

SPECIAL MISSIONS



**RAPID RESPONSE
PROVEN SOLUTIONS**

A Method for Determining the Effects of Overpressure from Small/Medium Weapons Fire – Abstract 11838

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- Small/Medium Caliber Weapons on Air Platforms
- SH-60S Armed Helicopter
 - GAU-21 (.50-cal)
 - M240 7.62 mm
 - 20 mm Weapon Systems
 - RAMICS
- Aircraft Skin Limits



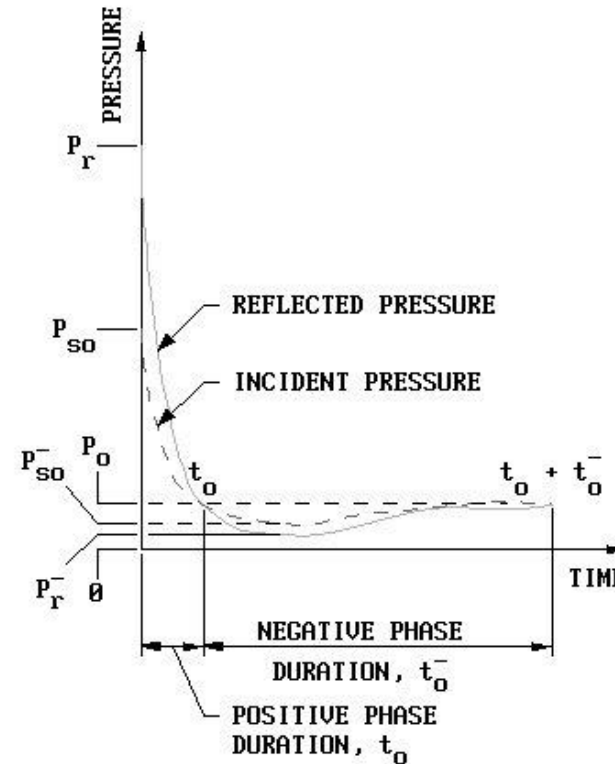
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Shockwaves



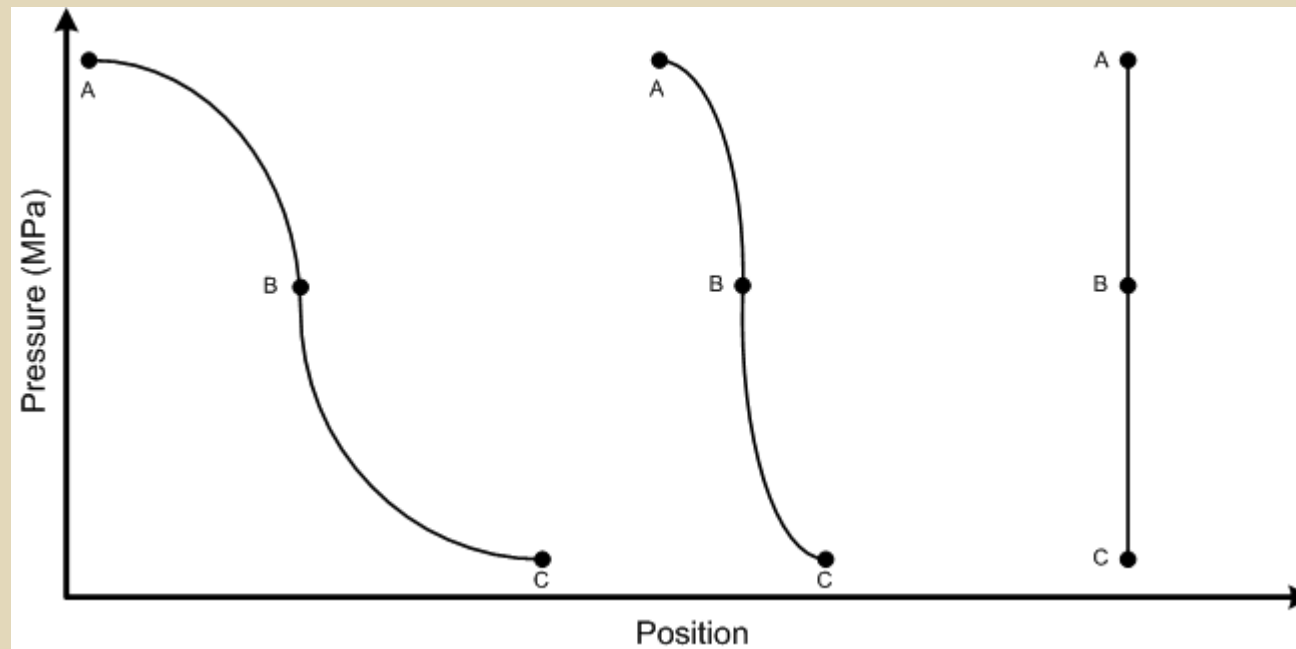
- Shockwave - a region across which there is a rapid pressure, temperature and density rise, usually caused by a body moving supersonically in a gas or by a detonation
- Characteristics:
 - Near-discontinuous pressure rise
 - Exponential decay. Positive Phase duration. Relatively short duration.
 - Negative phase.
 - Dependent on angle of incidence.

