

# Removing Full-Scale Testing Barriers: A Fundamental Detonation Characterization Technique for Novel Energetic Formulations at the Laboratory Scale

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Matthew M. Biss  
U.S. Army Research Laboratory  
Aberdeen Proving Ground, MD  
[matthew.biss@us.army.mil](mailto:matthew.biss@us.army.mil)

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## Background

## Objective

$$1. U = C_0 + SU$$

$$2. \rho = \frac{U\rho_{air}}{U-u}$$

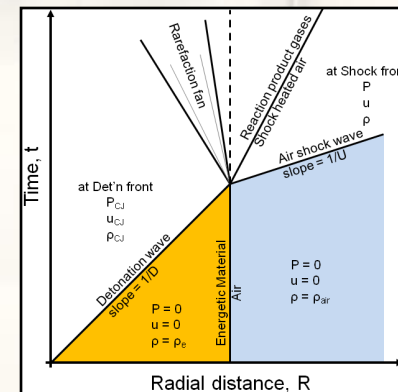
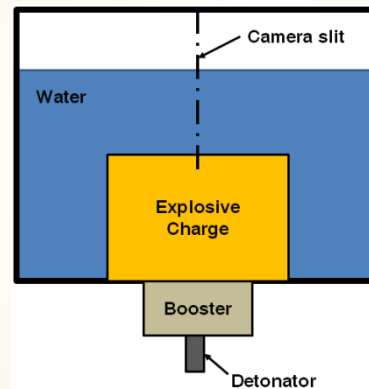
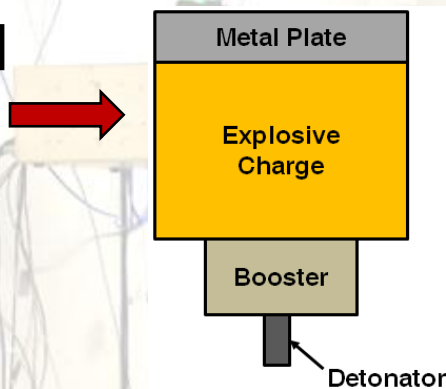
$$3. P = \rho_{air}C_0u + \rho_{air}Su^2$$

$$4. \rho_{CJ} = 1.386\rho_e^{0.96}$$

$$5. \frac{P}{P_{CJ}} = 235 \left( \frac{u}{u_{CJ}} \right)^{-8.71}$$

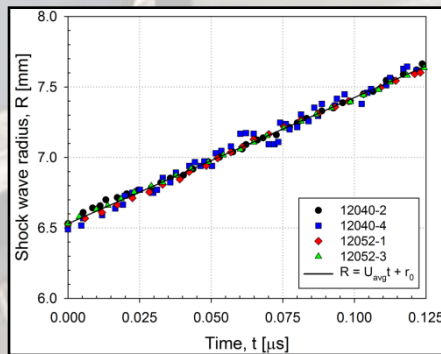
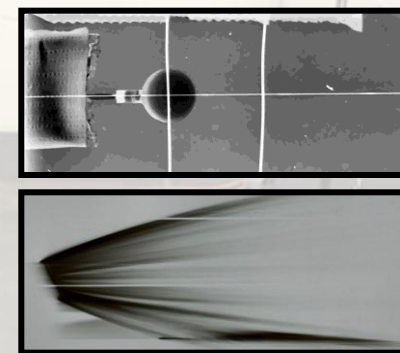
$$6. \frac{\rho_{CJ}}{\rho_0} = \frac{D}{D-u_{CJ}}$$

$$7. P_{CJ} = \rho_e u_{CJ} D$$



## Theory/Methodology

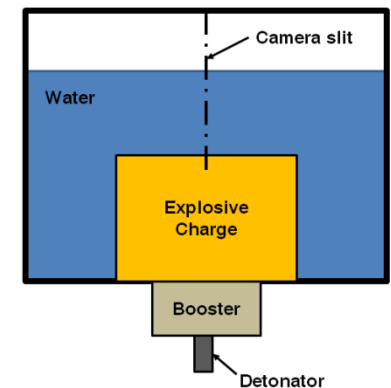
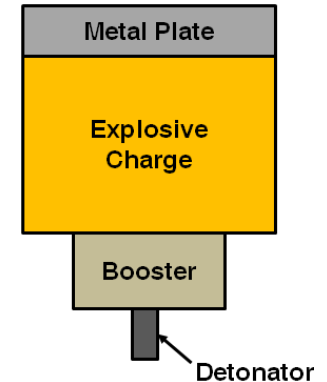
## Experimental Methods



## Results and Discussion

## Conclusions

- **Early detonation characterization research performed by Goranson<sup>1</sup>**
  - Free-surface velocity measurements of ‘flyer plates’ positioned adjacent to an energetic charge
  - Determined reaction-zone length and CJ pressure
- **Holton extended experiment by replacing the flyer plate with an optically transparent material (most commonly water)<sup>2</sup>**
  - Streak image taken parallel to charge axis of sympathetically detonated cylindrical charge submerged in distilled water
  - Water shock wave velocity measured
  - Empirical water shock wave parameters implemented
  - Detonation velocity as a function of density relationship known *a priori*
  - Detonation pressure calculated using above and hydrodynamic theory



1. Duff, R.; Houston, E. Measurement of the Chapman-Jouguet pressure and reaction zone length in a detonating high explosive. *The Journal of Chemical Physics* **1955**, 23 (7), 1268.

