



Physics-Based Modeling and Simulation of Shock-to-Detonation Transition in Energetic Materials

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Physics-based Modeling In Design & Development for U.S. Defense Conference

Promoting National Security Since 1919

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Outline

- *IMSim* Infrastructure
 - Insensitive Munitions Simulation package
- *Rocpack*
 - Models the microstructure
 - Validation
- *RocSDT*
 - Shock-to-detonation physics code
 - Verification
 - Examples

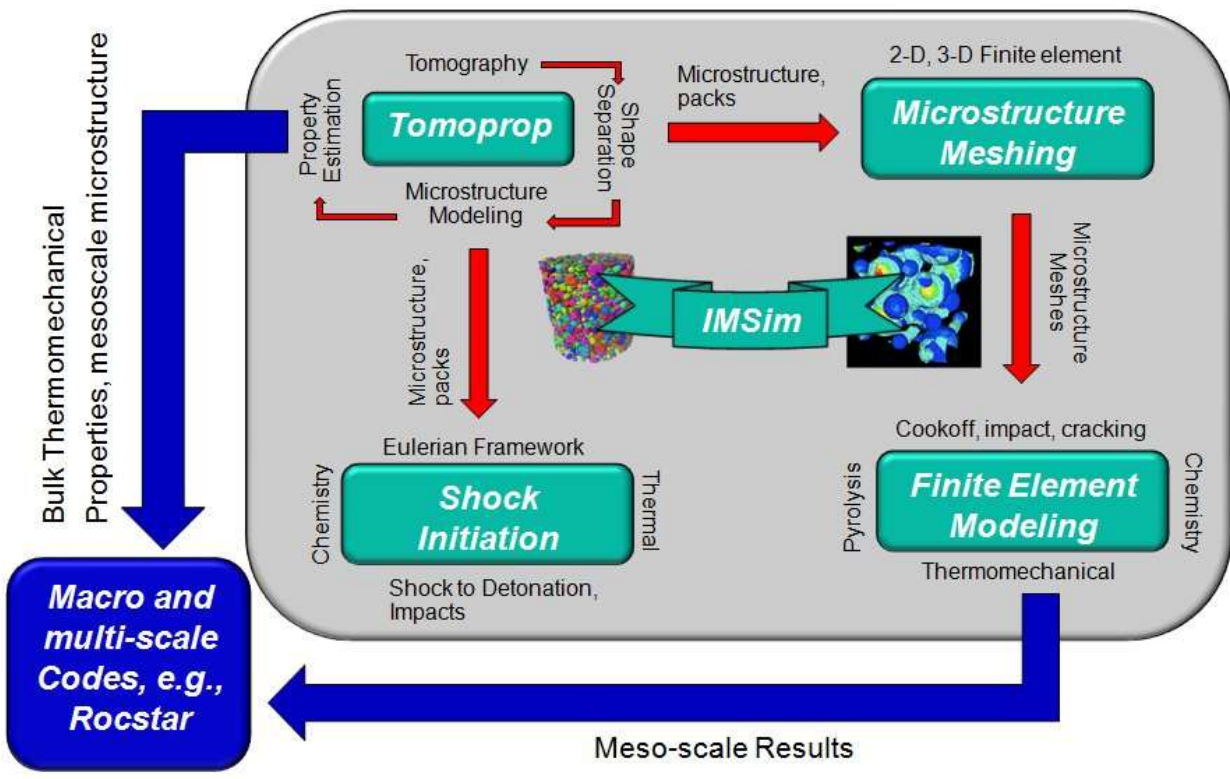


Insensitive Munitions and *IMSim*

Characterization

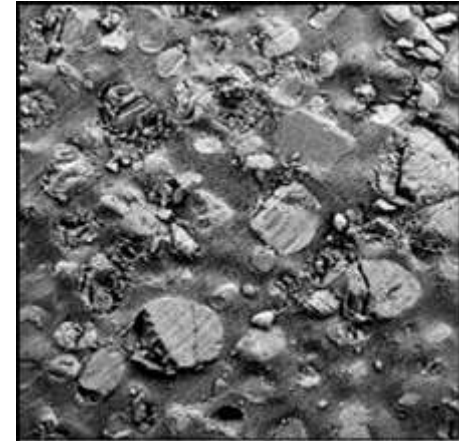
Fast and Slow Cookoff

Bullet and Fragment Impact

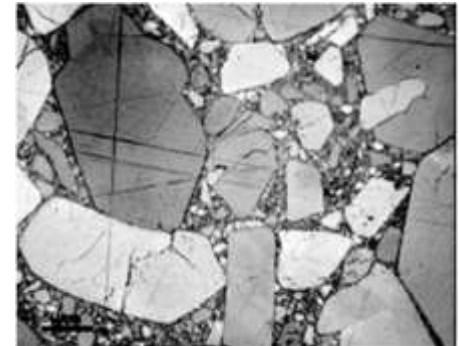


Issues with Energetic Materials

- Shock sensitivity of energetic materials
 - Material defects can augment shock sensitivity
 - Geometric effects (voids, crystal shape, binder) are important
- Modeling the microstructure is important for predictive simulations
 - Homogeneous modeling not predictive
- Difficulties at the mesoscale
 - Complex geometry
 - Multi-material interfaces
 - Complex chemical reaction pathways
- Goal
 - Develop virtual engineering infrastructure to predict properties and dynamics of shock-induced initiation in energetic materials



AP/HTPB Solid Propellant



PBX9501 (C. Skidmore, LANL)

Value Proposition

- Mesoscale structures and effects control the response of energetic materials
- IMSim tools, when complete will allow
 - Analyzing existing materials to explain observed effects
 - Designing new materials to tailor predicted properties and IM response before formulation and testing
- Replace “some” of the make-and-break cycle
- Produce detailed mesoscale response and effects for input to macroscale simulation tools
 - IllinoisRocstar’s *Rocstar Simulation Suite*
 - Other shock physics, FEA, CFD codes



Microstructure Modeling

- Rocpack packing code
- Microtomography data for real energetic materials

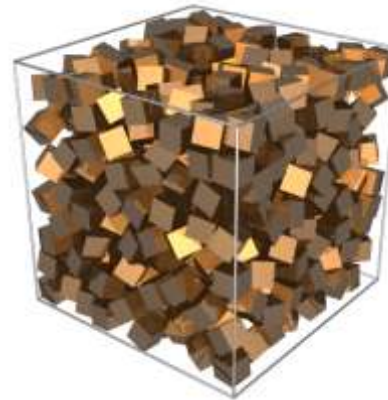
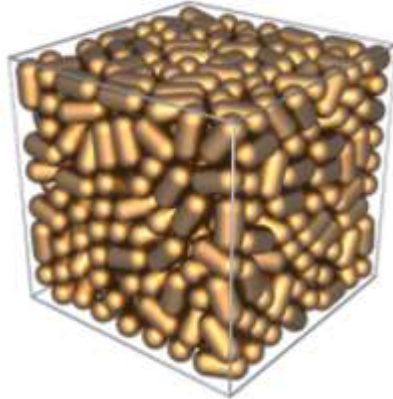
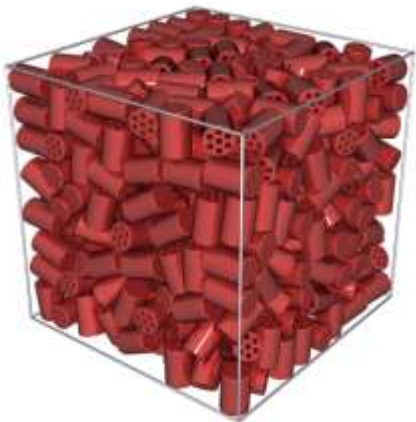
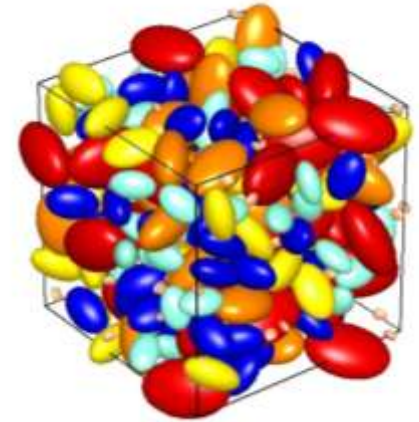
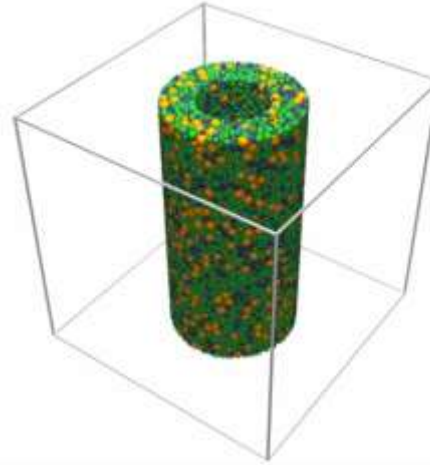
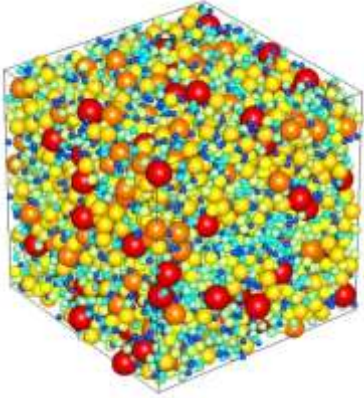


Rocpack

- *Rocpack* is based on the concurrent packing algorithm described by Lubachevsky and Stillinger, J. Stat. Phys. 1990
- Spheres of zero initial radius with random locations and velocities grow in a box at a prescribed growth rate a_i
- Stopping criterion
 - specified packing fraction
 - jammed



Shapes generated by *Rocpack*



Modeling Crystals for Energetic Materials Using *Rocpack*

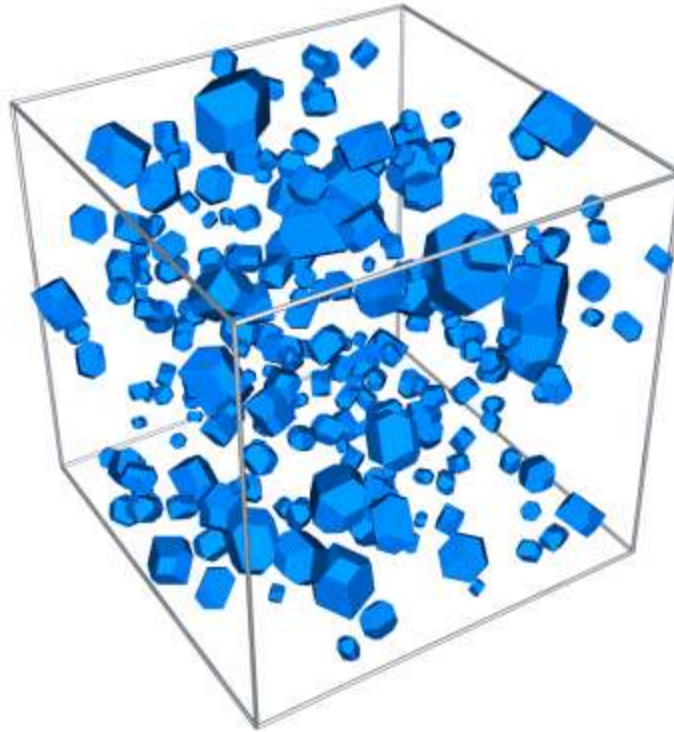
- Sphere packing algorithm extended to include crystals using level sets to describe the shapes



- Stafford, D.S. and Jackson, T.L. (2010) Using level sets for creating virtual random packs of non-spherical convex shapes. *Journal of Computational Physics*, Vol. 229, pp. 3295-3315.
- Jackson, T.L., Hooks, D.E., and Buckmaster, J. (2011) Modeling the Microstructure of Energetic Materials with Realistic Constituent Morphology. *Propellants, Explosives, Pyrotechnics* (in press).