Figure 2-5. Pressure-time variation for a free-air burst



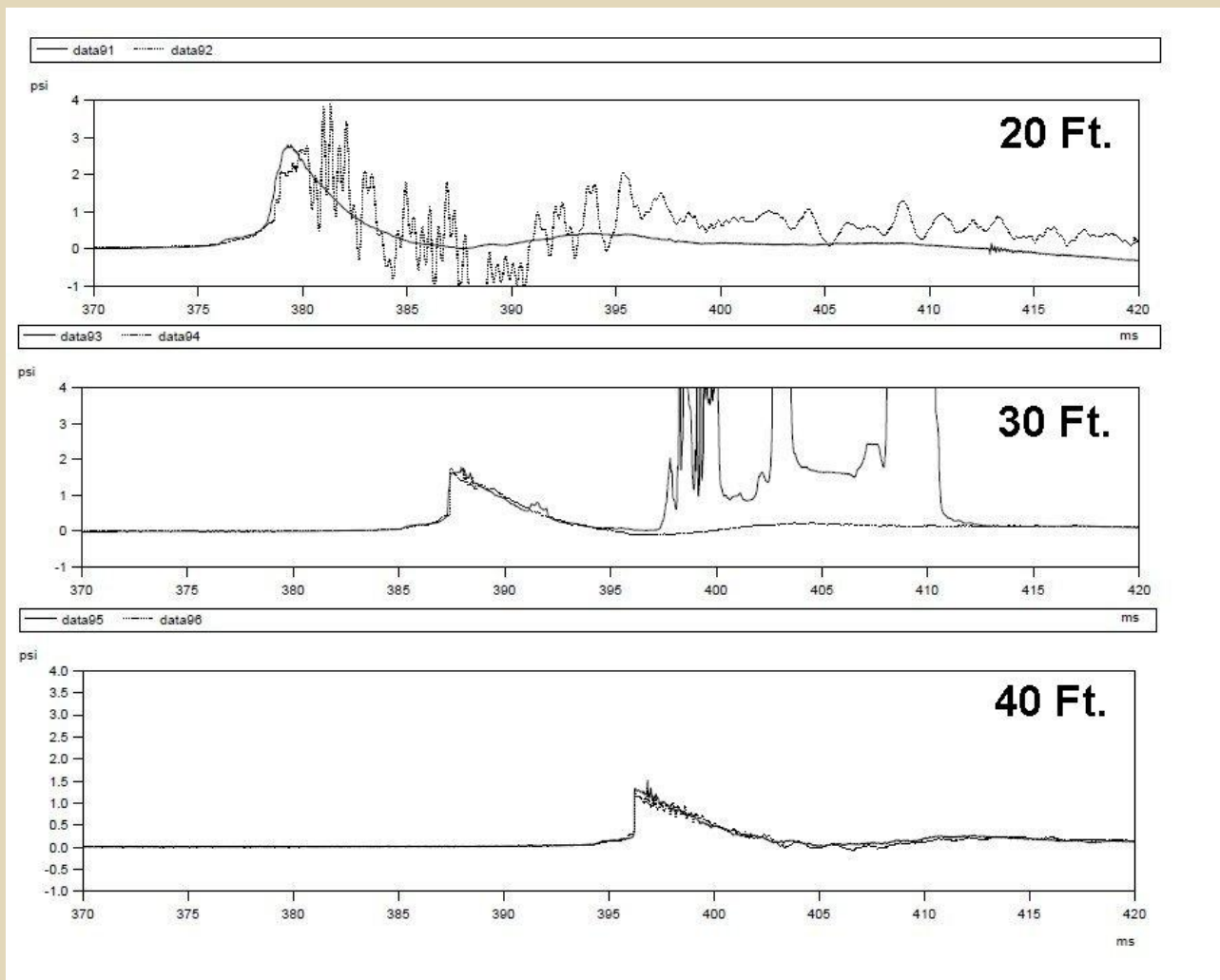
Shock Waves from Gunfire

- Non-ideal source. Source is not a detonation.