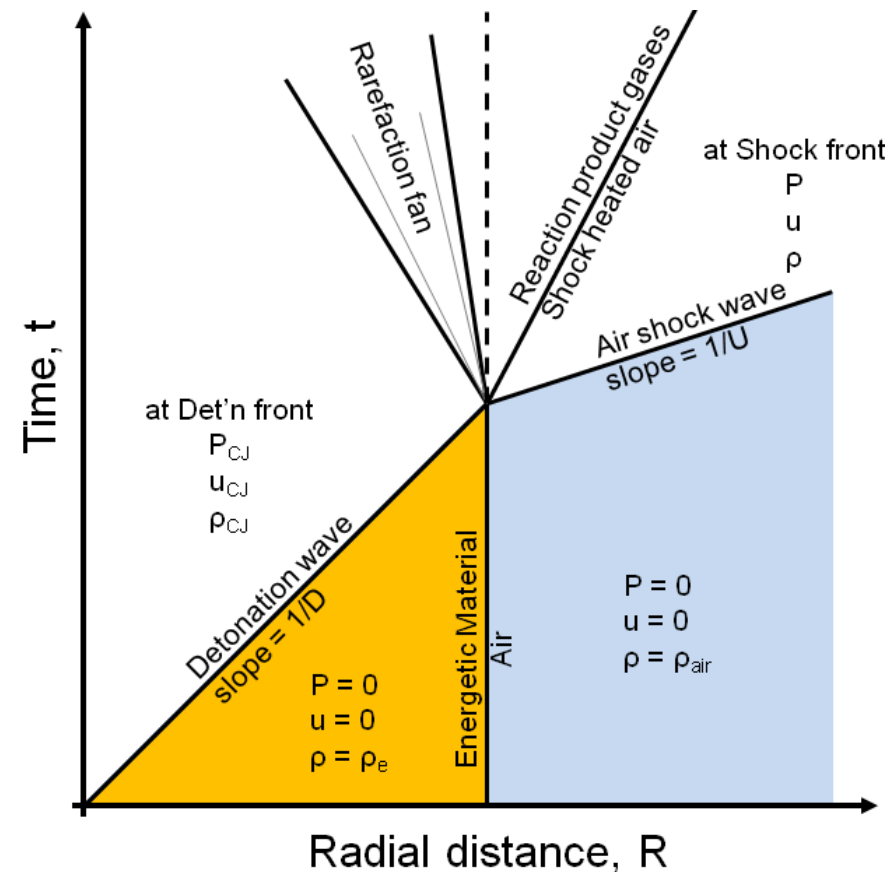
2. Holton, W. *The detonation pressures in explosives as measured by transmitted shocks in water*; NAVORD Report 3968; Naval Ordnance Laboratory: White Oak, MD, December 1954.

Proposed to measure air shock wave velocity  $U$  at the energetic material—air interface and infer all other state properties using theoretical/empirical foundation

## Energetic material detonating in atmospheric air

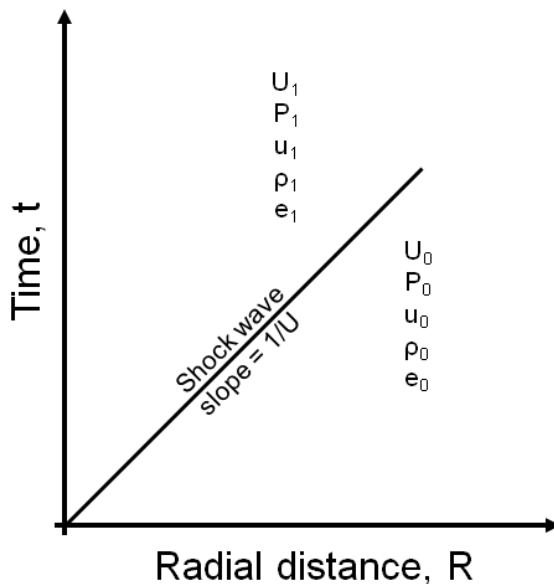
- Detonation wave transferred into air as shock wave possessing different state property values
- 8 variables needed to define interaction
  - Detonation wave:  $D, P_{CJ}, u_{CJ}, \rho_{CJ}$
  - Air shock wave:  $U, P, u, \rho$

## Detonation Interaction



## Shock wave fully defined by five state variables:

- Velocity  $U$ , pressure  $P$ , particle velocity  $u$ , specific volume,  $v$  (or density  $\rho$ ), and specific internal energy,  $e$
- Specific internal energy eliminated by combining equation of state, *i.e.*,  $e = f(P, \rho)$ , and conservation of energy



$$\begin{array}{c} \text{Mass} \\ \hline \frac{\rho_1}{\rho_0} = \frac{U - u_0}{U - u_1} = \frac{v_0}{v_1} \end{array}$$

$$\begin{array}{c} \text{Momentum} \\ \hline P_1 - P_0 = \rho_0 (u_1 - u_0)(U - u_0) \end{array}$$

$$\begin{array}{c} \text{Energy} \\ \hline e_1 - e_0 = \frac{P_1 u_1 - P_0 u_0}{\rho_0 (U - u_0)} - \frac{1}{2} (u_1^2 - u_0^2) \end{array}$$