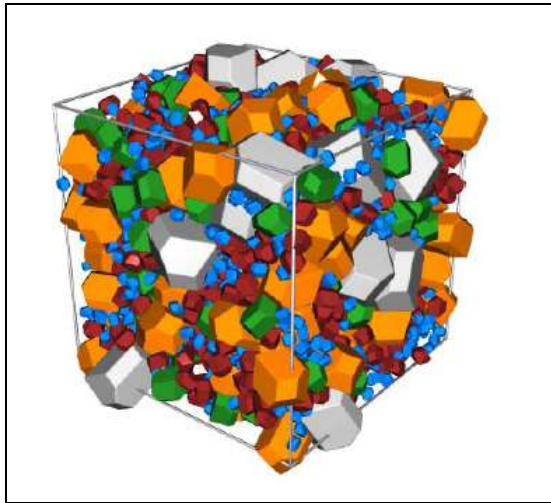
Rocpack Crystal Packing



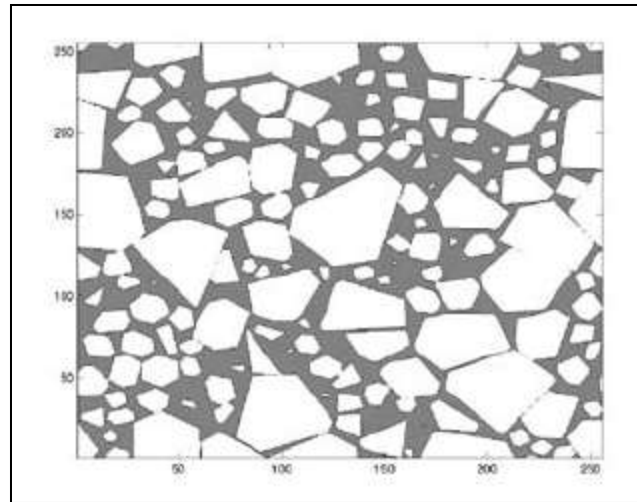
250 total HMX crystals
10 different particle sizes [55, 281] microns
Frames stopped at volume fraction 0.68

Computational Crystal Pack

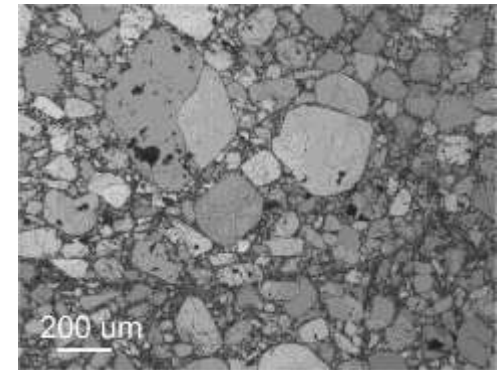
- Example: Low-density unpressed HMX (68%) pack
- Figure shows 3-D pack (each size colored differently) and a 2-D slice through the 3-D pack



3-D

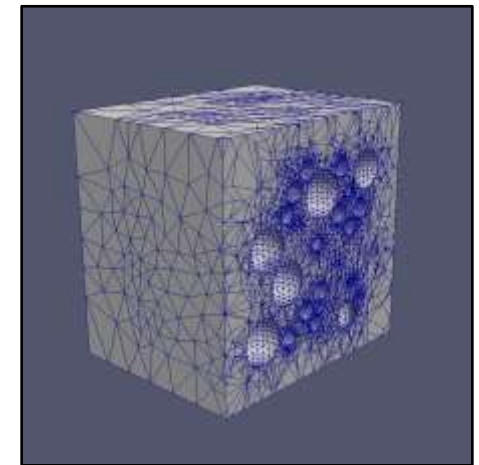
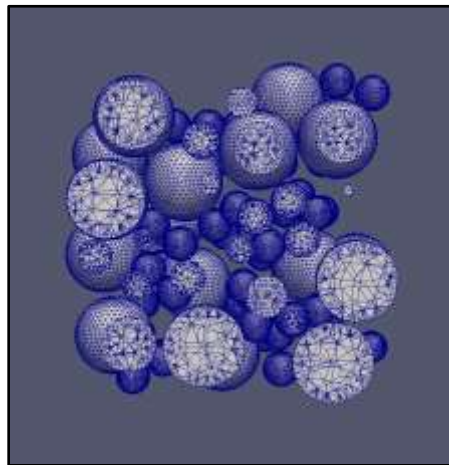
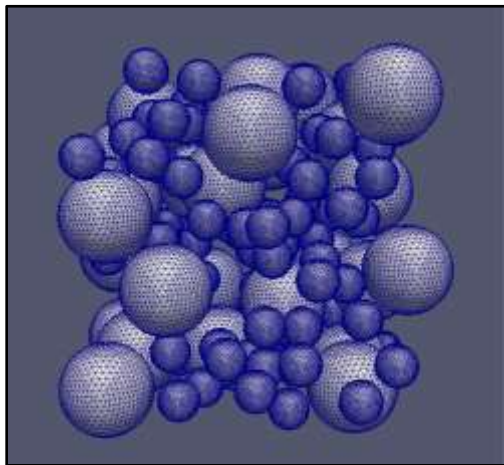
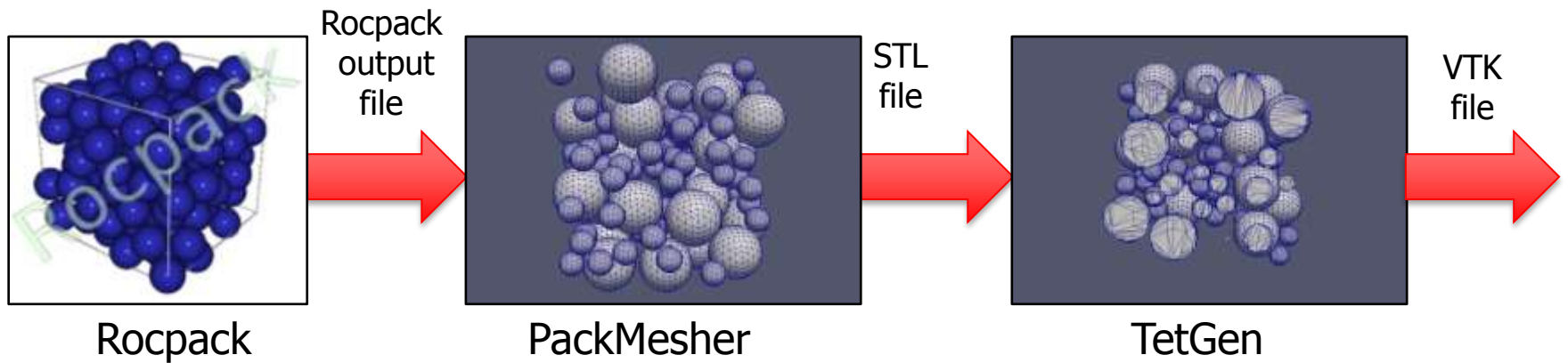


2-D slice



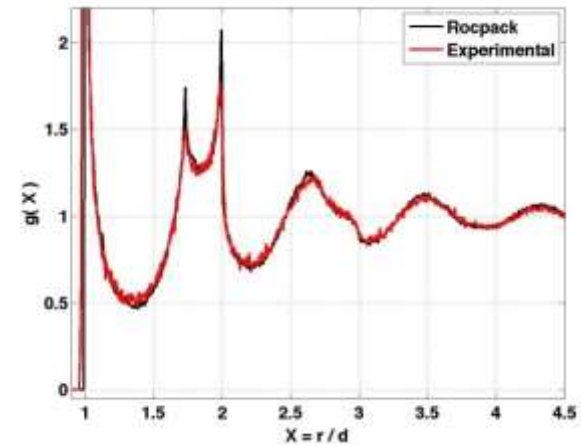
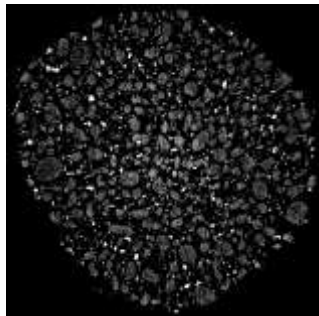
Plastic bonded explosive
(HMX 95%, 5% binder)

PackMesher



- Currently supports separated spheres and tetrahedral mesh
- Extending to all other *Rocpack* shapes and shapes that touch

