the successful operation of hardened fuzes.
- The new LS-DYNA concrete material model (*MAT 159) and eroding contact option allows rapid simulation of impact penetration and by-passes the need for excessive computer run times often required for Arbitrary Lagrangian Eulerian (ALE) LS-DYNA models and equation of state (EOS) material models.
- This paper describes a simple, fast running LS-DYNA application for simulating cannon and sled tests which runs on a “Dell workstation employing one Intel processor” in a few hours of equation-solver time and accurately predicts; depth of penetration, exit velocity, deceleration, and the typical “conical” entrance and exit fracture patterns in a concrete target.



Three types of impacts



Three impact cases are investigated and the results compared to test data. The three cases are:

- Case-1, typical calibration impact case of a known penetrator impacting, arrested, and captured by a large concrete block. **Compare to open literature.**
- Case-2, typical cannon test with concrete target blocks. **Compare to on-board data recorder.**
- Case-3, typical sled test with a sequential target set consisting of concrete blocks, air voids, and back stop. **Compare to prior tests.**





Post-test photographs of the impact face of the 1.83, 1.37, and 0.91-m diameter targets.



$D/d = 24$
 $V_s = 335 \text{ m/s}$



$D/d = 18$
 $V_s = 332 \text{ m/s}$



$D/d = 12$
 $V_s = 337 \text{ m/s}$



Case 1b, no exit, large target, correct damage pattern, penetration and rigid body deceleration