**Equation of state**

$$e = f(P, v \text{ or } \rho)$$

**Hugoniot**  
 $P = f(\rho)$

## Detonation wave

Unknown:  $D, P_{CJ}, u_{CJ}, \rho_{CJ}$

### Mass

$$\frac{\rho_{CJ}}{\rho_e} = \frac{D}{D - u_{CJ}}$$

### Momentum

$$P_{CJ} = \rho_e u_{CJ} D$$

## Air shock wave

Unknown:  $P, u, \rho$

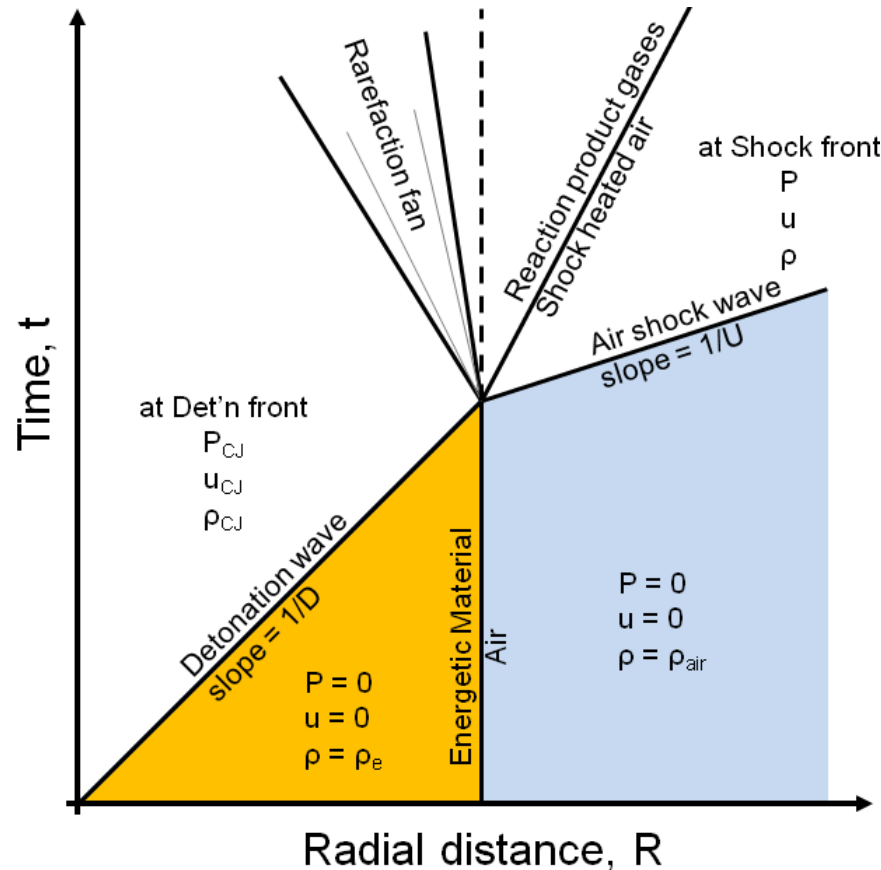
Known:  $U$

### Mass

$$\frac{\rho}{\rho_{air}} = \frac{U}{U - u}$$

### Momentum

$$P = \rho_{air} U u$$



## Detonation wave equations

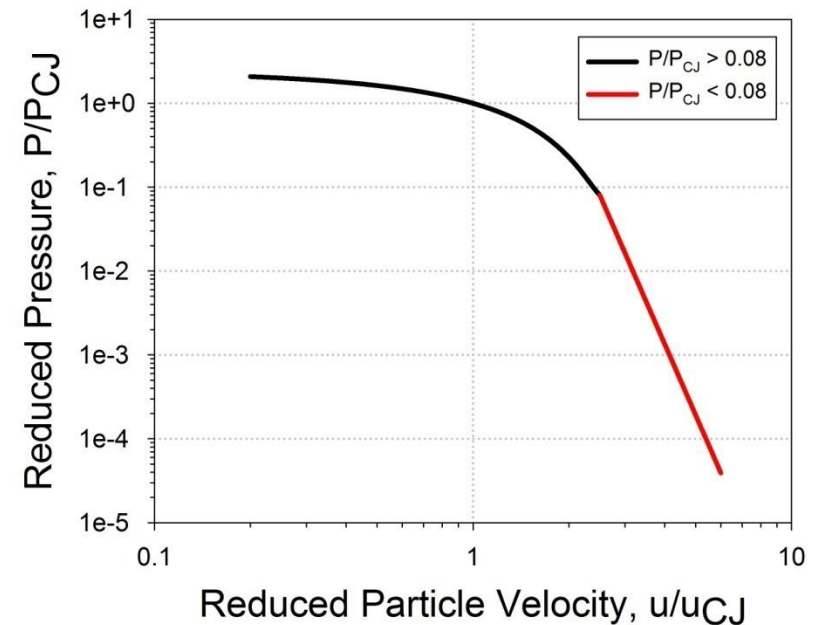
- Cooper developed reduced form of  $P-u$  Hugoniot for compilation of energetic materials<sup>3</sup>
- Data collapsed into a narrow band able to be approximated by two correlations based upon reduced pressure:

For reduced pressures above 0.08:

$$\frac{P}{P_{CJ}} = 2.412 - 1.7315 \left( \frac{u}{u_{CJ}} \right) + 0.3195 \left( \frac{u}{u_{CJ}} \right)^2$$

and for reduced pressures below 0.08:

$$\frac{P}{P_{CJ}} = 235 \left( \frac{u}{u_{CJ}} \right)^{-8.71}$$

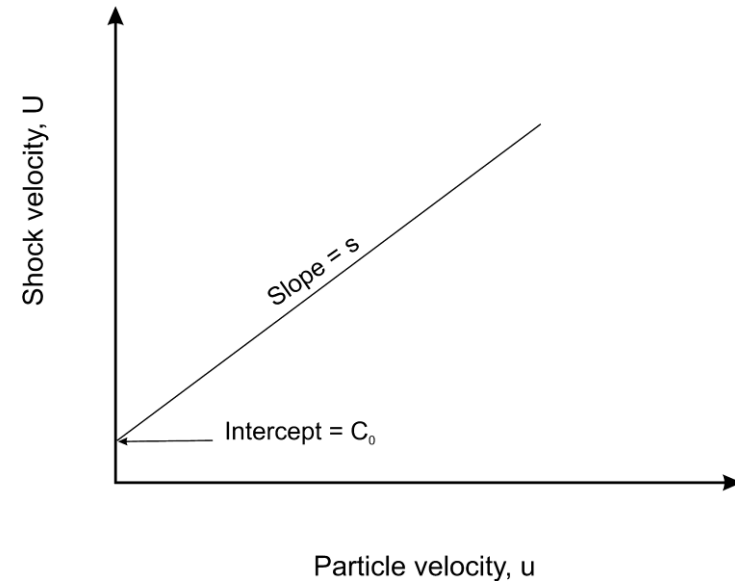
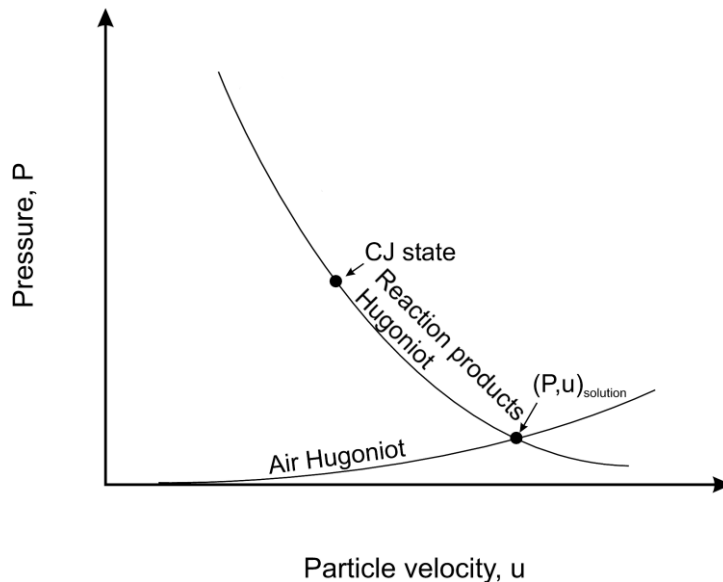