- Similar to “Shocking Up”



Shock Waves from Gunfire

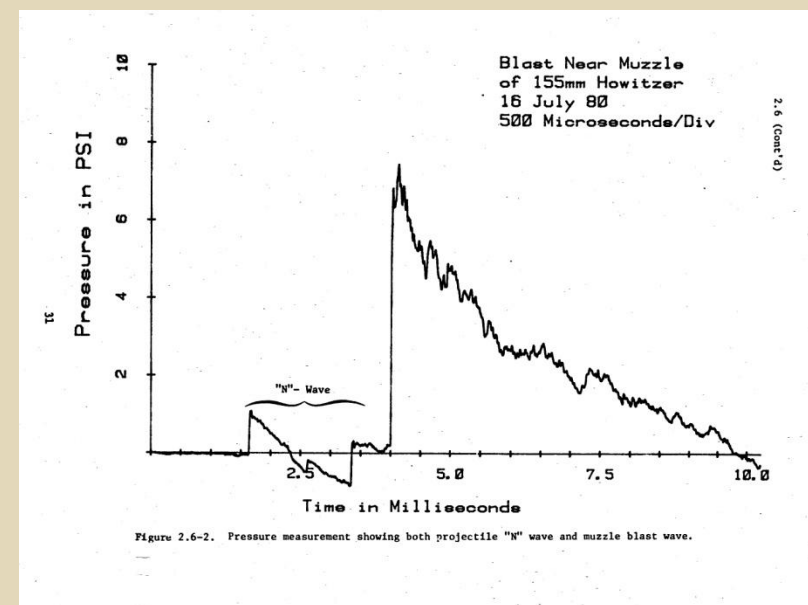
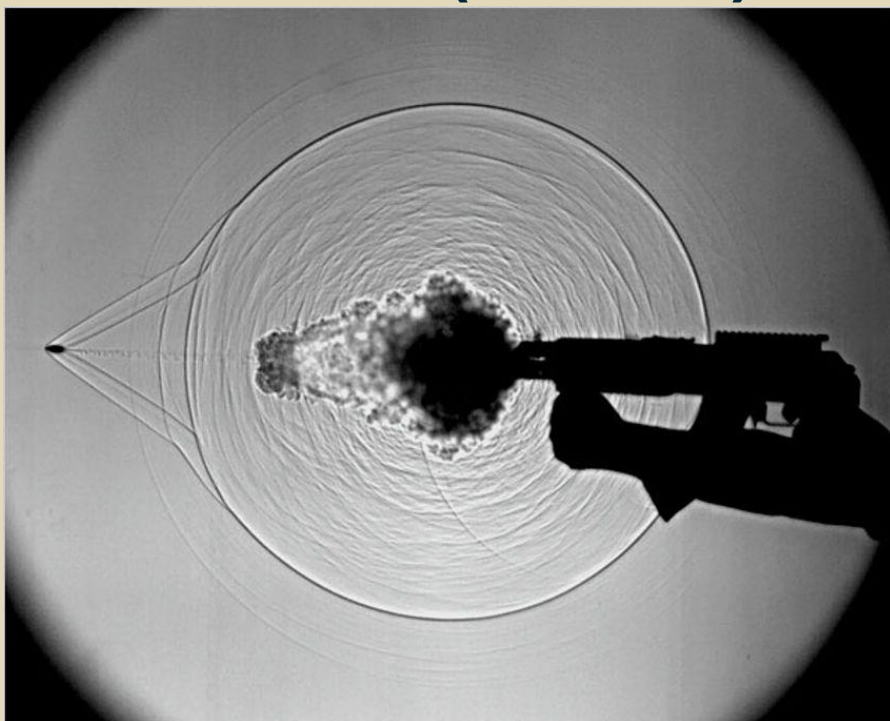
• Shocking Up