LS-DYNA user input

Time = 0

Contours of Effective Plastic Strain

min=0, at elem# 28465

max=0, at elem# 28465

Fringe Levels

0.000e+00

382.6



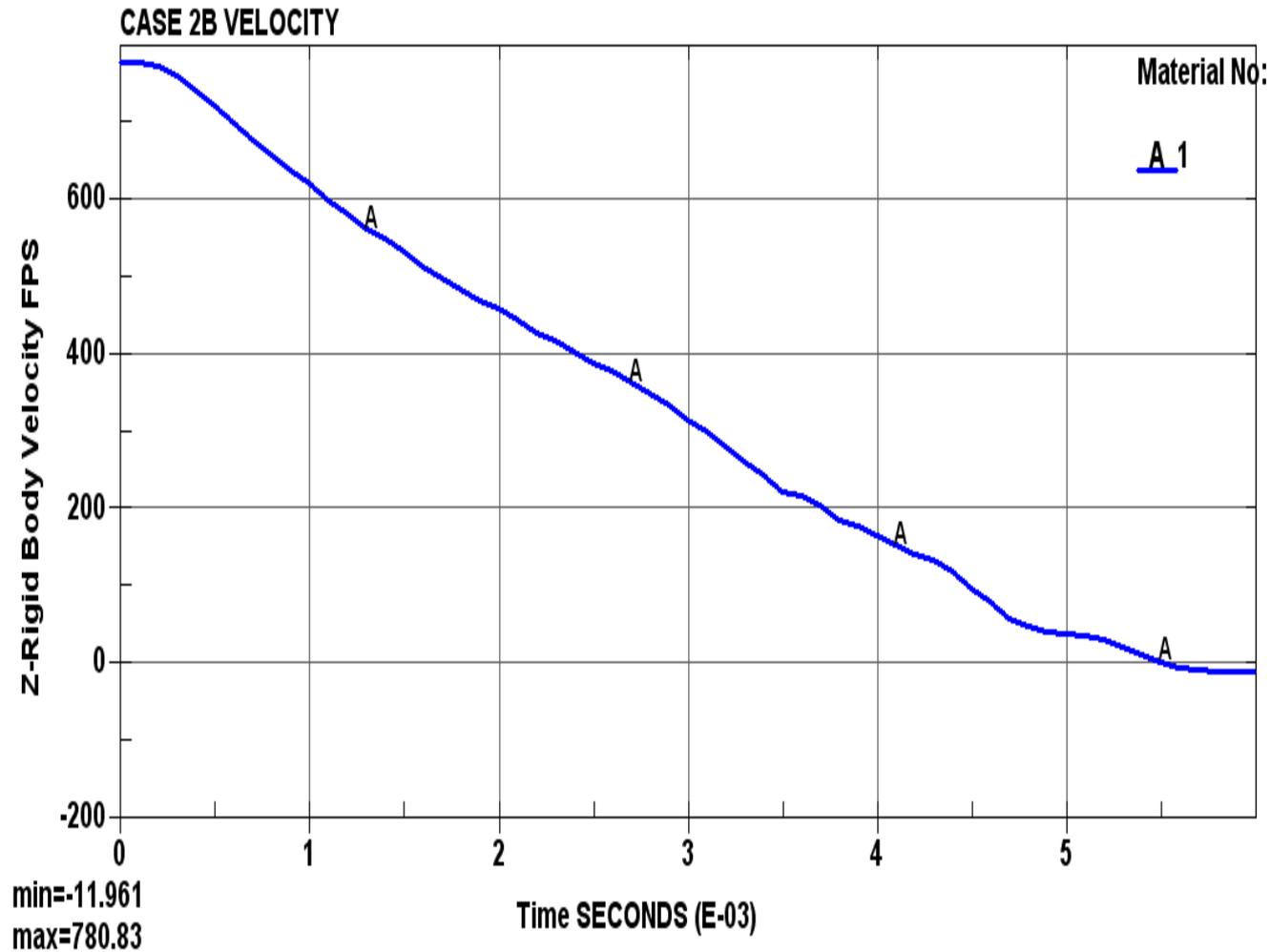
1/3 to 1/2
dia
damage





Case 1b Velocity

Approx
Linear negative
slope



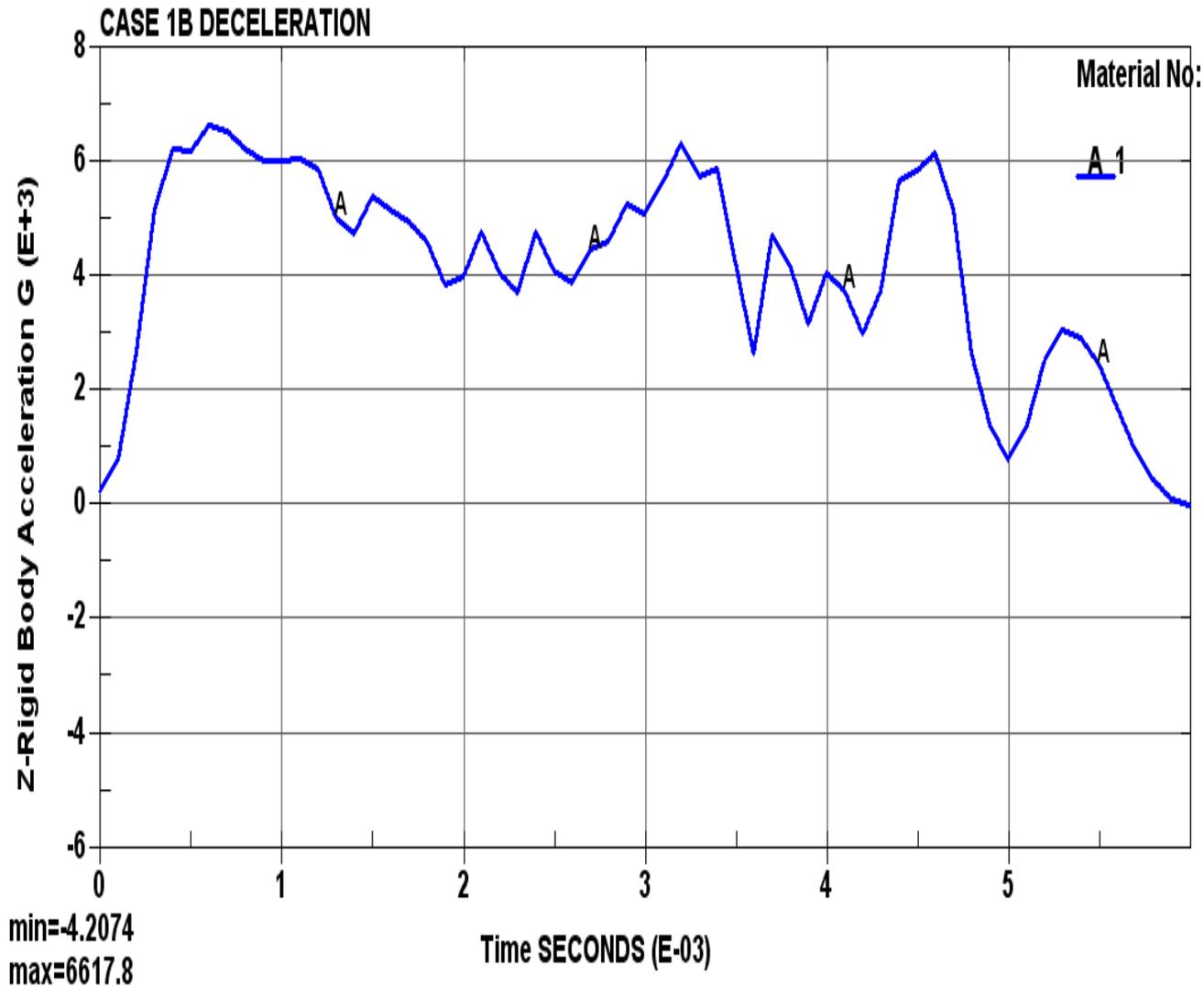


Case 1b Deceleration



Square wave
Deceleration pulse
For case1 only

Concrete acts as
Energy absorber
Applications
Back stop





Case 2 Eglin Air Force Cannon test





Case 2 Eglin Cannon test exit face



Note exit face 100%
fracture

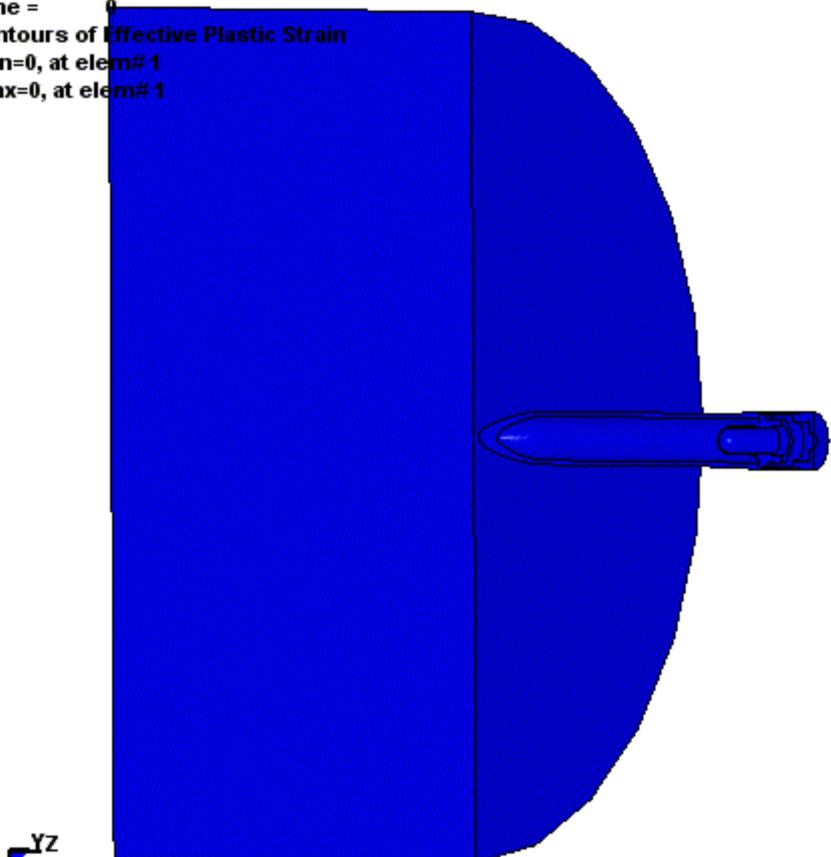




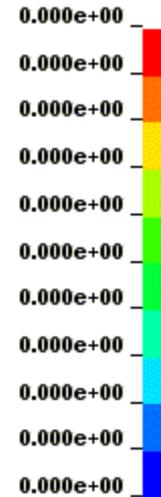
Case 2, cannon, 4 feet concrete correct exit velocity and deceleration