## Detonation wave equations

- Reduced pressure  $P/P_{CJ}$  is anticipated to be extremely low due to large shock impedance discrepancy ( $\rho_e \approx 1500 * \rho_{air}$ )

**Energetic material:**  $Z_e = \rho_e D$       **Air:**  $Z_{air} = \rho_{air} U$

- Assume detonation velocity  $D$  and air shock wave velocity  $U$  are on the same order of magnitude
  - Air shock wave pressure  $P < P_{CJ}$ , air particle velocity  $u > u_{CJ}$
  - $P/P_{CJ}$  anticipated to fall below 0.08 threshold





## Detonation wave

Unknown:  $D, P_{CJ}, u_{CJ}, \rho_{CJ}$

### Mass

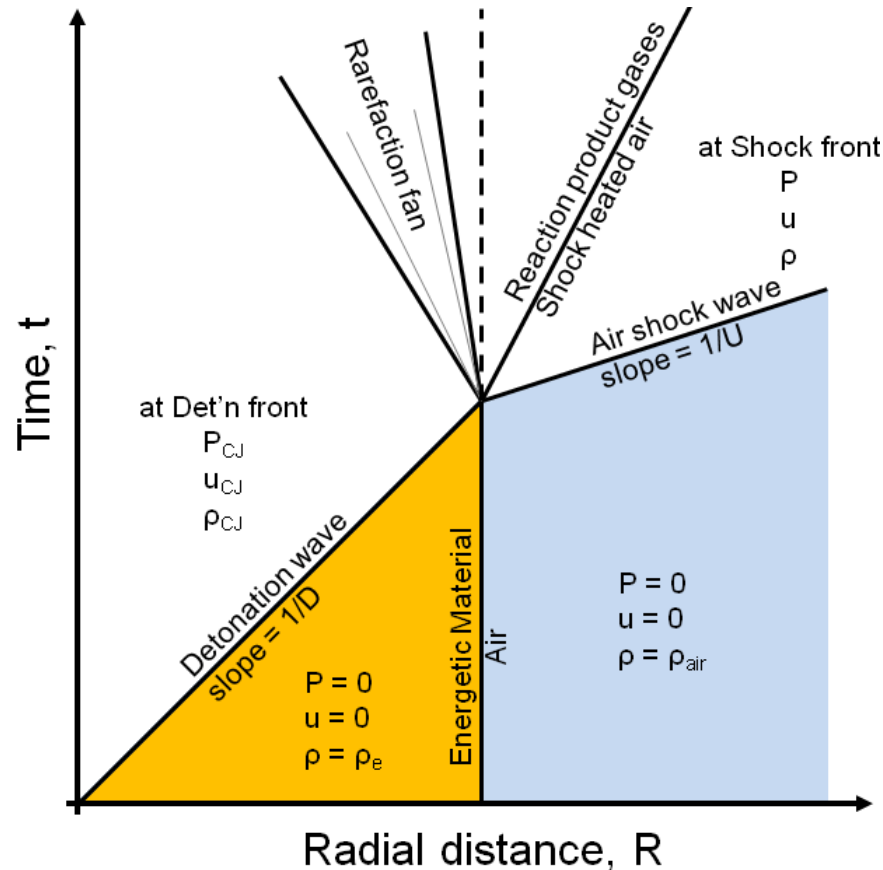
$$\frac{\rho_{CJ}}{\rho_e} = \frac{D}{D - u_{CJ}}$$

### Momentum

$$P_{CJ} = \rho_e u_{CJ} D$$

### P-u Hugoniot

$$\frac{P}{P_{CJ}} = 235 \left( \frac{u}{u_{CJ}} \right)^{-8.71}$$



## Air shock wave

Unknown:  $P, u, \rho$

Known:  $U$

### Mass

$$\frac{\rho}{\rho_{air}} = \frac{U}{U - u}$$

### Momentum

$$P = \rho_{air} U u$$

### U-u Hugoniot

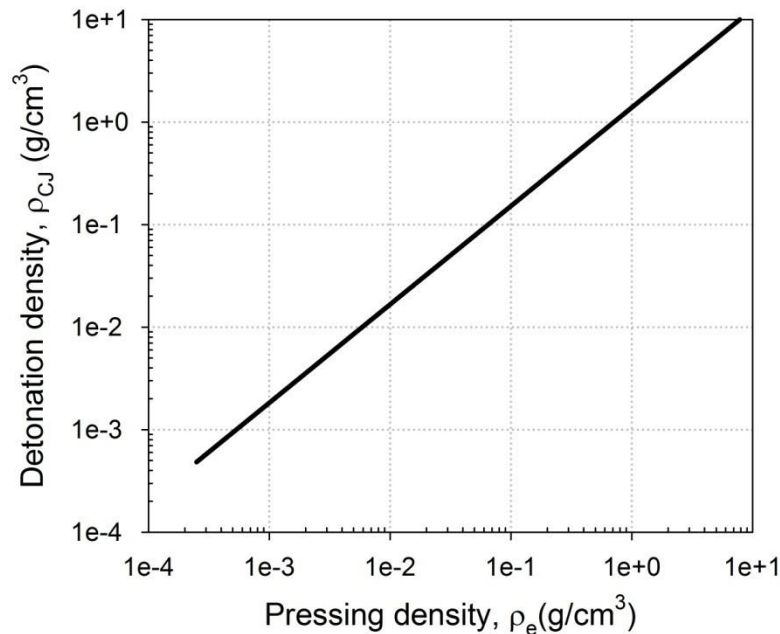
$$U = C_0 + s u$$

## Detonation density relationship

- Second universal energetic reaction products Hugoniot unavailable
- Cooper developed relationship to relate detonation density to energetic pressing density