Validation of *Rocpack*

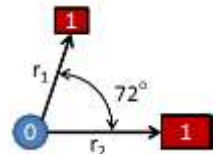
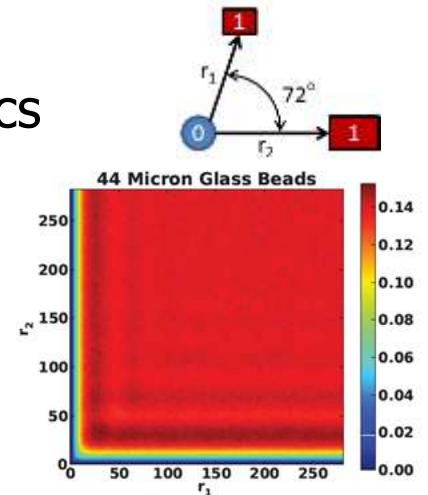
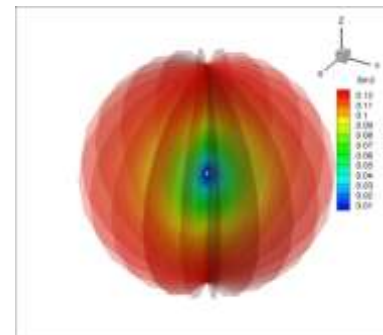
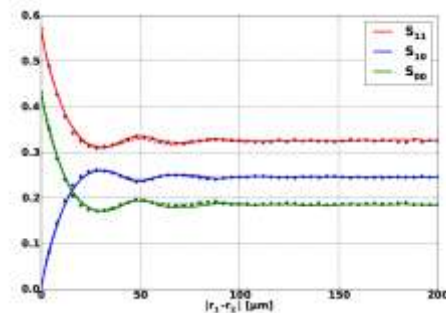
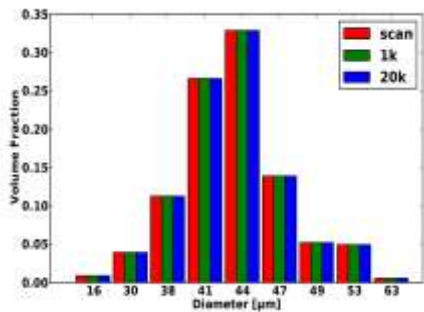


Radial distribution function

Tomography

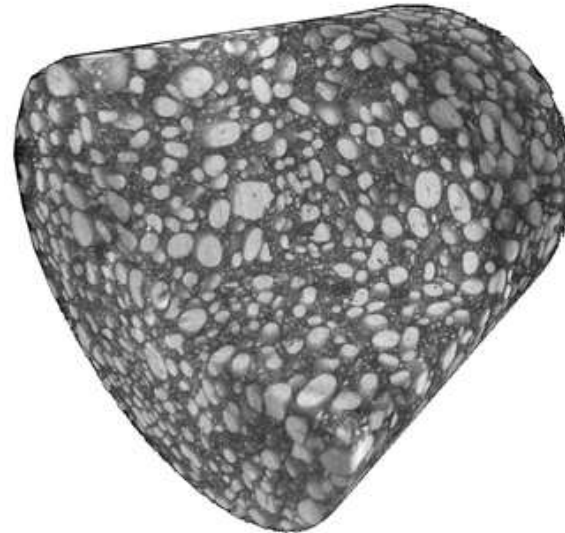
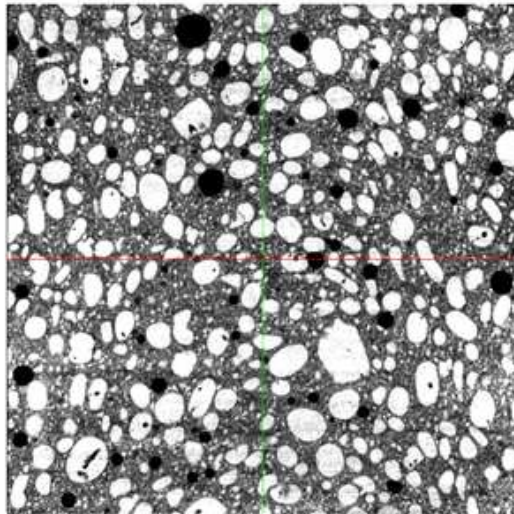
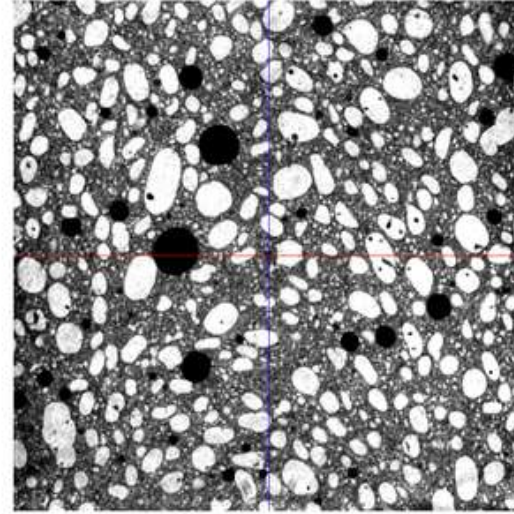
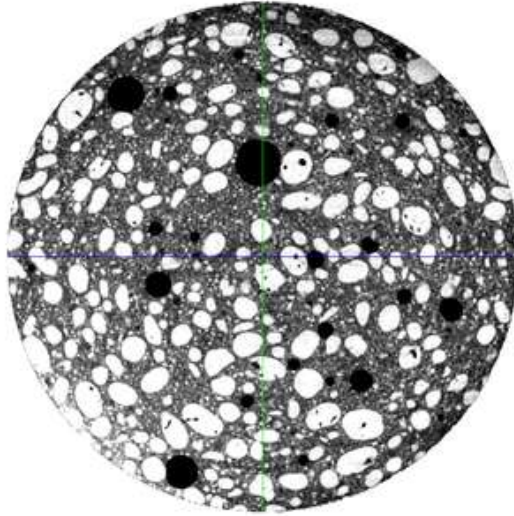
Validation data or directly for packs

Compare first, second, and third-order statistics



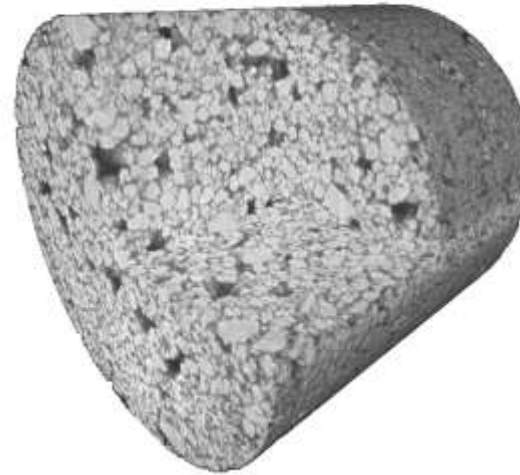
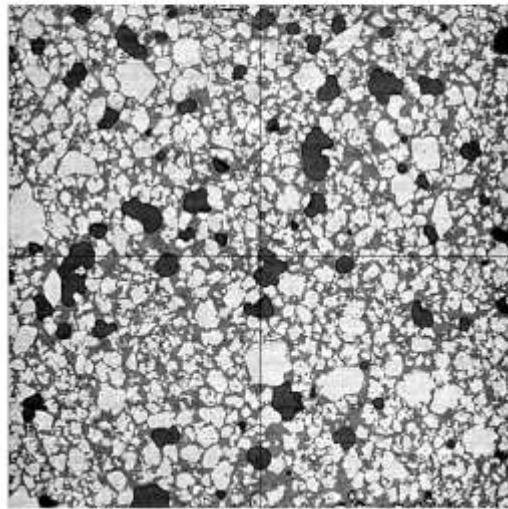
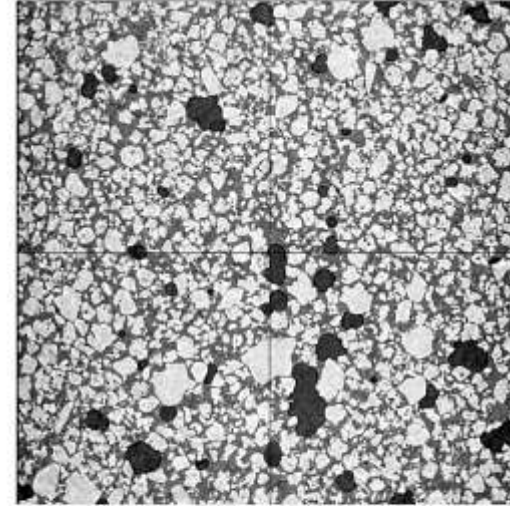
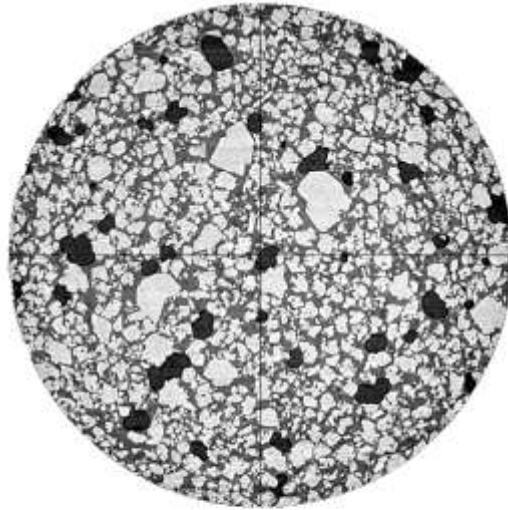
AP/HTPB

80% 200 micron AP; 1:1 fine to coarse; 20% HTPB



CL20/HTPB

80% 200 micron AP; 1:1 fine to coarse; 20% HTPB



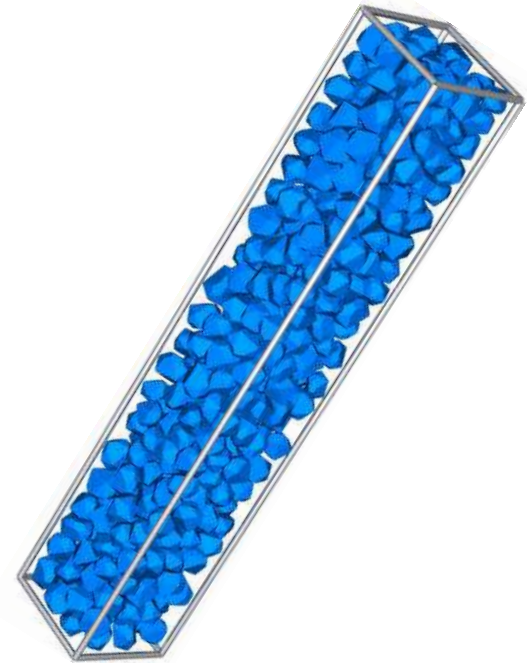
Shock to Detonation Modeling

- Code status
- Background
- Verification
- Borne data comparison



RocSDT

- Three-dimensional compressible reactive flow solver for explosives
- Current characteristics of *RocSDT*
 - Strong shocks ✓
 - Sharp material interfaces ✓
 - High density ratios (voids) ✓
 - Multiple EOS ✓
 - Kinetics/Chemistry
 - Microstructure from *Rocpack* ✓
 - Material deformation
 - Three-dimensional ✓
 - Parallel using MPI ✓



Pack of HMX crystals produced by *Rocpack*

Zhang, J, Jackson, T.L., Buckmaster, J.D., and Freund, J.B (2012) "Numerical Modeling of Shock-to-Detonation Transition in Energetic Materials," recently accepted in *Combustion & Flame*.