1350FPS 90 DEG 6000PSI 4FT

Time = 0
Contours of Effective Plastic Strain
min=0, at elem# 1
max=0, at elem# 1



Fringe Levels



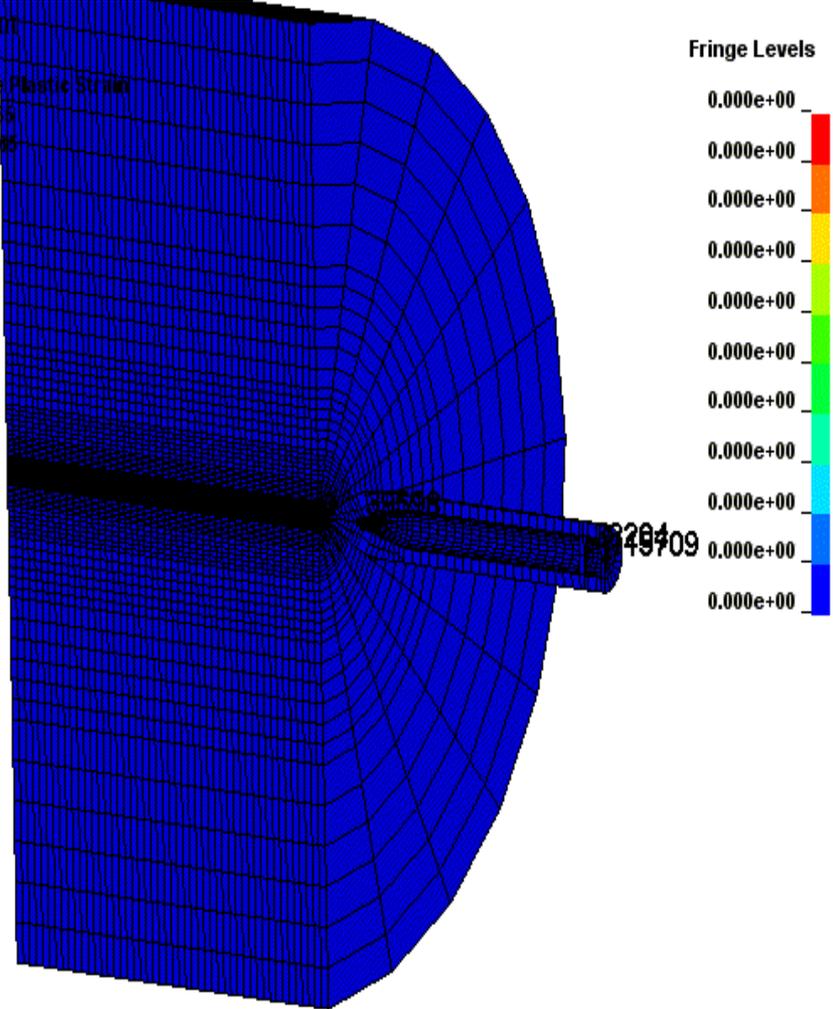


Approx fracture pattern



The concrete fracture region (erosion region) and spall pattern of the present methodology also agrees in general appearance with high speed test film but varies from test to test due to the nearly random crack propagation of concrete. The high speed film of the test shows that the concrete continues to fracture after the penetrator has exited the target.