### Density Relationship

$$\rho_{CJ} = 1.386 \rho_e^{0.96}$$



## P-u Hugoniot for air

### Momentum

$$P = \rho_{air} Uu$$

+

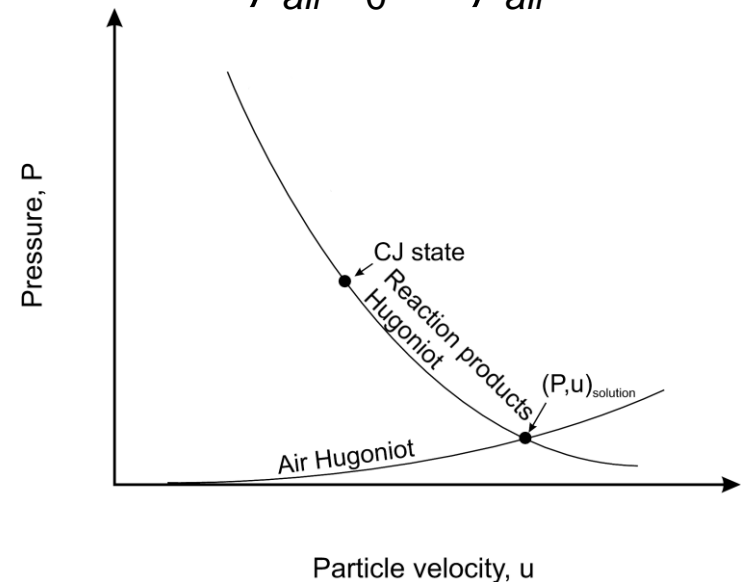
### U-u Hugoniot

$$U = C_0 + Su$$

=

### P-u Hugoniot

$$P = \rho_{air} C_0 u + \rho_{air} s u^2$$



## Detonation wave

Unknown:  $D, P_{CJ}, u_{CJ}, \rho_{CJ}$

### Mass

$$\frac{\rho_{CJ}}{\rho_e} = \frac{D}{D - u_{CJ}}$$

### Momentum

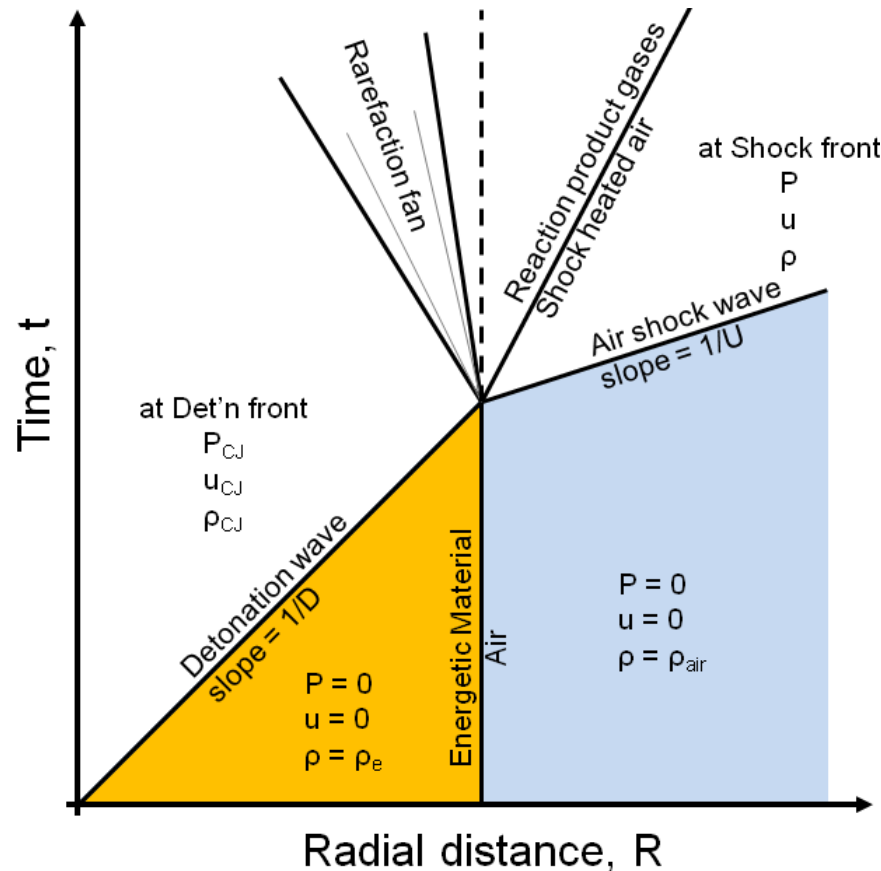
$$P_{CJ} = \rho_e u_{CJ} D$$

### P-u Hugoniot

$$\frac{P}{P_{CJ}} = 235 \left( \frac{u}{u_{CJ}} \right)^{-8.71}$$

### Density Relationship

$$\rho_{CJ} = 1.386 \rho_e^{0.96}$$



## Air shock wave

Unknown:  $P, u, \rho$

Known:  $U$

### Mass

$$\frac{\rho}{\rho_{air}} = \frac{U}{U - u}$$

### U-u Hugoniot

$$U = C_0 + su$$

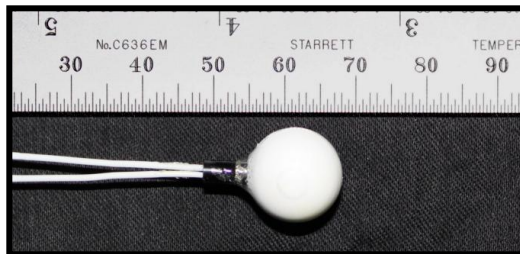
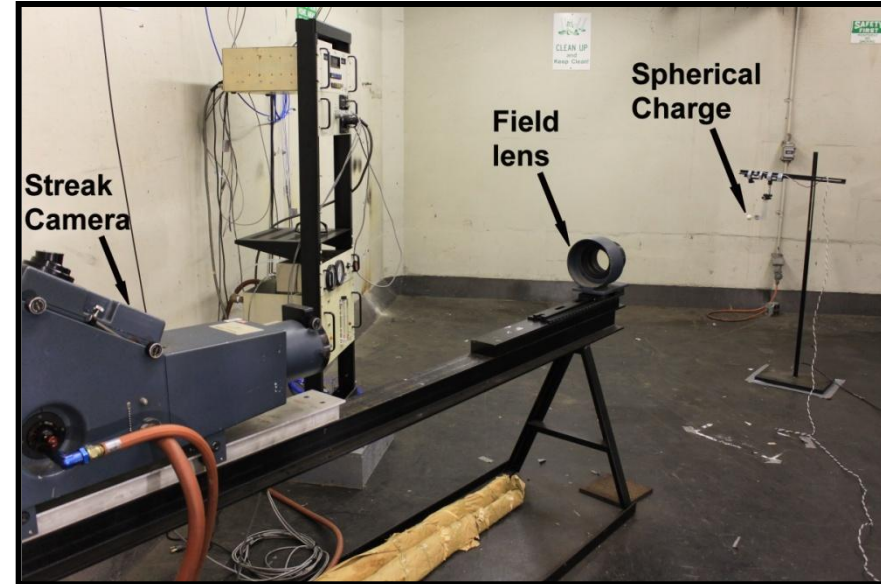
### P-u Hugoniot

$$P = \rho_{air} C_0 u + \rho_{air} s u^2$$

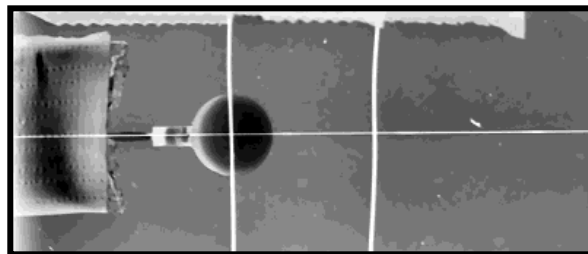
- **Film-based streak camera captures radial shock wave expansion rate at the energetic material–air interface**