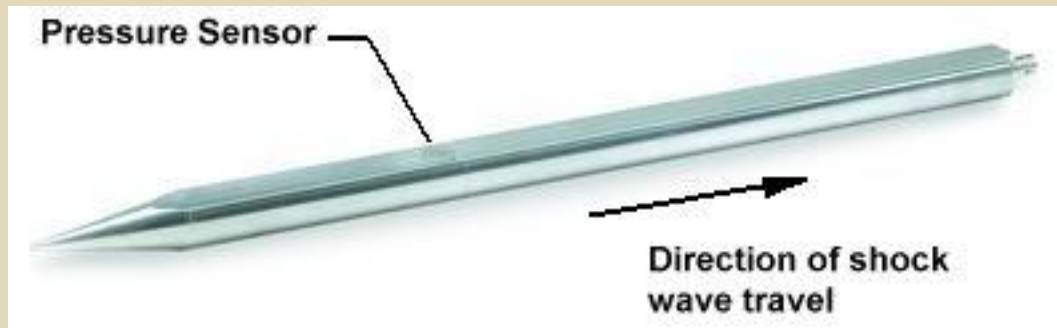
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Shock Waves from Gunfire

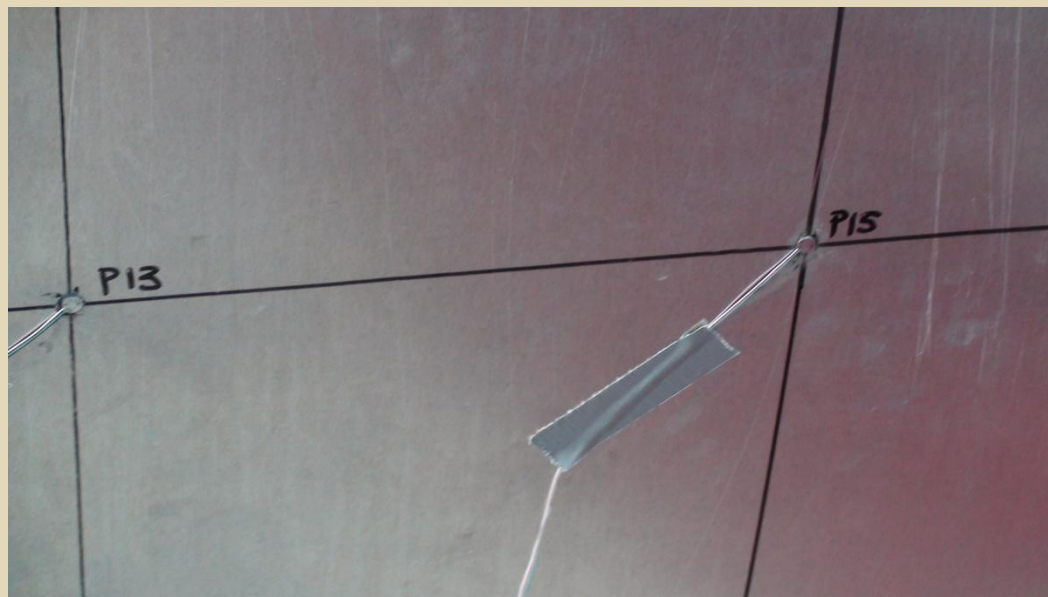
- Measurement may see both projectile shockwave (N-wave) and the Muzzle Blast



Shock Measurements



PCB Model 137A23
Blast Probe – (Incident
Pressure)



Endevco Model 8515C-15
Pressure Sensor
(Reflected Pressure)

Incident Pressure vs. Reflected Pressure (Ideal)