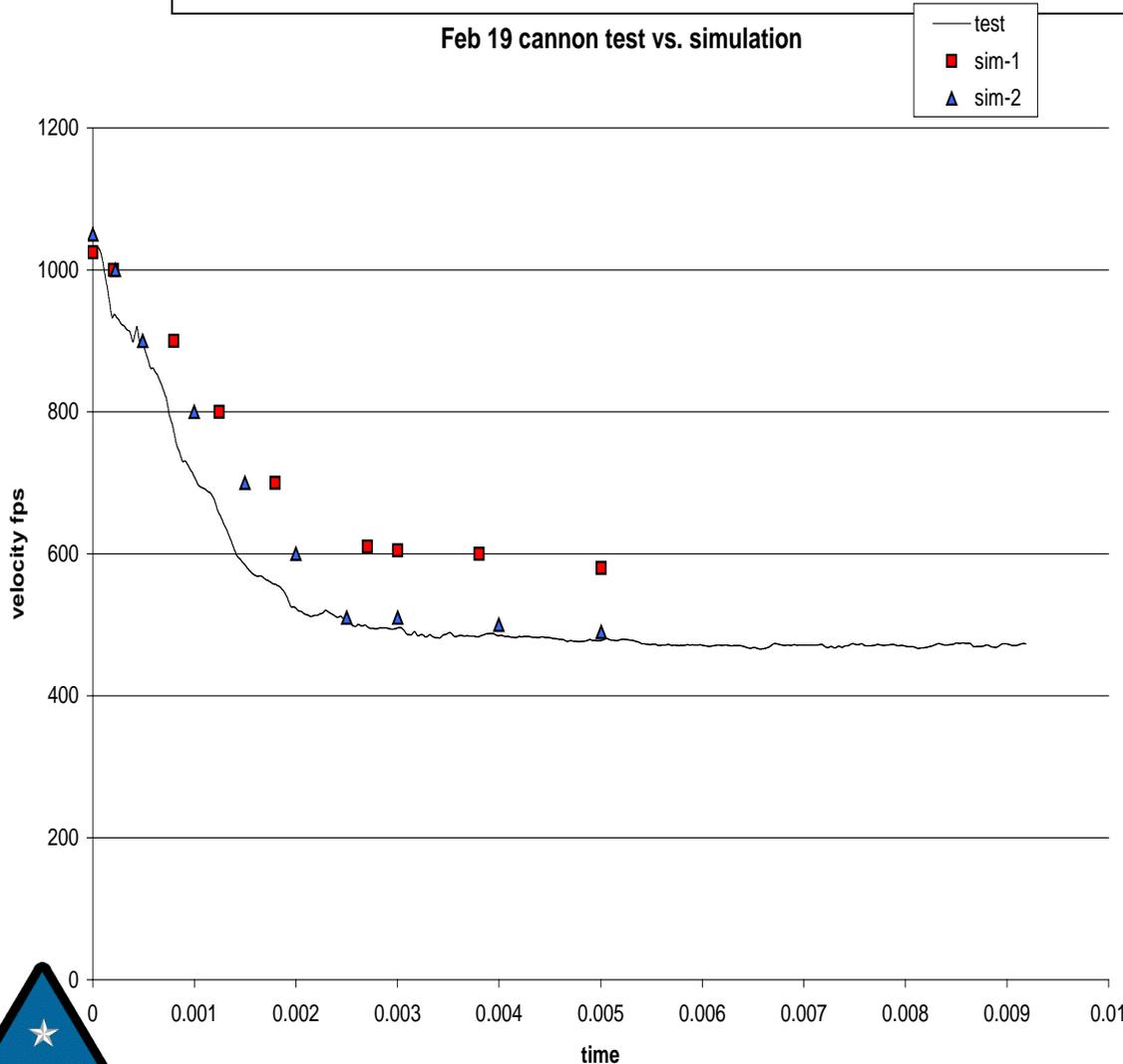
LS-DYNA user input
Time = 0
Contours of Effective Plastic Strain
min=0, at elem# 28465
max=0, at elem# 28465





Comparison test vs. simulation; velocity vs. time

Feb 19 cannon test vs. simulation



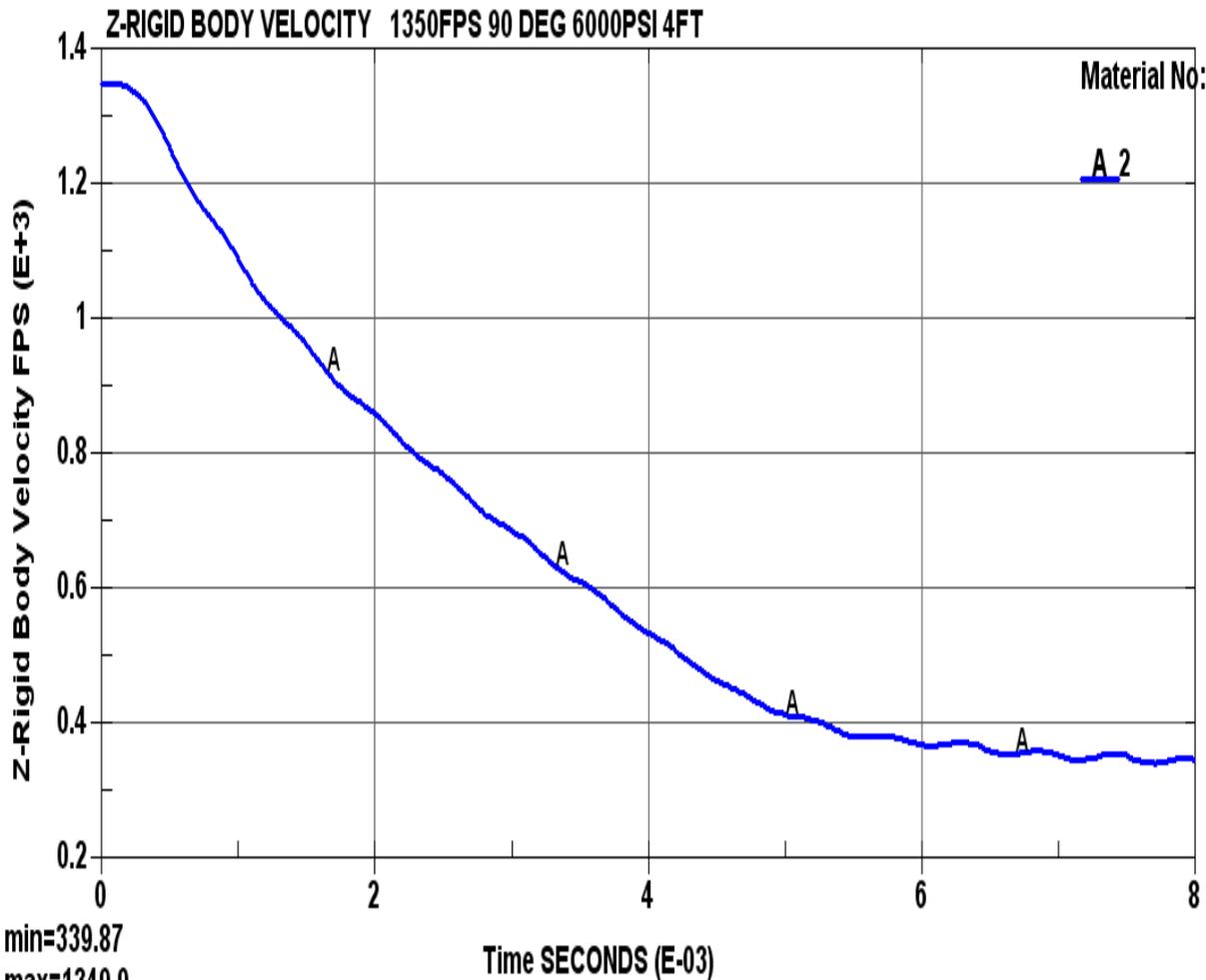
Second iteration
Approx matches
Test data