Governing Equations

- Reactive Euler equations

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0$$

$$\frac{\partial(\rho \mathbf{u})}{\partial t} + \nabla p + \nabla \cdot (\rho \mathbf{u} \mathbf{u}) = 0$$

$$\frac{\partial E}{\partial t} + \nabla \cdot ((E + p) \mathbf{u}) = Q \Omega$$

$$\frac{\partial(\rho Y)}{\partial t} + \nabla \cdot (\rho \mathbf{u} Y) = -\Omega$$

$$\Omega = Da \rho Y e^{-E_a/R_u T}$$

$$E = \rho \left(e + \frac{1}{2} \mathbf{u} \cdot \mathbf{u} \right)$$

- Multiple Equations of State (ideal, stiffened, Mie-Gruneisen)



Maintain Sharp Interfaces

- Interface capturing method; Φ is a material marker
 - Changes over small number of mesh points near interfaces

$$\frac{\partial \phi}{\partial t} + \mathbf{u} \cdot \nabla \phi = 0$$

Move interface using this...

$$\frac{\partial \phi}{\partial \tau} = \mathbf{n} \cdot \nabla (\epsilon_h |\nabla \phi| - \phi(1 - \phi))$$

Correct interface position each timestep using this...
 τ =pseudo time
 \mathbf{n} =normal vector

- Density compression:

$$\frac{\partial \rho}{\partial \tau} = H(\phi) \mathbf{n} \cdot (\nabla (\epsilon_h \mathbf{n} \cdot \nabla \rho) - (1 - 2\phi) \nabla \rho)$$

- Temperature and mass fraction compressions:

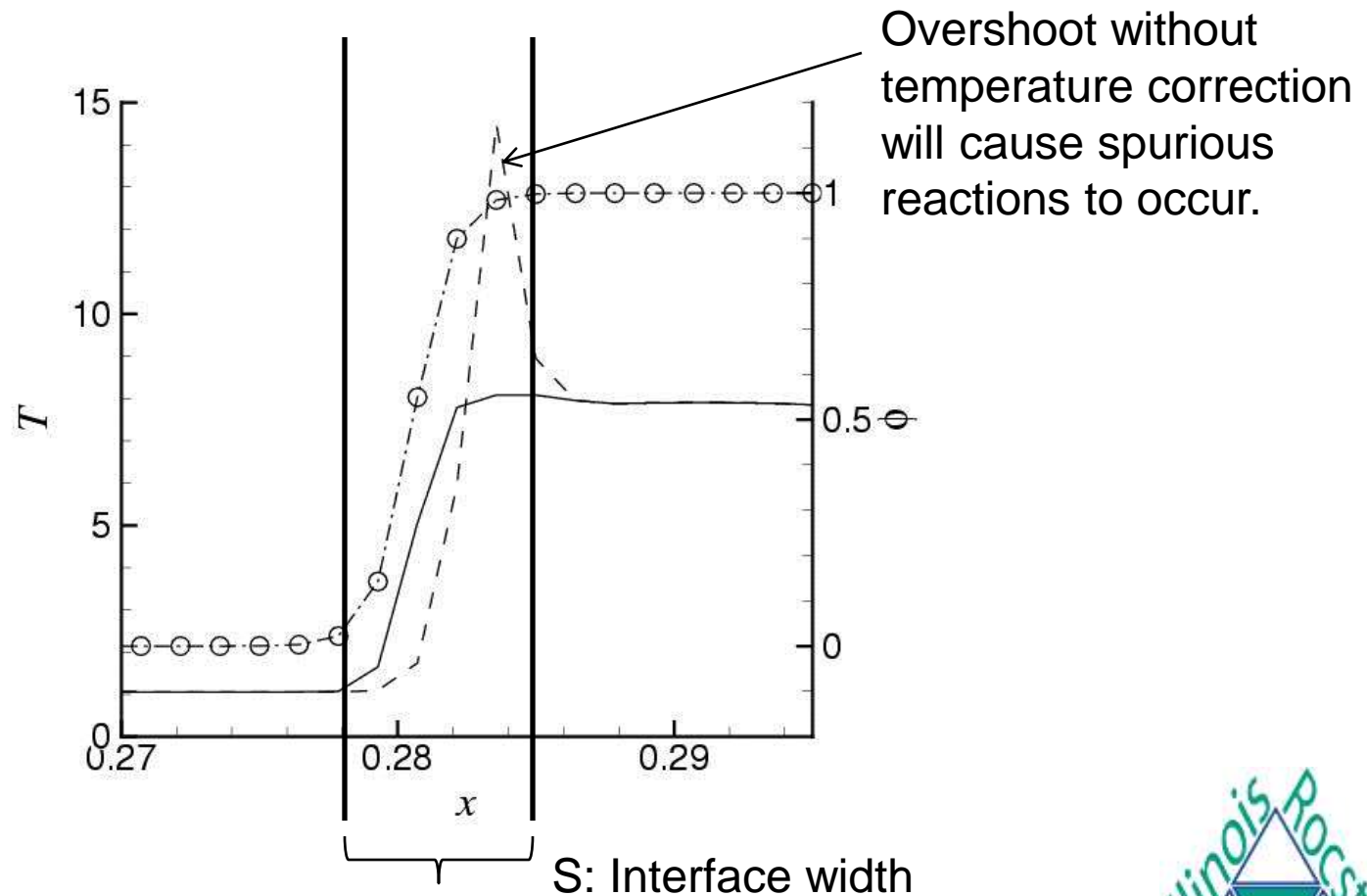
$$\frac{\partial T}{\partial \tau} = H(\phi) \mathbf{n} \cdot (\nabla (\epsilon_h \mathbf{n} \cdot \nabla T) - (1 - 2\phi) \nabla T)$$

$$\frac{\partial Y}{\partial \tau} = H(\phi) \mathbf{n} \cdot (\nabla (\epsilon_h \mathbf{n} \cdot \nabla Y) - (1 - 2\phi) \nabla Y)$$



Temperature Correction

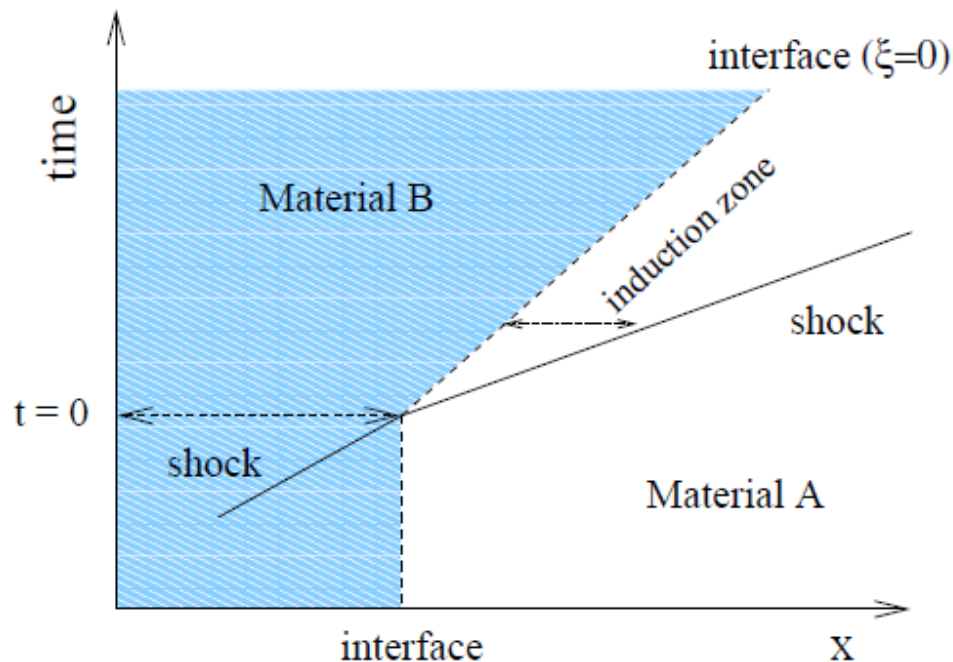
- Comparison of temperature profile with (solid) and without (dash) temperature correction
- Dash/circles denote location of material interface ϕ



Verification of *RocSDT*

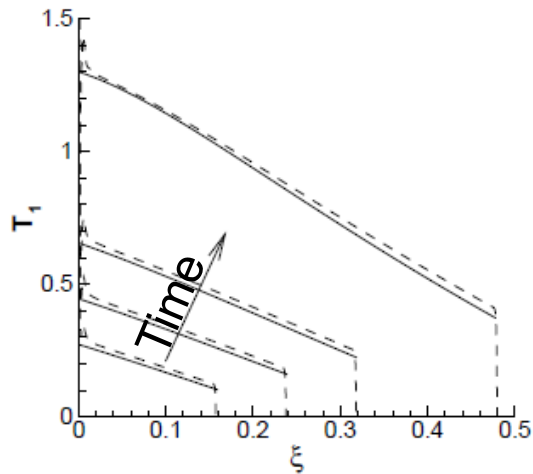
Shock-Material Interface

- Assume shock is strong enough to raise temperature between shock and interface to an ignition temperature T_0 , thereby switching on chemical reaction
- The induction zone defined to lie between the shock and the (moving) material interface

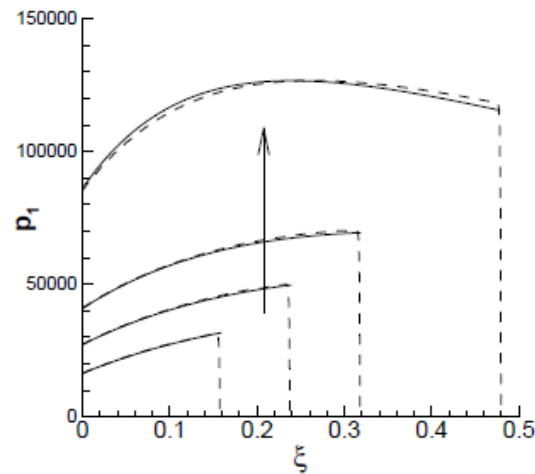


Results for Shock-Material Interface (1)