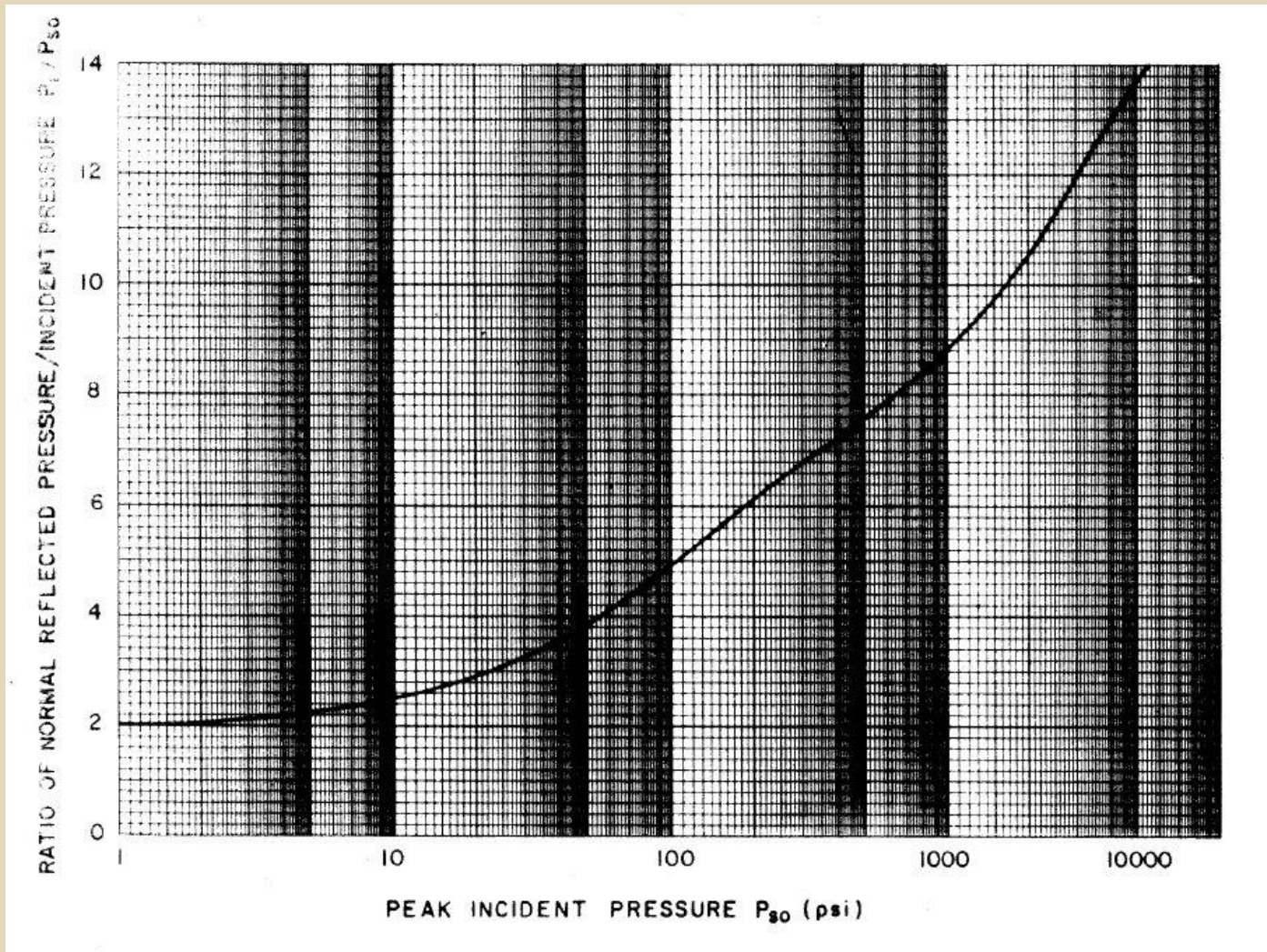


Figure 2-6 Peak incident pressure versus the ratio of normal reflected pressure/ incident pressure for a free air burst