Concave curve
Entrance max negative slope
Break exit face
Sliding friction





Rigid body velocity exit 340 vs. 358



Concave curve
Break exit face
Sliding friction

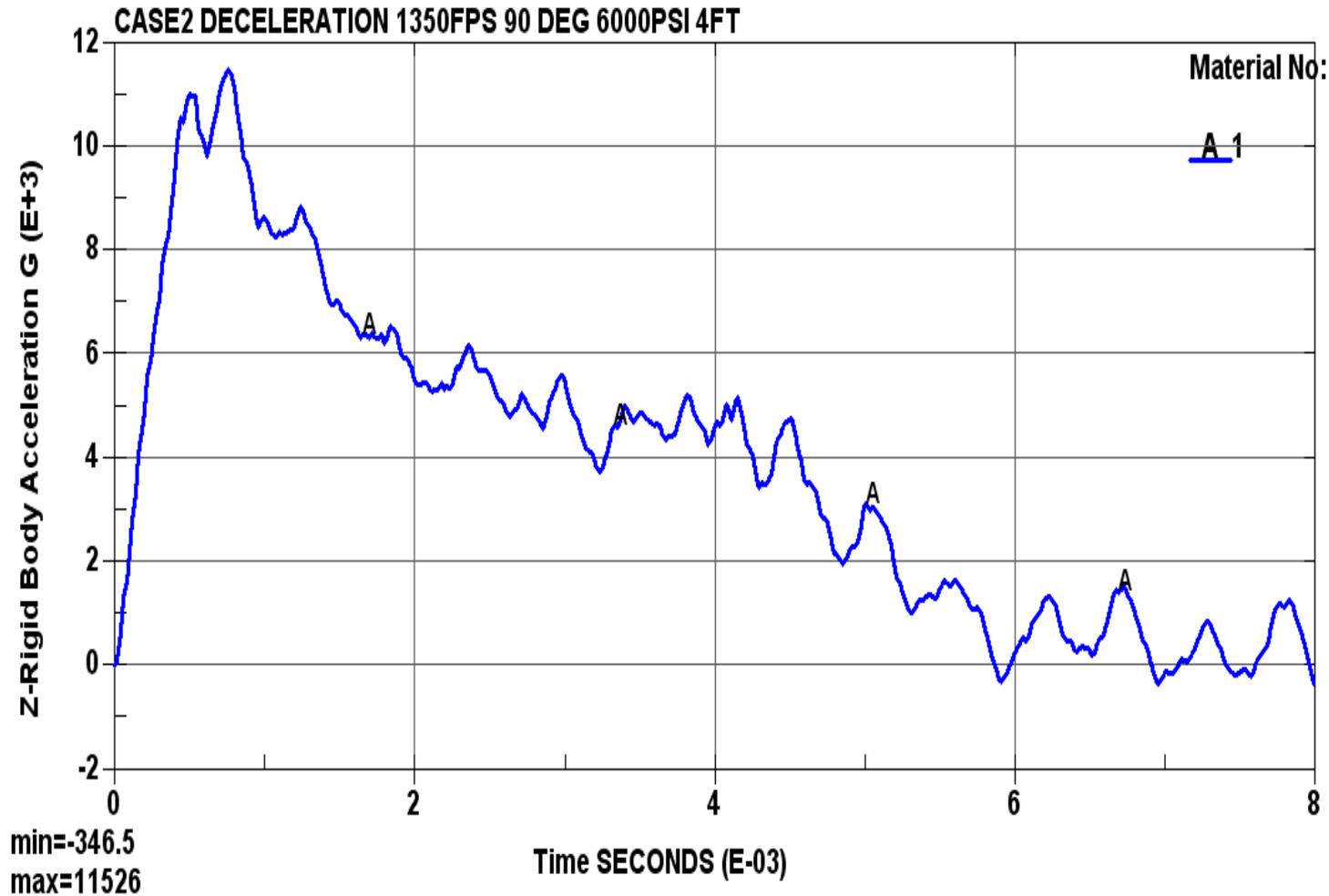




Rigid body deceleration



Peak G reported depends on
Filter
Location
Type accelerometer
Sampling rate



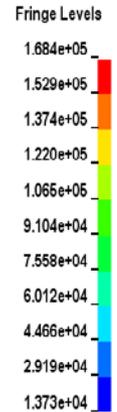
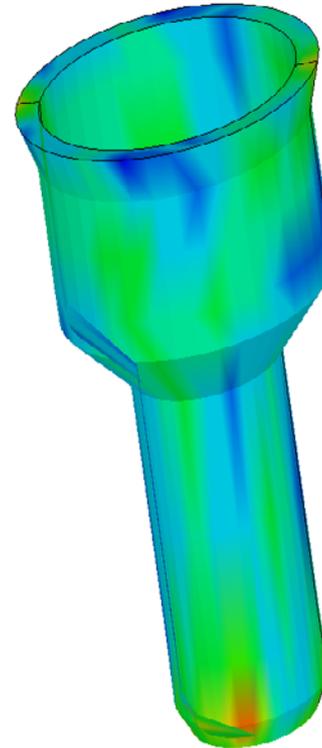


Max stress during impact for generic fuze well



TEST 5 SMOOTH
Time = 0.02816
Contours of Effective Stress (v-m)
min=13730.7, at elem# 622483
max=168355, at elem# 622771