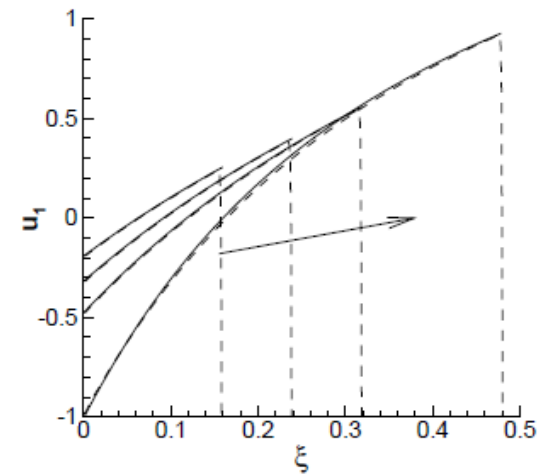
- Form non-dimensional perturbation solution
- Comparison of perturbation temperature, pressure, and velocity in the induction zone using stiffened EOS
 - Asymptotic solutions: solid
 - RocSDT: dash
 - ξ = non-dimensional interface position



(d) Stiffened; Temperature



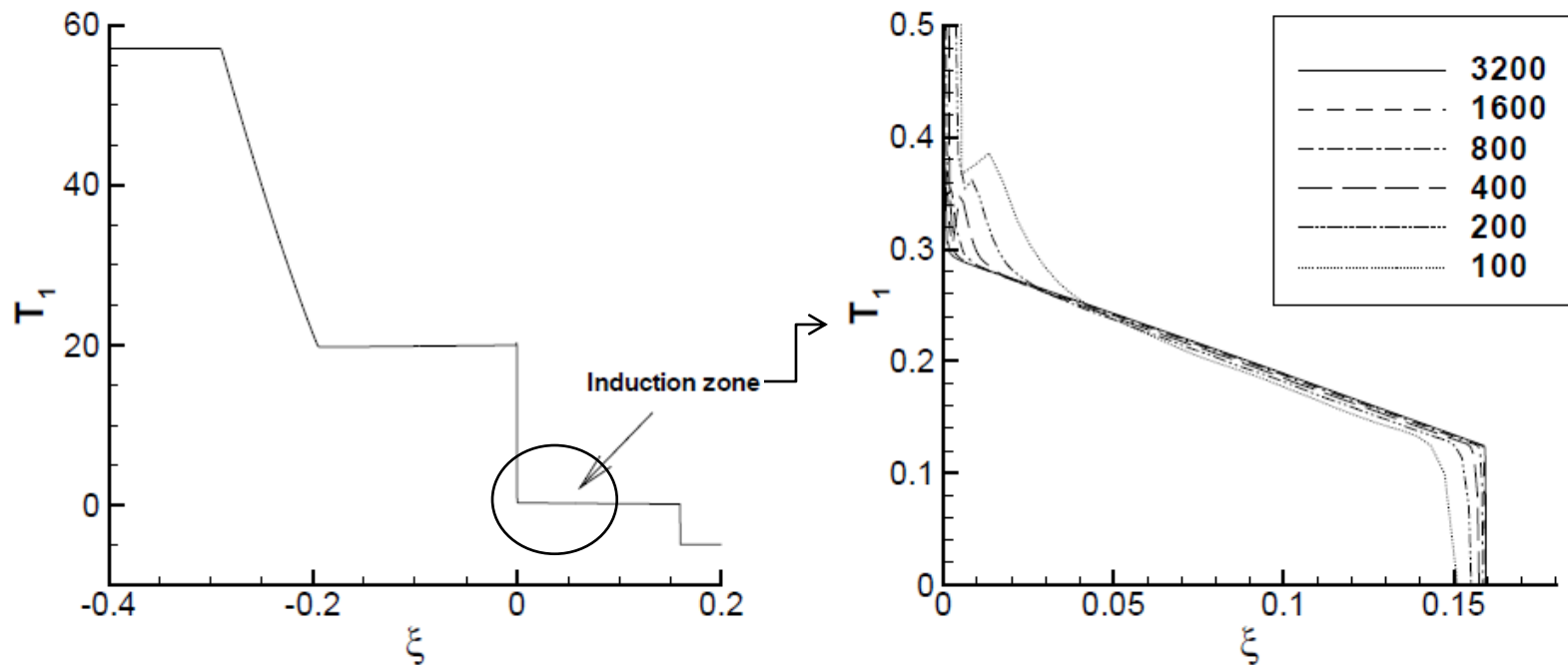
(e) Stiffened; Pressure



(f) Stiffened; Velocity

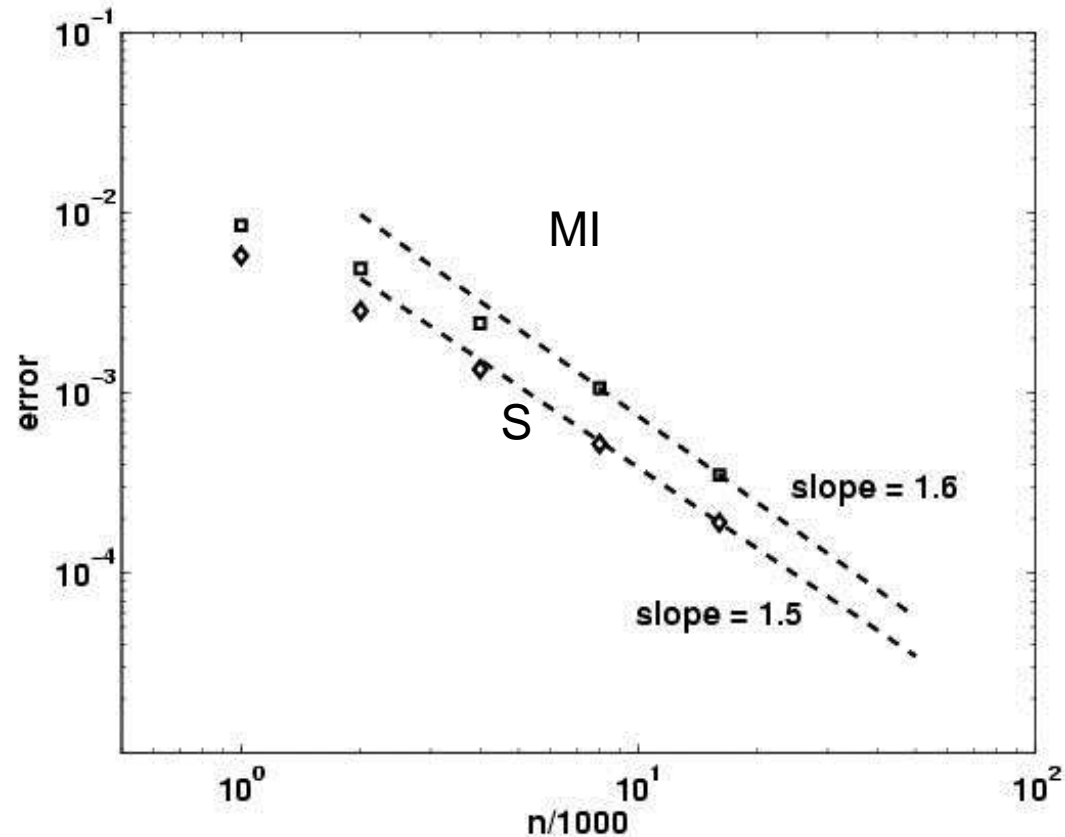
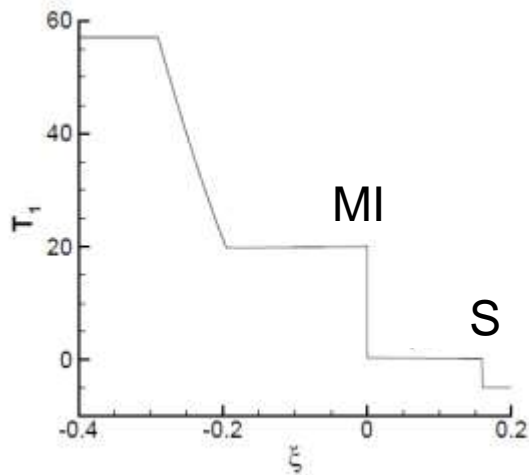
Results for Shock-Material Interface (2)

- Grid resolution study showing grid convergence of perturbation temperature
- T_1 is the perturbation temperature



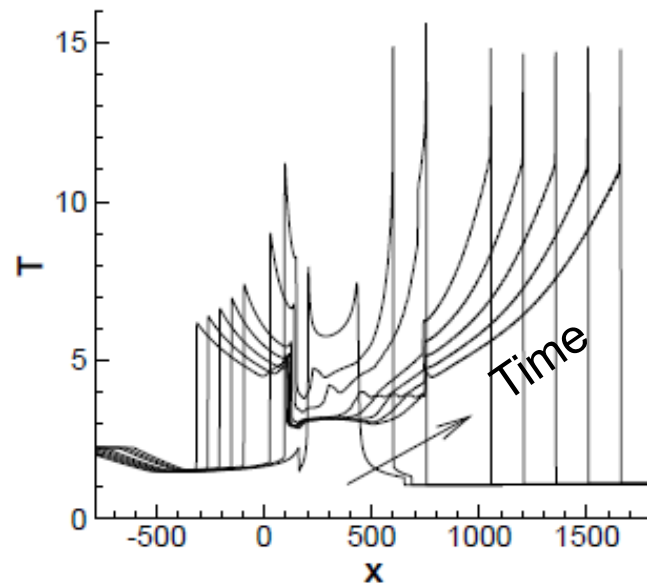
Results for Shock-Material Interface (3)

- Convergence rate of perturbation temperature as a function of n (number of grid points) at material interface (square) and shock location (diamond)
- Relative error in maximum perturbation temperature