- Beckman & Whitley Model 770
- 8 mm/ $\mu$ s writing speed
- 90 cm  $f/6.3$  field lens
- Spherical 2 g RDX charges
- RP-3 EBW detonator [29 mg PETN]

- **Spherical RDX charges**



a) Fully assembled 2 g spherical RDX charge



b) Static streak-camera image of the spherical charge in the test plane



c) Dynamic spherical charge detonation streak record

- **Streak records digitized using high-resolution scanner**

- HP 8200 flatbed scanner
- 8-bit grayscale @ 4800 dpi



- **Digitized records analyzed in MATLAB to track radial shock wave expansion rate**

- Standardized test-bed image used for calibration
- ‘Canny’ edge-detection filter with threshold
- First 1.2 mm of radial shock wave expansion<sup>4</sup>

Image.jpg



Canny filter



w/ Threshold



- **Best-fit linear correlation determined for each data set<sup>4</sup>**

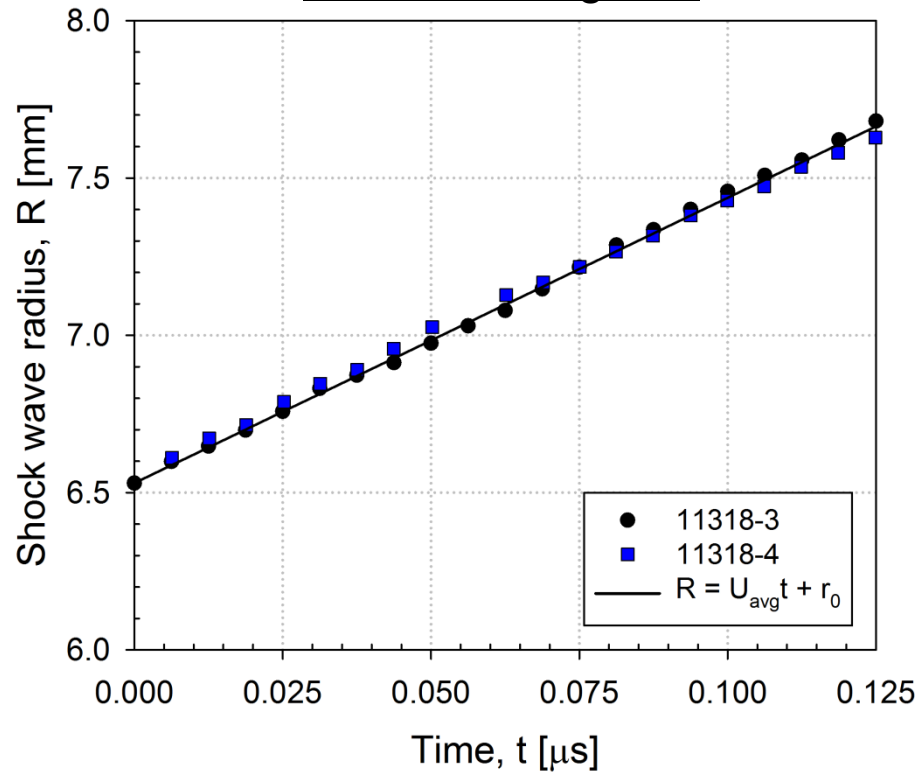
$$R = Ut + r_0 \quad R: \text{shock wave radius, } t: \text{time, } r_0: \text{charge radius, } U: \text{shock wave velocity}$$