Angle of Incidence

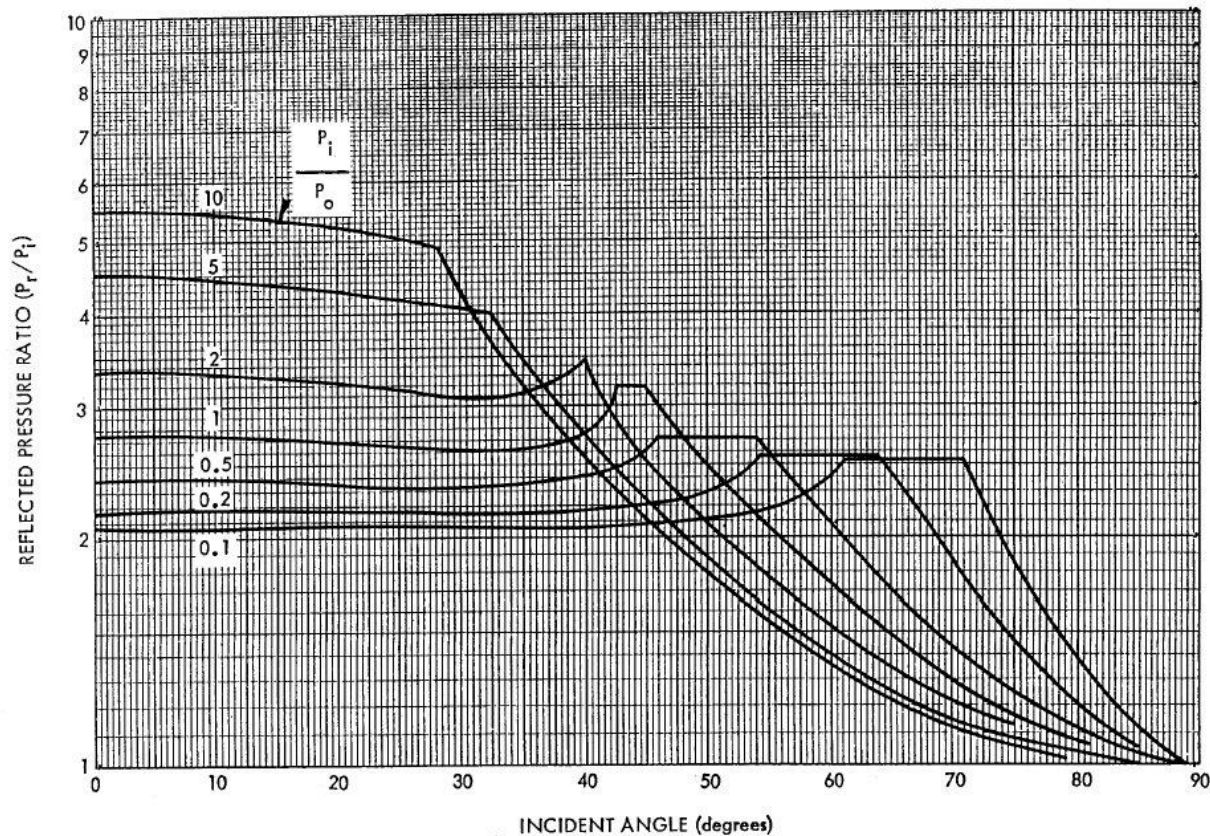


FIG. 13a REFLECTED OVERPRESSURE RATIO VS ANGLE OF INCIDENCE FOR VARIOUS INCIDENT OVERPRESSURE RATIOS

107

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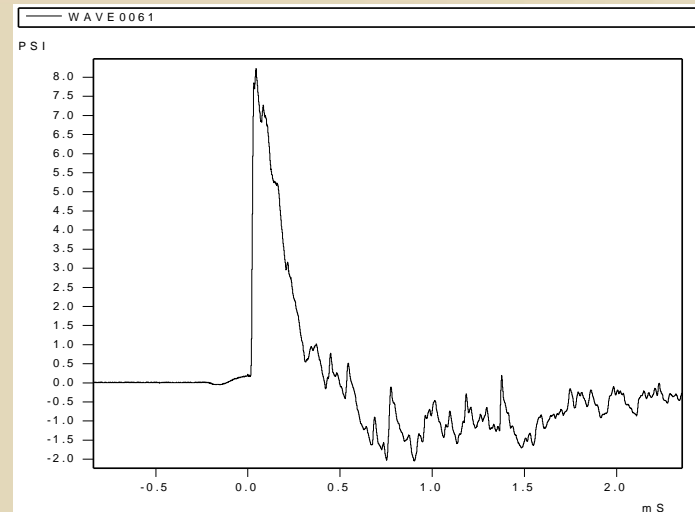
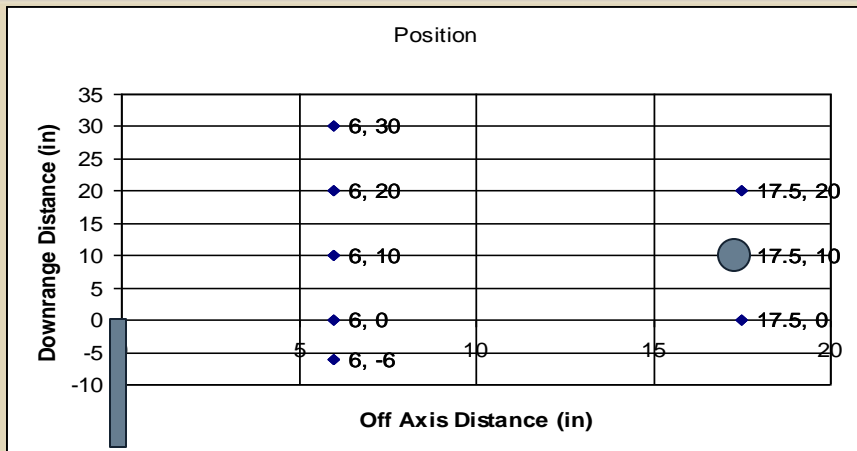