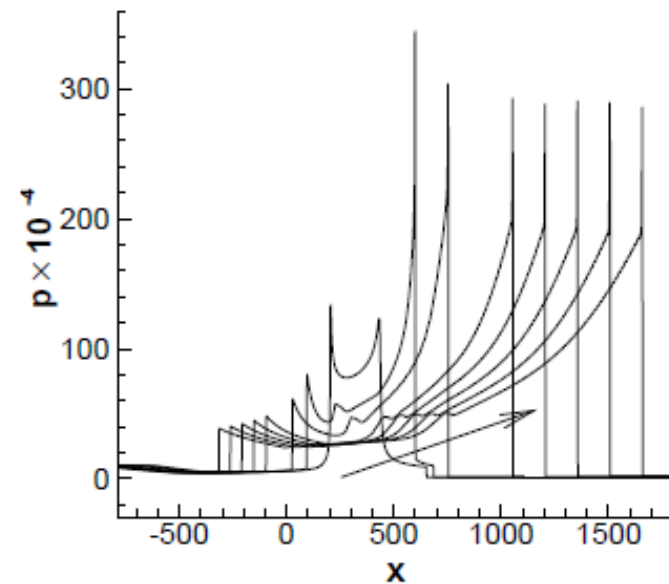


Results for Shock-Material Interface (4)

- Transition to detonation
 - The peaks are within 4% of those obtained on a grid with four times the resolution
 - CJ states captured to within 1%
 - Transition to detonation around $x=600$



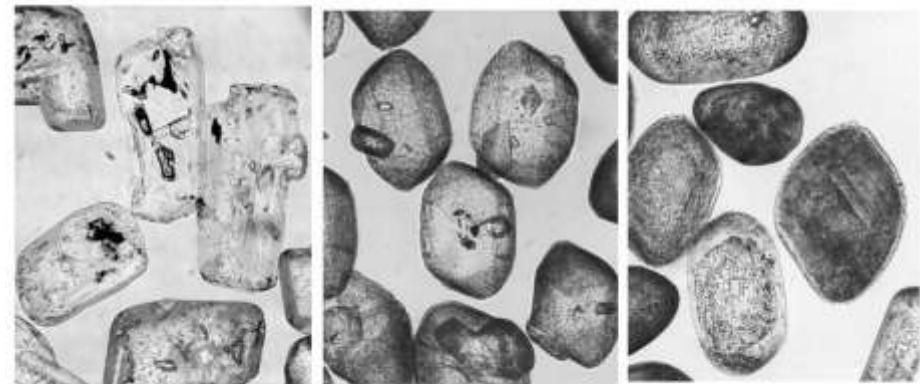
Temperature



Pressure

Example: Borne Experiment

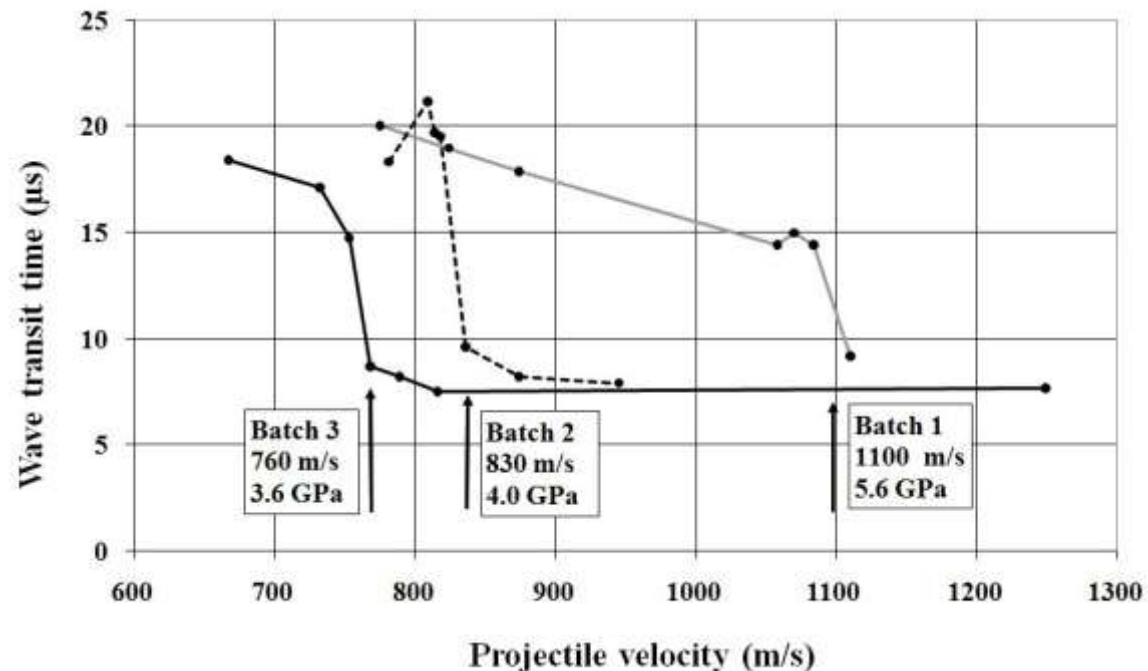
- Borne (1982)
 - Experimental investigation of HMX crystals in wax
 - Projectile against plate to introduce shock
- Void content varied
 - 0.1% (Batch 1)
 - 0.5% (Batch 3)
- Experimentally measured velocity threshold for detonation; function of crystal impurity



Batch 1

Batch 2

Batch 3



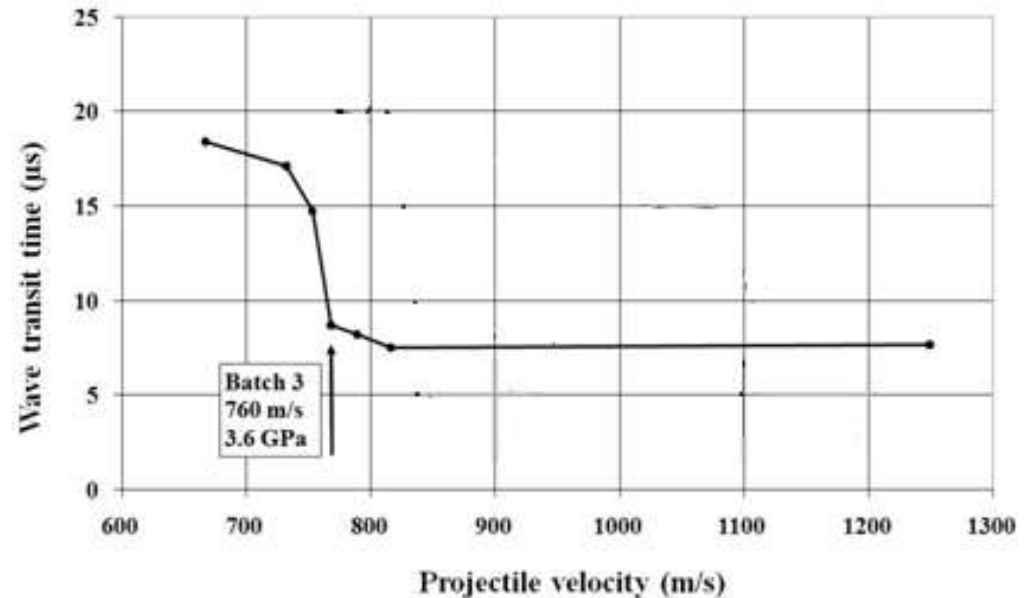
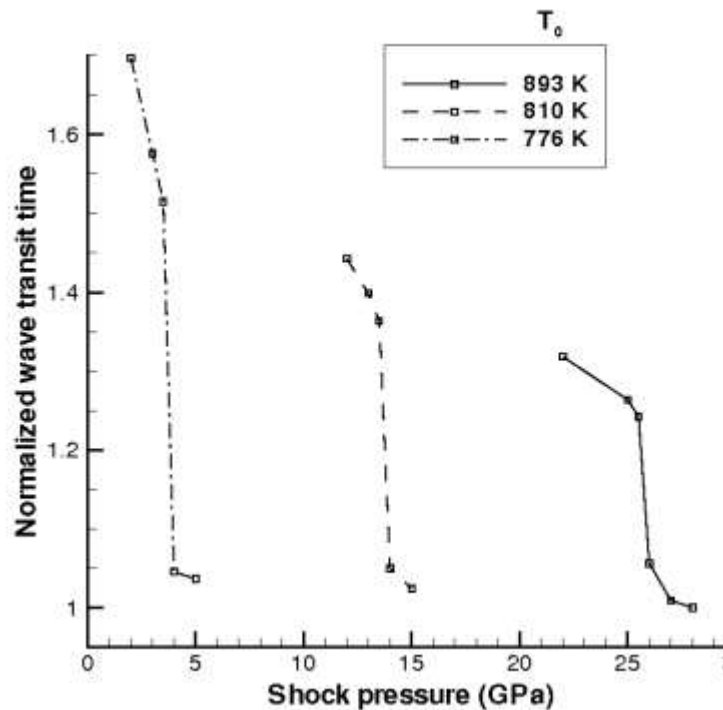
Periodic Single Void Model

- Borne's experiments suggests that hot spot formation due to void collapse is an important ingredient for transition to detonation
- Numerical experiment with current capabilities
 - One-step global kinetics
 - We mimic the experiment by modeling hot spots as a periodic array in an infinite slab of HMX
 - Vertical distance between hot spots corresponds roughly to volume percent of voids in HMX crystals
 - 2 μm diameter hot spot



Example: Borne Experiment (1)