Max strain and stress
For each part at each
time step
Determine failure





Case 2b, 15 degree, 2 feet concrete

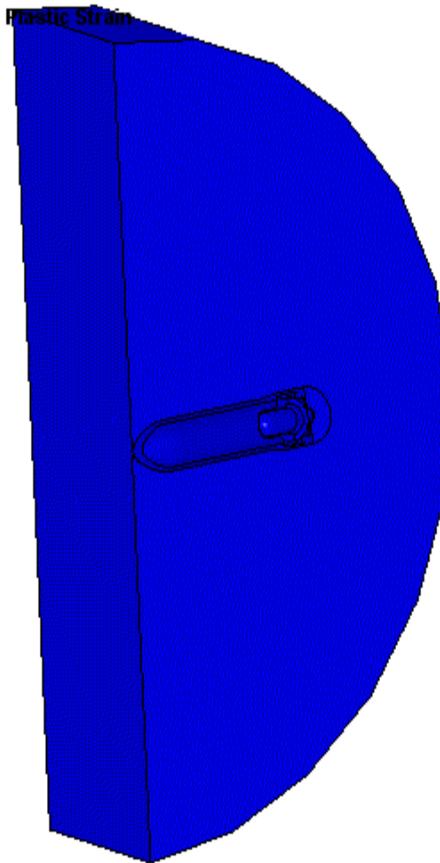


LS-DYNA user input
Time = 0
Contours of Effective Plastic Strain
min=0, at elem# 1
max=0, at elem# 1

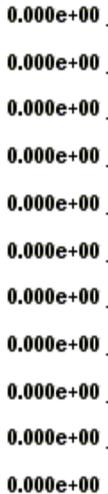
Same Input parameters for;

- 6 target sets
- Large and small penetrators
- Large and small diameter targets
- Range of impact velocities
- Range of angles of impact
- Half and quarter models
- Course and fine mesh