Table 1. Raw Data

Test	Peak Incident (Side-On) Overpressure (psig)	Positive Phase Duration (ms)	Incident Impulse (psi-ms)
61	8.225	0.394	1.375
62	7.585	0.353	1.340
63	7.876	0.416	1.357

Table 2. Some Calculated Data

Test	Reflected Overpressure	Incident Impulse (psi-ms)	Calculated Equivalent Weight of TNT (lbs)
61	20.14	1.375	0.004139
62	18.20	1.340	0.003619
63	18.93	1.357	0.003813



- Biggs, Introduction to Structural Dynamics, MIT, 1964
 - Assumed undamped linear spring-mass system

$$DLF = \frac{y}{y_{st}}$$

- Generates a General Response Equation

$$y = y_0 \cos \omega t + \frac{\dot{y}_0}{\omega} \sin \omega t + y_{st} \omega \int_0^t f(\tau) \sin \omega(t - \tau) d\tau$$

- For Triangular Force Input,

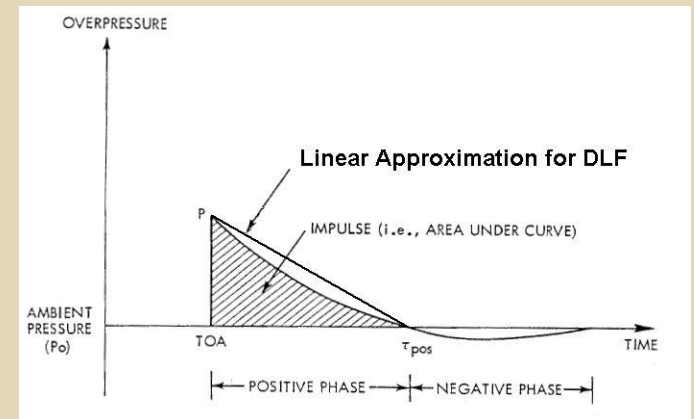
$$f(\tau) = 1 - \frac{\tau}{t_d}, t \leq t_d$$