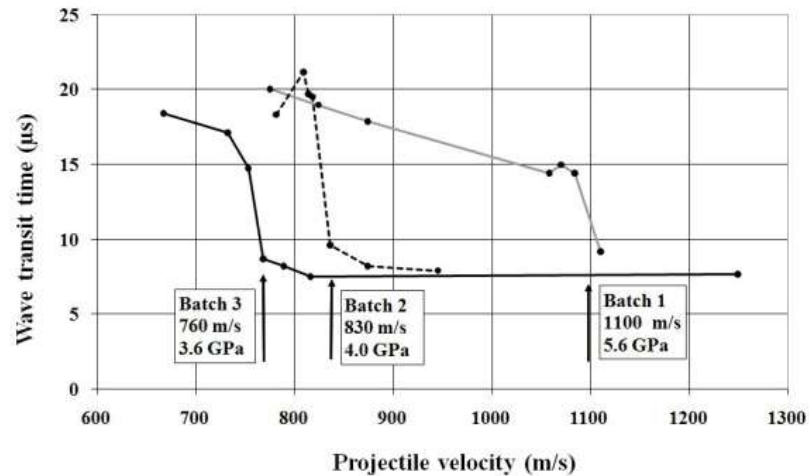
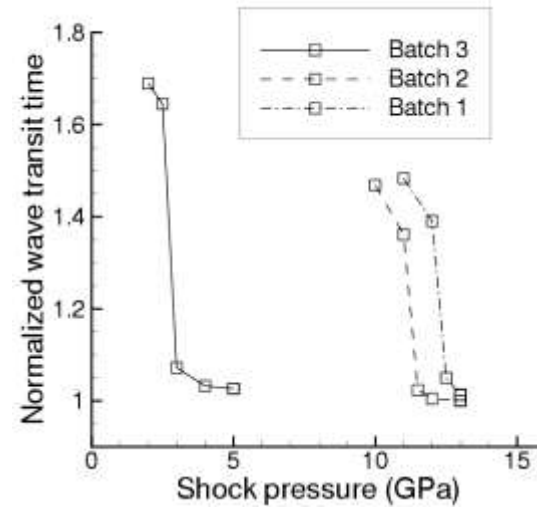
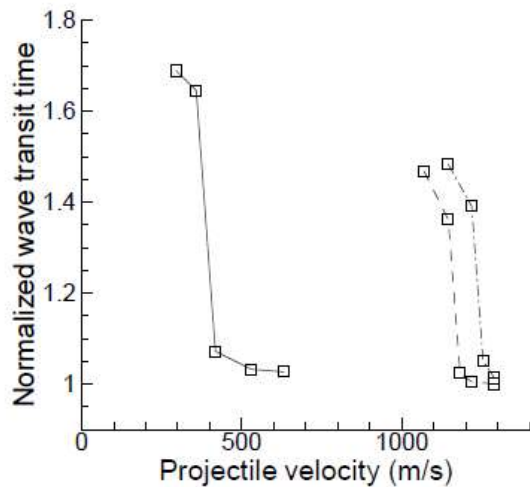
- T_0 (the ignition temperature) is calibrated for Batch 3; held fixed for batches 1 and 2



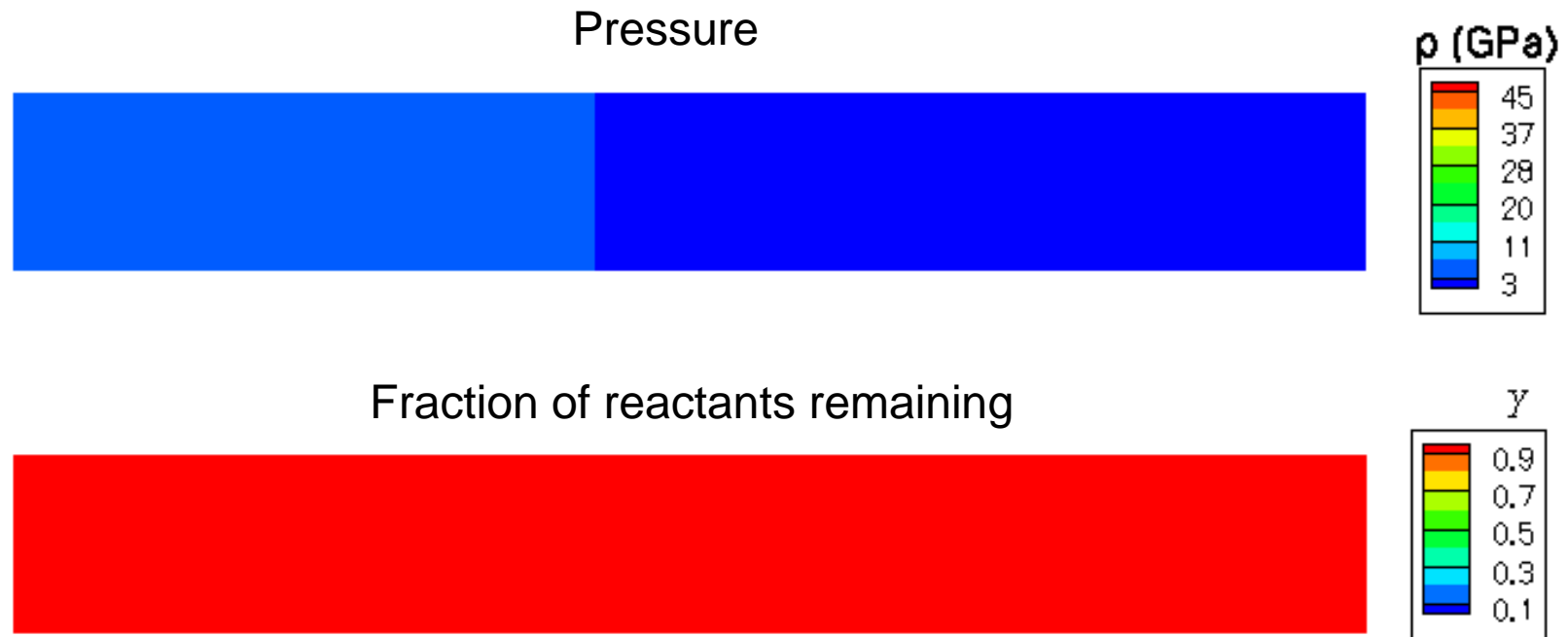
Results for Batch 3
Effect of changing T_0

Example: Borne Experiment (2)

- Numerical simulations qualitatively reproduce experimental trend

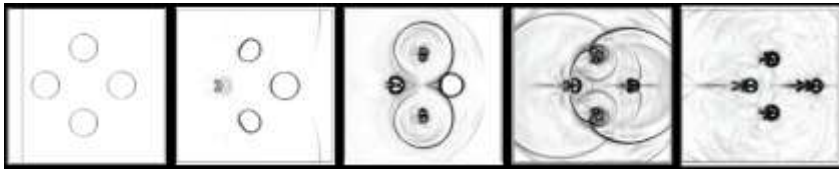


Pressure and Species Contours for Batch 3

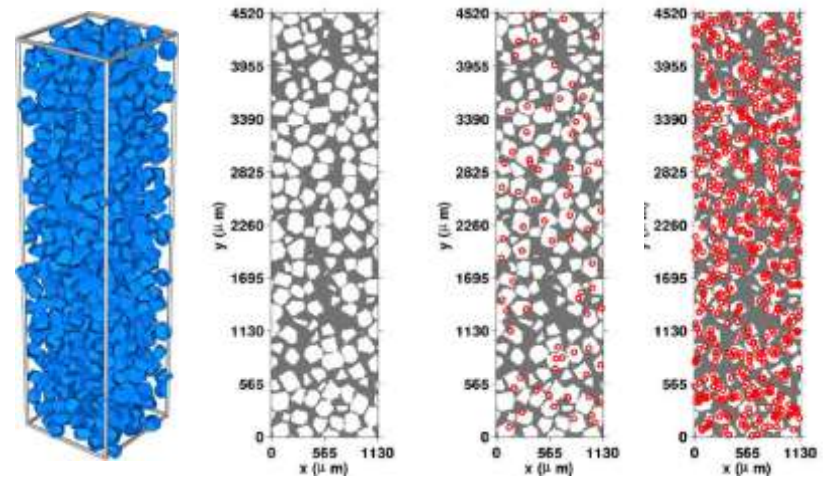


Example: Statistical Hot Spot Model

- Due to grid considerations, it is not possible to resolve both void collapse and heterogeneity at the same time
- Adopt a subgrid modeling approach
 - Subgrid : Simulate a small collection of voids
 - Mesoscale: Use data as input for a statistical hot spot model at the crystal/grain level

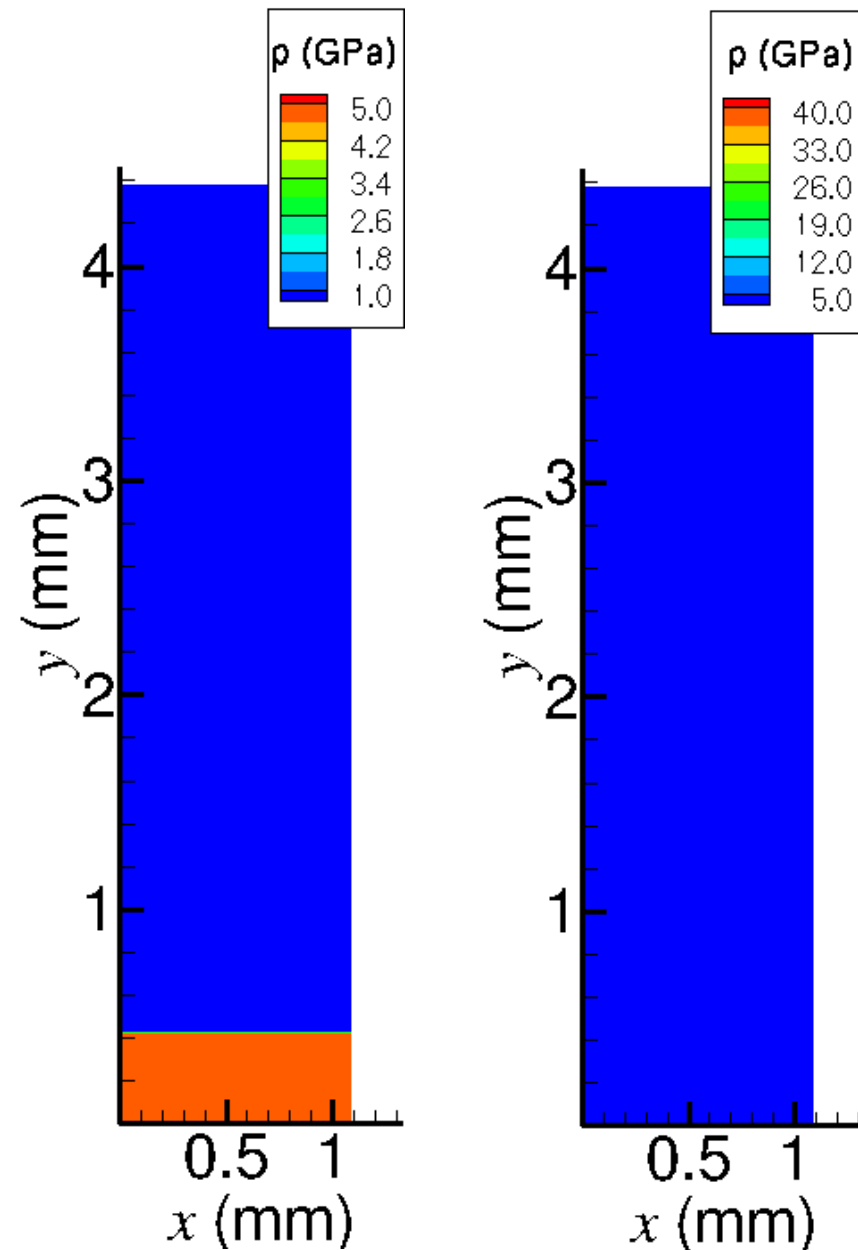


Collapse of four air-filled "voids" by a shock in a stiffened-EOS medium. Numerical Schlieren are plotted.