All compare well with test data



Fringe Levels





Case 3 SNORT

Rocket sled track test

NAV  AIR

Full scale China Lake test

AOA for SNORT tests is random
1-3 deg





Case 3 SNORT test



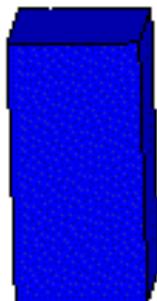
LS-DYNA user input

Time = 0

Contours of Effective Plastic Strain

min=0, at elem# 28465

max=0, at elem# 28465



Fringe Levels

0.000e+00

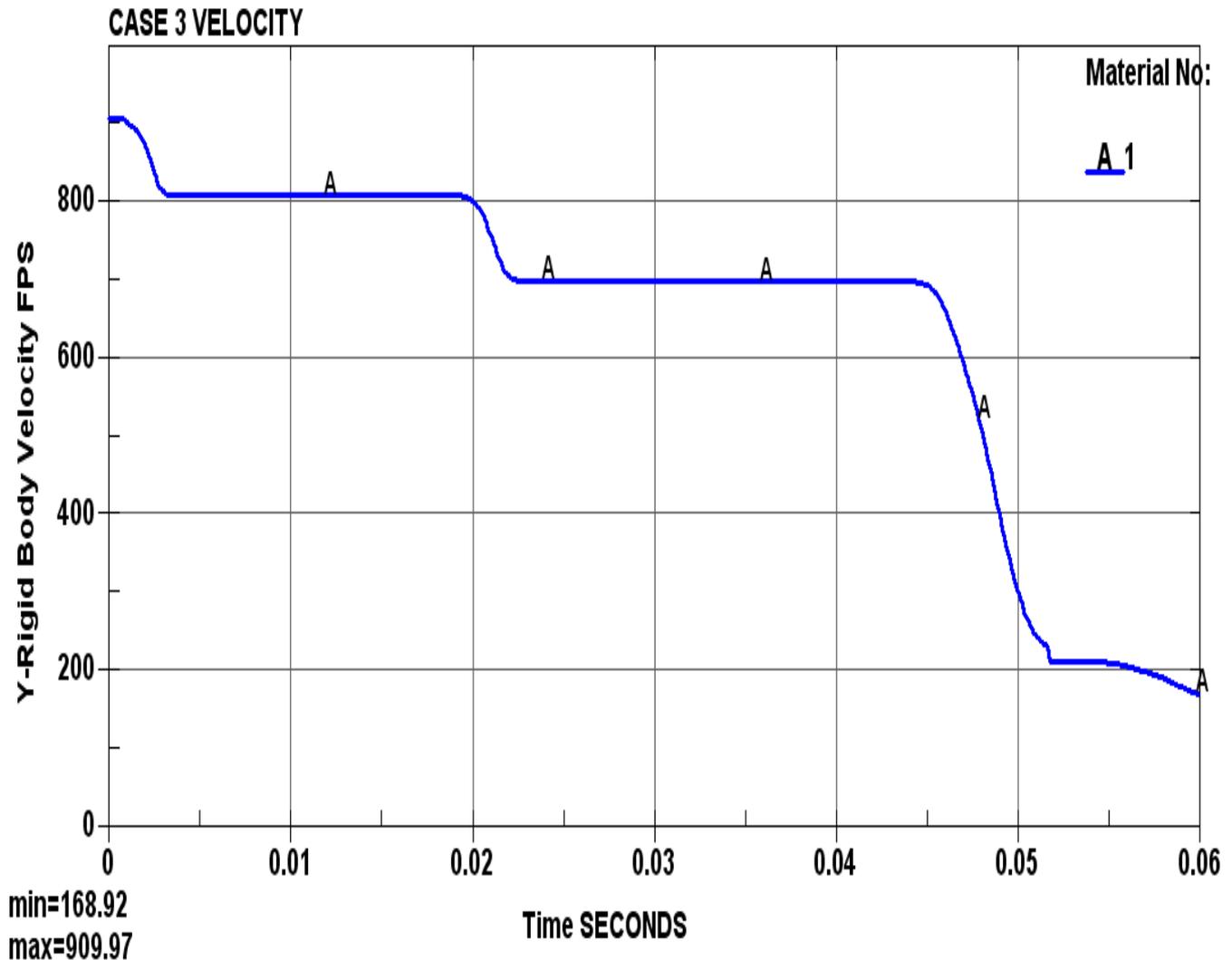




Case 3 velocity vs. time



Smooth well
Behaved curve
Fuze can Sense
velocity

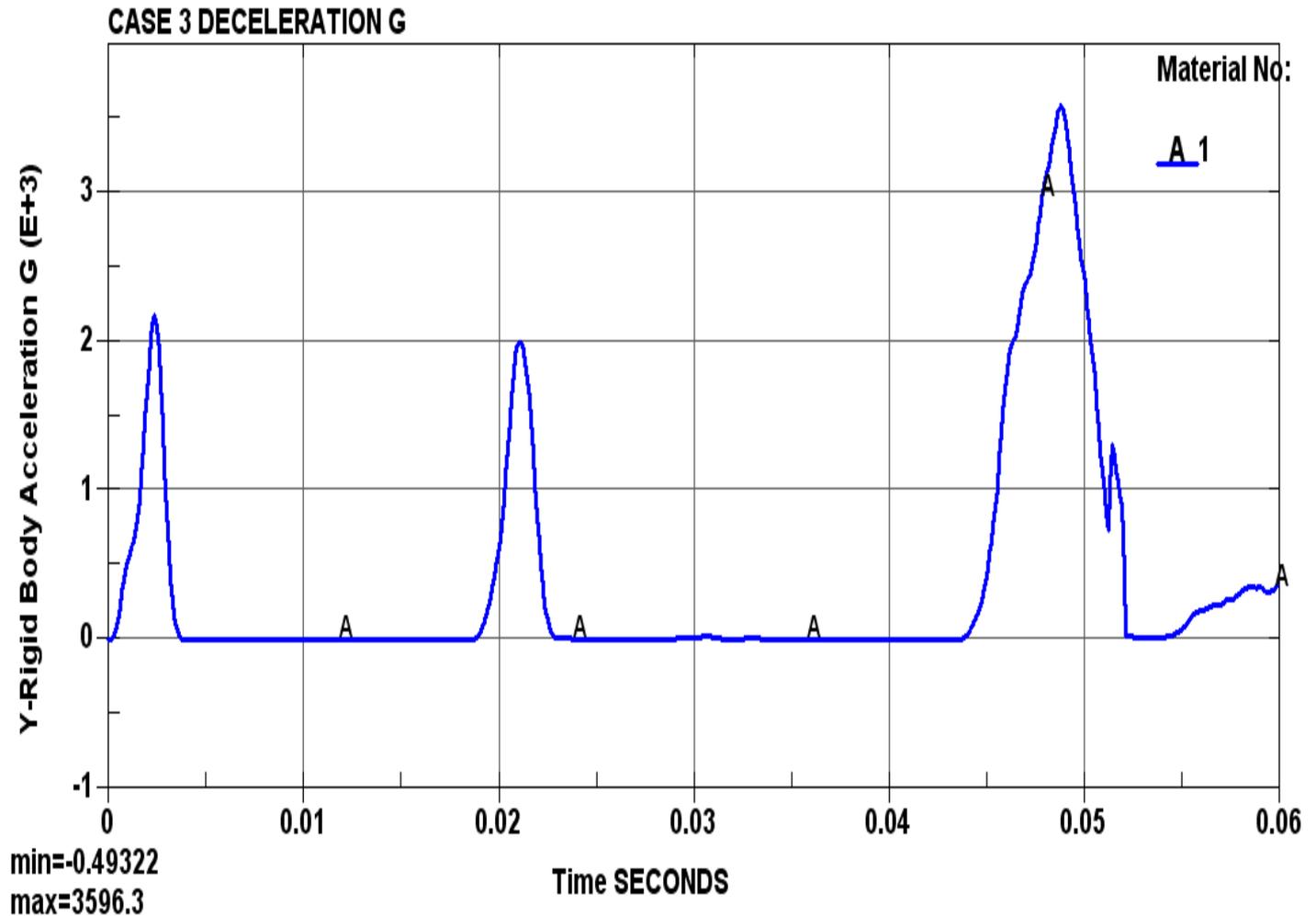




Case 3 Deceleration, g



Short
Deceleration
Pulses
May approach
High frequency
noise

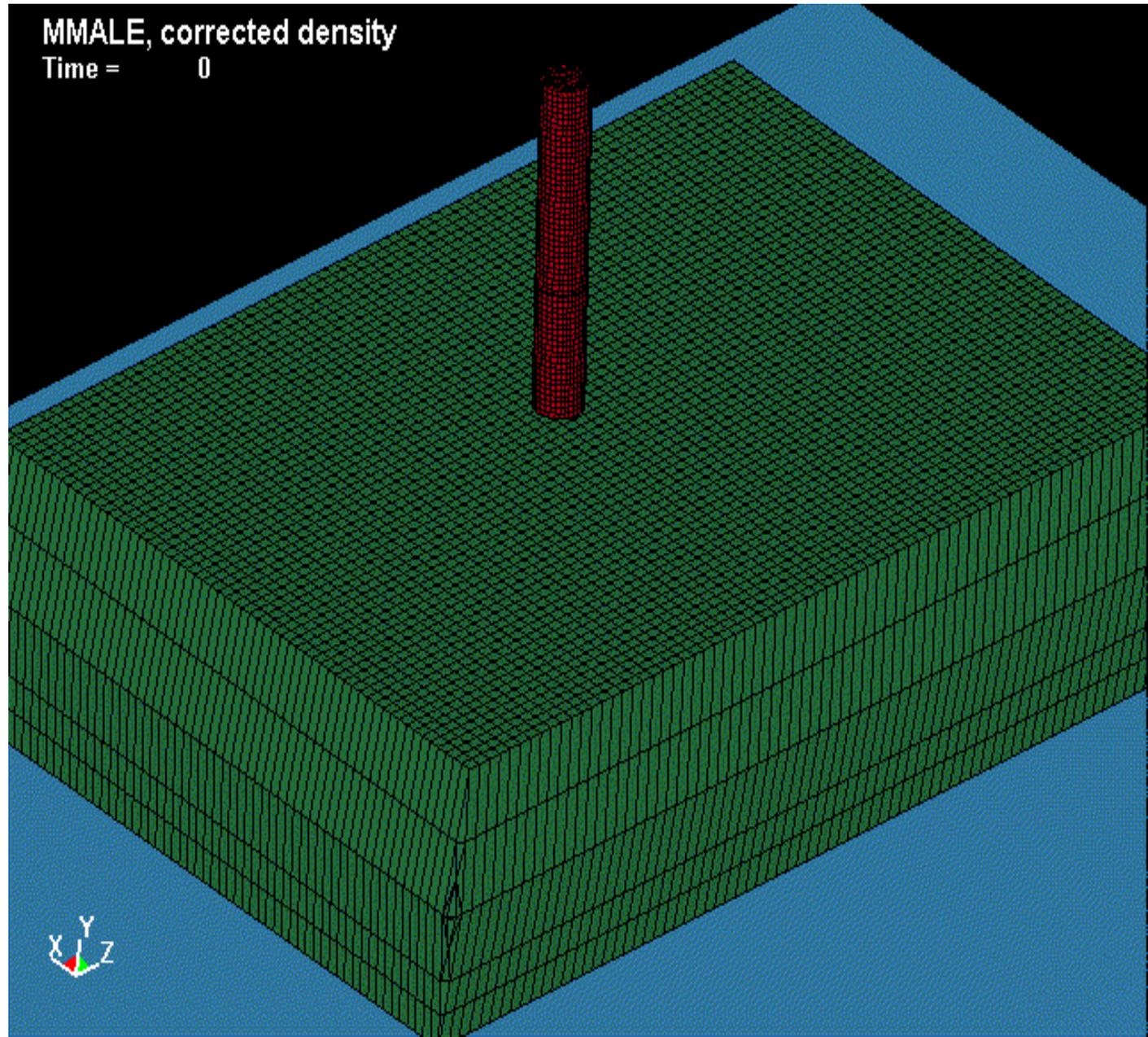




FLUID example requiring full ALE method with fluid interaction



low
velocity
impact into
air bag
floating on
“China
Lake”





Recommendations

TEST 4

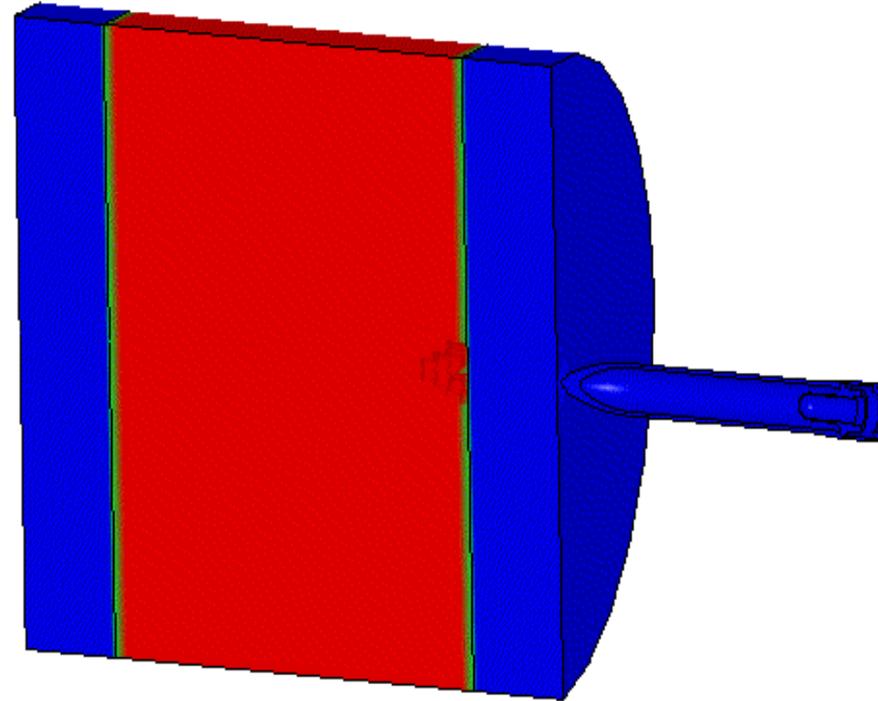
Time = 0

Contours of Effective Plastic Strain

min=0, at elem# 1

max=0.99, at elem# 876810

- TEST---Better concrete and soil target specification; density, compression mod, no aggregate, consistent mix
- Peak deceleration---- better specification of filter, location, standard method
- Fuze--- velocity sensor
- Simulation---Standard template for each test





Conclusion



- A new application of LS-DYNA has been developed by the Safe-Arm Development Branch, NAWCWD to determine stress and strain loadings on fuzes during cannon and sled tests. The simulation results are in **good agreement with test data**. The new simulation tool will find **application as a standard method of specifying fuze performance requirements and allows calculation of stress and strain**, under a wide range of impact conditions and targets.





Thank You



- Please download the written paper and direct questions to
- Paul Glance
- Paul.glance@navy.mil
- 760-939-7358

TEST 2 1300 FPS
Time = 0
Contours of Effective Plastic Strain
min=0, at elem# 1
max=0, at elem# 1