- **Detonation wave and air shock wave data calculated from measured shock wave velocity and theory**

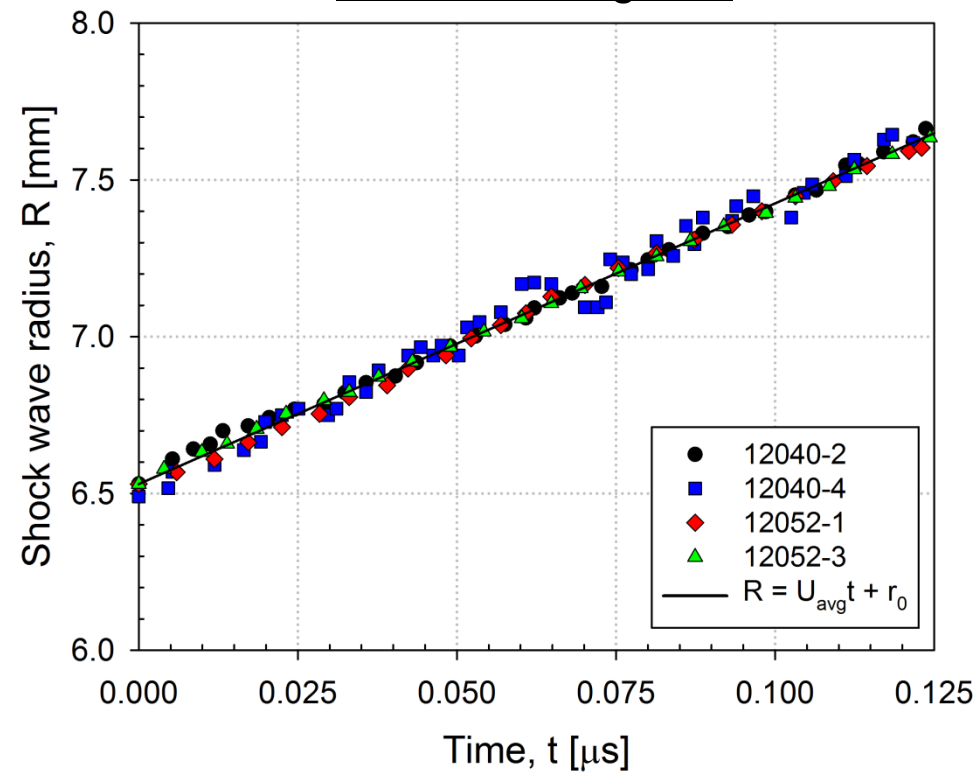
4. Rigdon, J. K.; Akst, I. B. An analysis of the “Aquarium technique” as a precision detonation pressure measurement gage. In *Proceedings of the Fifth Symposium (International) on Detonation*; U.S. Naval Ordnance Laboratory and the Office of Naval Research: Pasadena, CA, 1970.

## Shock wave radius-versus-time data

RDX at 1.77 g/cm<sup>3</sup>



RDX at 1.63 g/cm<sup>3</sup>



## Calculated detonation wave and air shock wave properties for RDX at 1.63g/cm<sup>3</sup>

| Charge    | $\rho_{\text{air}}$  | U             | D             | $P_{\text{CJ}}$ | $\rho_{\text{CJ}}$   | $u_{\text{CJ}}$ | P     | U             |
|-----------|----------------------|---------------|---------------|-----------------|----------------------|-----------------|-------|---------------|
|           | (g/cm <sup>3</sup> ) | (mm/ $\mu$ s) | (mm/ $\mu$ s) | (GPa)           | (g/cm <sup>3</sup> ) | (mm/ $\mu$ s)   | (MPa) | (mm/ $\mu$ s) |
| Published | -                    | -             | 8.34          | 28.3            | 2.16                 | -               | -     | -             |
| 12040-2   | 1.207e <sup>-3</sup> | 8.85          | 8.40          | 30.4            | 2.22                 | 2.22            | 87.0  | 8.14          |
| 12040-4   | 1.207e <sup>-3</sup> | 9.06          | 8.61          | 31.9            | 2.22                 | 2.28            | 91.2  | 8.34          |
| 12052-1   | 1.213e <sup>-3</sup> | 9.16          | 8.71          | 32.7            | 2.22                 | 2.31            | 93.7  | 8.44          |
| 12052-3   | 1.206e <sup>-3</sup> | 8.74          | 8.30          | 29.7            | 2.22                 | 2.19            | 84.8  | 8.04          |
| Average   | 1.208e <sup>-3</sup> | 8.95          | 8.51          | 31.2            | 2.22                 | 2.25            | 89.2  | 8.24          |
| St. Dev.  | 3.202e <sup>-6</sup> | 0.19          | 0.19          | 1.4             | 0                    | 0.05            | 4     | 0.18          |
| % Dev.    | -                    | -             | 1.98          | 10.2            | 2.78                 | -               | -     | -             |

## Calculated detonation wave and air shock wave properties for RDX at 1.77g/cm<sup>3</sup>

| Charge    | $\rho_{\text{air}}$  | U             | D             | $P_{\text{CJ}}$ | $\rho_{\text{CJ}}$   | $u_{\text{CJ}}$ | P     | u             |
|-----------|----------------------|---------------|---------------|-----------------|----------------------|-----------------|-------|---------------|
|           | (g/cm <sup>3</sup> ) | (mm/ $\mu$ s) | (mm/ $\mu$ s) | (GPa)           | (g/cm <sup>3</sup> ) | (mm/ $\mu$ s)   | (MPa) | (mm/ $\mu$ s) |
| Published | -                    | -             | 8.69          | 33.6            | 2.34                 | -               | -     | -             |
| 11318-3   | 1.202e <sup>-3</sup> | 9.18          | 8.73          | 35.3            | 2.40                 | 2.28            | 93.3  | 8.46          |
| 11318-4   | 1.202e <sup>-3</sup> | 8.96          | 8.51          | 33.6            | 2.40                 | 2.23            | 88.9  | 8.25          |
| Average   | 1.202e <sup>-3</sup> | 9.07          | 8.62          | 34.4            | 2.40                 | 2.26            | 91.1  | 8.36          |
| % Dev.    | -                    | -             | 0.81          | 2.53            | 2.56                 | -               | -     | -             |