3-D pack of HMX and corresponding 2-D slices. Also shown are hot spot locations (red circles) for 0.1% and 0.5% voids.

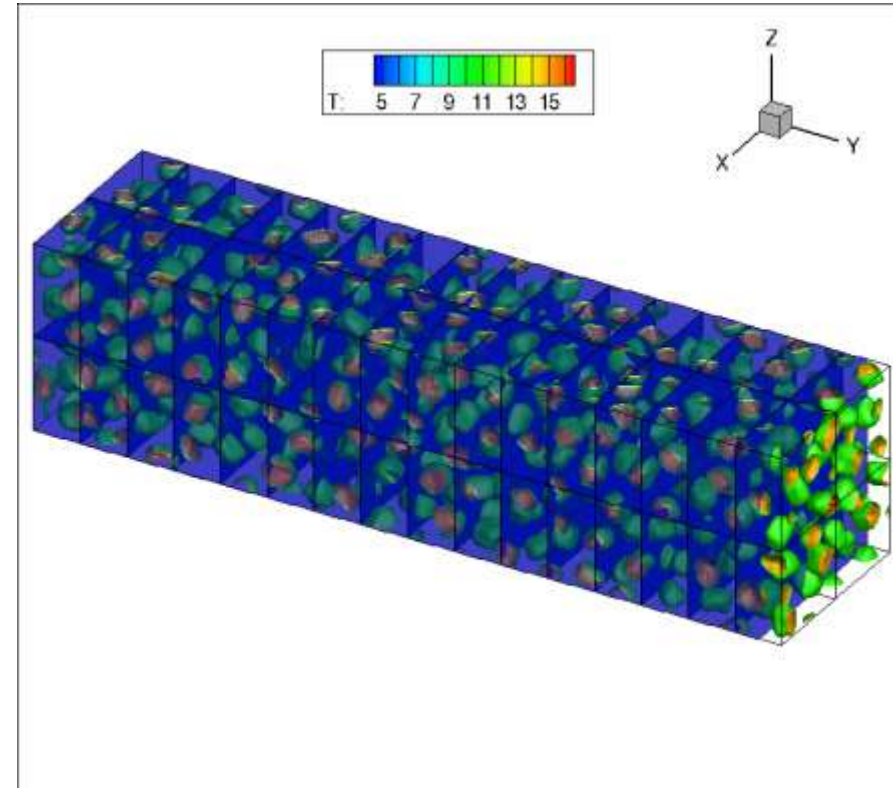
2D Example: Statistical Hot Spot Model



- Pressure fields for 0 (left) and 0.1% (right) void content
- Initial shock 5 GPa
- Sample with higher void content transitions to detonation, in general agreement with Borne (1988)
- Sample without voids does not transition
- Beginning to rerun with new 3-D code

Summary

- Realistic mesoscale microstructures are important for predictive simulations
 - *Rocpack* packs or tomographic scan data may be used
- 2-D *RocSDT* simulations with basic chemistry show qualitative agreement with data
- Interface capturing, density and temperature compression critical to maintaining sharp and stable solution
- 3-D, parallel *RocSDT* under production – will be a core component in *IMSim* infrastructure



Early non-reacting 3-D simulation

Acknowledgements

- This work has been supported by several organizations over 10 years;
 - Department of Energy through the University of Illinois Center for Simulation of Advanced Rockets (Rocpack)
 - An Air Force SBIR through Buckmaster Research (RocSDT)
 - An Air Force SBIR to IllinoisRocstar (RocSDT)
- Continuing work funded by a Phase II SBIR to IllinoisRocstar through Eglin AFB



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Modeling of Void Collapse as Subgrid Component of Mesoscale Simulations

- Mesoscale simulations require the dynamics of void collapse be treated as a subgrid component due to grid resolution constraints
- Goal: Develop a subgrid model for hot spot dynamics that can be incorporated in mesoscale simulations
 - Hot spot model parameters:
 - Ignition delay time
 - Pressure and temperature
 - Time and length scales
 - Void diameter
 - Porosity
 - Etc.
- As an initial effort, we have recently developed a 2-D flow solver with deformation for collapse of single or multiple voids



- Example 1: Wave propagation in heterogeneous medium
 - Propagation of shock through aluminum medium
 - Reflected and transmitted shear and pressure waves observed without spurious oscillations at copper-aluminum interface

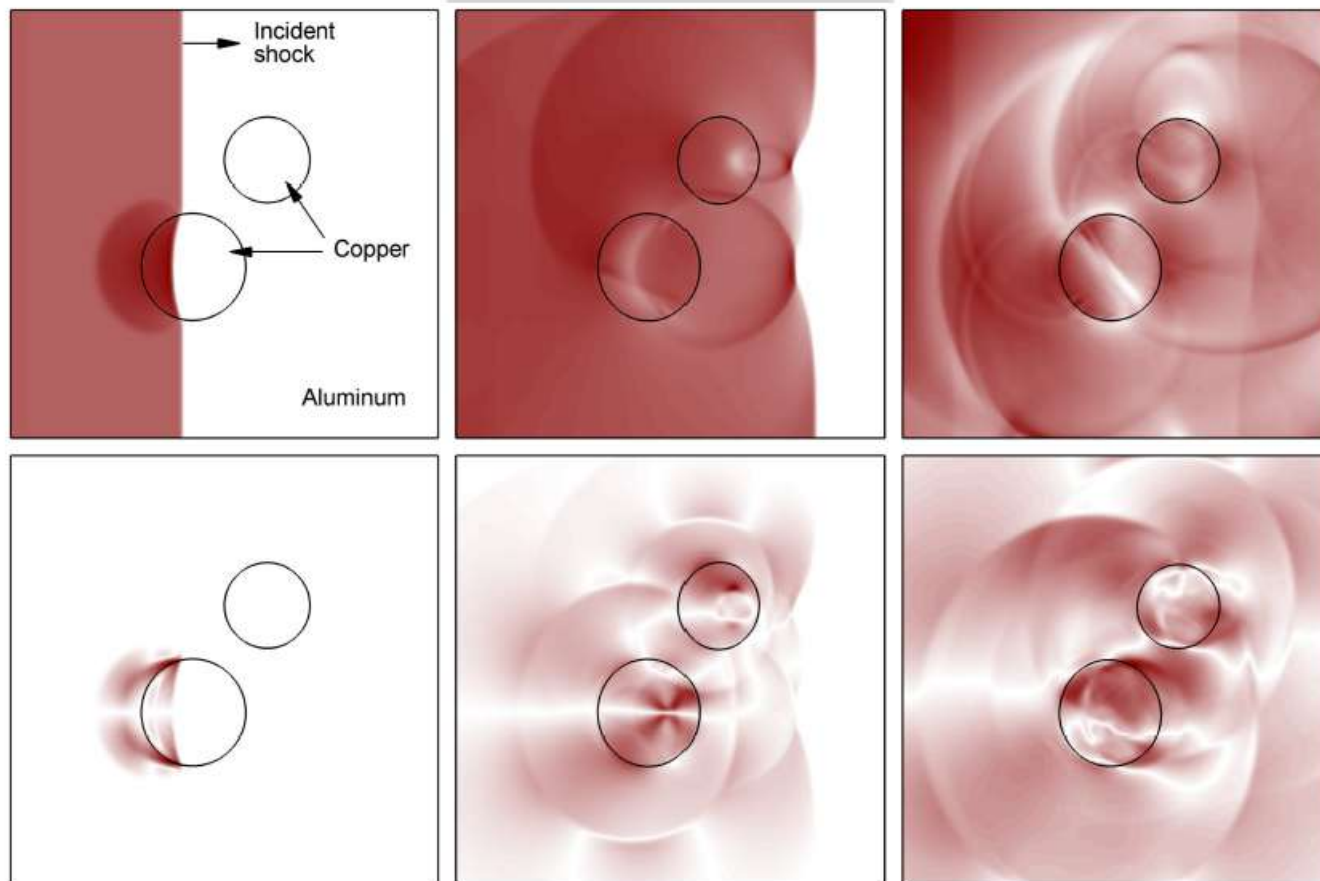


Fig. 1: (Top) Pressure ($P = -(1/3)tr(\sigma)$) and (bottom) shear stress as a function of time.

■ Example 3: Two-dimensional void collapse

- Figure shows collapse of void (air) in copper medium
- Numerical method stable for high density ratios ($\sim 10^4$) and different EOS
- Strong pressure and shear waves observed in final stages of collapse

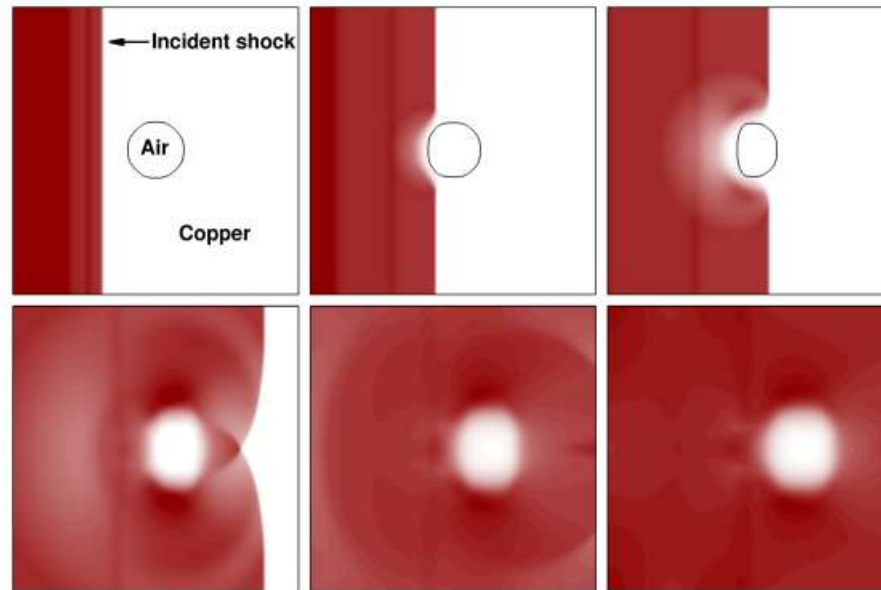


Fig. 4: Pressure contours and $\phi = 0.5$ iso-contour (solid line) as a function of time for two-dimensional void collapse.