$$f(\tau) = 0, t \geq t_d$$

- Substituting, Integrating and Simplifying,

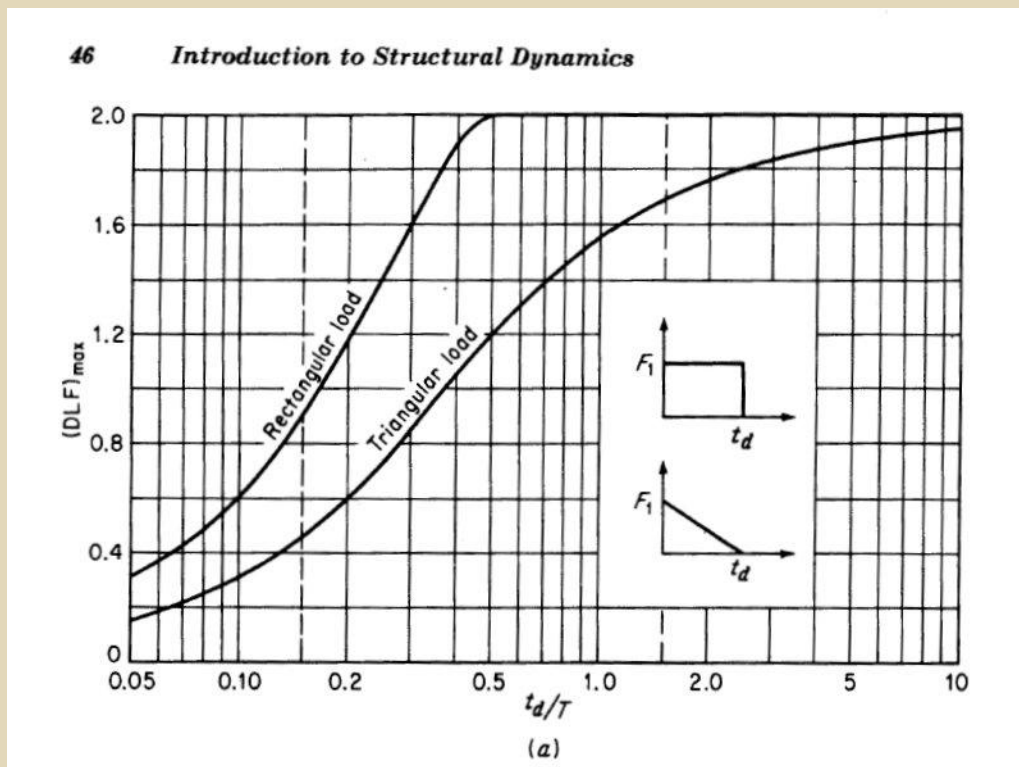
$$DLF = 1 - \cos \omega t + \frac{\sin \omega t}{\omega t_d} - \frac{t}{t_d}, t \leq t_d$$

$$DLF = \frac{1}{\omega t_d} \left[\sin \omega t - \sin \omega(t - t_d) \right] \cos \omega t, t \geq t_d$$



Dynamic Load Factor (DLF)

- Differentiating, equating to 0 and plotting versus t_d/T ,



Right Side
 $(t_d/T) > 5$



Left Side
 $t_d/T < 0.1$

- **Required Values**

- **From Pressure Measurements**

- T_d = Positive Phase Duration
- P_r = Peak Dynamic Pressure applied to surface

- **From Structure**

- T_n = Natural Period

- » Reference (d) gives a formula to determine the natural frequency of a flat plate with all of the edges fixed or simply supported (Table 36; cases 15&16):

$$f = \frac{K_1}{2\pi} \sqrt{\frac{Dg}{wa^4}}$$

where, $K_1=23.6$ for a rectangular plate with fixed edges and $K1 = 11.5$ for rectangular plate with simply supported edges

E = Modulus of Elasticity for material

ν = Poisson's Ratio for the material

g = gravitational constant

w = unit load per unit area including weight of plate

a = length of short edge of plate

GAU21/H-60S on full rear train



- Impinges on an 18" X 7.25" panel
 - $T_n = 3.88$ ms for fixed edges
 - $T_n = 7.97$ ms for dimply supported edge
- Worst pressure case from GAU-21 testing
 - $P_r = 20.14$ psi
 - $T_d = 0.394$ ms
- $T_d/T_n = 0.102$ for Fixed $DLF_{max} = 0.33$
- $T_d/T_n = 0.049$ for Simple $DLF_{max} = 0.17$

Equivalent Static Pressure

- $P_{eq} = P_r * DLF_{max}$
- **Fixed Edges**
 - $P_{eq} = 20.14 \text{ psi} * 0.33 = 6.65 \text{ psi}$
- **Simply Supported Edged**
 - $P_{eq} = 20.14 \text{ psi} * 0.17 = 3.42 \text{ psi}$



Alternatives and Caveats

- **Alternative - Dynamic FEA**
- **Only the simplest of structures can be hand cranked. FEA may be inevitable.**
- **Doesn't take into account flexing of the supporting structure.**
- **Pressure profiles for weapons are hard to come by and do not match pressure versus distance equations for explosives**



Conclusions

- That's why helicopters don't fall out of the sky when they fire their weapons.





Thank you for your time and attention!

For more information on NSWC Crane, please visit www.crane.navy.mil

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