Single laboratory-scale experiment provides same information as multiple full-scale tests that require kilograms of material

Theoretically calculated detonation wave properties predicted to within 3%\* of published data for two densities of Class V RDX

\* 5/6 properties, 10% deviation for empirically calculated value



## Calculated detonation wave and air shock wave properties from previous research

| Explosive            | $\rho_e$             | $\rho_{air}$         | U             | D             | $P_{CJ}$ | $\rho_{CJ}$          | P     | u             |
|----------------------|----------------------|----------------------|---------------|---------------|----------|----------------------|-------|---------------|
|                      | (g/cm <sup>3</sup> ) | (g/cm <sup>3</sup> ) | (mm/ $\mu$ s) | (mm/ $\mu$ s) | (GPa)    | (g/cm <sup>3</sup> ) | (MPa) | (mm/ $\mu$ s) |
| <b>HMX/Inert</b>     | 1.781                | $1.07e^{-2}$         | 7.42          | 8.73          | 33.5     | 2.34                 | 53.0  | 6.53          |
| Calculated           | -                    | -                    | -             | 8.60          | 34.5     | 2.41                 | 53.8  | 6.79          |
| % Dev.               | -                    | -                    | -             | 1.5           | 3.0      | 2.9                  | 1.5   | 4.0           |
| <b>HMX/TNT/Inert</b> | 1.776                | $3.79e^{-3}$         | 7.84          | 8.21          | 31.2     | 2.40                 | 21.2  | 7.13          |
| Calculated           | -                    | -                    | -             | 8.26          | 31.7     | 2.41                 | 21.3  | 7.18          |
| % Dev.               | -                    | -                    | -             | 0.6           | 1.7      | 0.4                  | 0.5   | 0.7           |
| <b>TNT</b>           | 1.636                | $0.971e^{-3}$        | 7.34          | 6.93          | 20.7     | 2.15                 | 47.8  | 6.71          |
| Calculated           | -                    | -                    | -             | 6.80          | 20.0     | 2.22                 | 47.8  | 6.71          |
| % Dev.               | -                    | -                    | -             | 1.9           | 3.4      | 3.2                  | 0     | 0             |
| <b>Composition B</b> | 1.717                | $0.947e^{-3}$        | 8.67          | 7.98          | 29.5     | 2.34                 | 65.5  | 7.97          |
| Calculated           | -                    | -                    | -             | 8.05          | 29.2     | 2.33                 | 65.5  | 7.98          |
| % Dev.               | -                    | -                    | -             | 0.9           | 1.0      | 0.4                  | 0     | 0.1           |

## Calculated detonation wave and air shock wave properties from previous research

| Explosive  | $\rho_e$             | $\rho_{air}$         | U             | D             | $P_{CJ}$ | $\rho_{CJ}$          | P     | u             |
|------------|----------------------|----------------------|---------------|---------------|----------|----------------------|-------|---------------|
|            | (g/cm <sup>3</sup> ) | (g/cm <sup>3</sup> ) | (mm/ $\mu$ s) | (mm/ $\mu$ s) | (GPa)    | (g/cm <sup>3</sup> ) | (MPa) | (mm/ $\mu$ s) |
| Cyclotol   | 1.752                | 0.936e <sup>-3</sup> | 8.64          | 8.27          | 31.3     | 2.38                 | 64.2  | 7.94          |
| Calculated | -                    | -                    | -             | 8.01          | 29.5     | 2.37                 | 64.2  | 7.95          |
| % Dev.     | -                    | -                    | -             | 3.1           | 5.8      | 0.4                  | 0     | 0.1           |
| Octol      | 1.821                | 0.943e <sup>-3</sup> | 8.86          | 8.49          | 34.2     | 2.46                 | 68.1  | 8.14          |
| Calculated | -                    | -                    | -             | 8.23          | 32.2     | 2.46                 | 68.1  | 8.15          |
| % Dev.     | -                    | -                    | -             | 3.1           | 5.8      | 0                    | 0     | 0.1           |
| HBX-1      | 1.712                | 1.253e <sup>-3</sup> | 7.61          | 7.31          | 22.0     | 2.18                 | 67.0  | 6.97          |
| Calculated | -                    | -                    | -             | 7.22          | 22.4     | 2.21                 | 66.5  | 6.97          |
| % Dev.     | -                    | -                    | -             | 1.2           | 1.8      | 1.4                  | 0.7   | 0             |

Theoretically calculated detonation wave and air shock wave properties predicted to within 3.5% of published data for 32/35 properties from seven historical data sets using single shock wave velocity measurement and atmospheric conditions

## Laboratory-scale experimental detonation characterization technique established and verified

- Composed from conservation laws, material Hugoniot, and empirical relationships
- Able to determine detonation wave properties:  $D$ ,  $P_{CJ}$ ,  $\rho_{CJ}$ , and  $u_{CJ}$  and shock wave properties:  $U$ ,  $P$ ,  $\rho$ , and  $u$ 
  - Verified using two densities of RDX (1.63 and 1.77 g/cm<sup>3</sup>)
    - Predicted 5/6 properties to within 3% of published data
  - Reproduced historical data sets for seven energetic materials
    - Predicted 32/35 properties to within 3.5% of published data

## Single laboratory-scale experiment provides same information as multiple full-scale tests that require kilograms of material

- Highly-advantageous cost-savings approach for the formulation of novel insensitive energetic materials
- Eliminates initial formulation scale-up requirements necessary for determining detonation performance parameters

# *Questions?*

**Matthew M. Biss**  
U.S. Army Research Laboratory  
Aberdeen Proving Ground, MD 21005  
[matthew.biss@us.army.mil](mailto:matthew.biss@us.army.mil)