First-Principles Hover Prediction Using CREATE-AV Helios



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Rotorcraft in Hover

Rotor wakes are largely dominated by the trailing

vortex system



UH-60 Black Hawk in hover



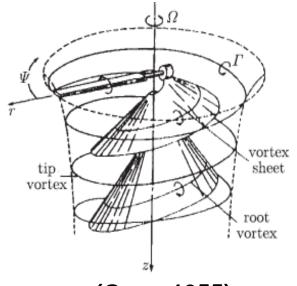
V-22 Osprey in hover

- The hover condition represents one of the true values of the helicopter
- A limiting design point in terms of power requirements



Why is "First-Principles" Simulation of Hover so Challenging?

- Rotary-wing vehicle aerodynamic loads are heavily influenced by their own vortical wakes
- "First-principles" simulations try to model the entire wake without empirical inputs or vortex-based method inputs
 - Numerical methods are dissipative
- Historically, a very challenging task because of the differences in scales (tip vortex from a UH60 rotor is ~1/300* Rotor Radius)
- The hover helical vortex system is entirely self-induced:
 - Feedback between vortex strength and vortex system dynamics – neutrally stable



(Gray, 1955)

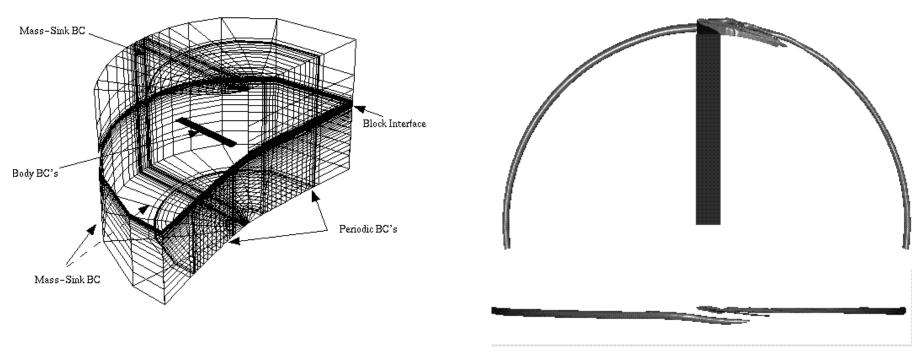
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Scope

- Several excellent survey articles that summarize rotorcraft flow simulation efforts are available in literature:
 - McCroskey [1995]
 - Srinivasan and Sankar [1994], Landgrebe [1994]
 - Hariharan and Sankar [2000]
 - Strawn and Caradonna [2005]
- The present work is not intended to be an allinclusive survey of rotorcraft wake modeling. In this paper, key technology enablers that make up current-day capabilities are reviewed.
- Results from the state-of-art, high-fidelity rotor-wake hover simulations are reviewed and status assessed



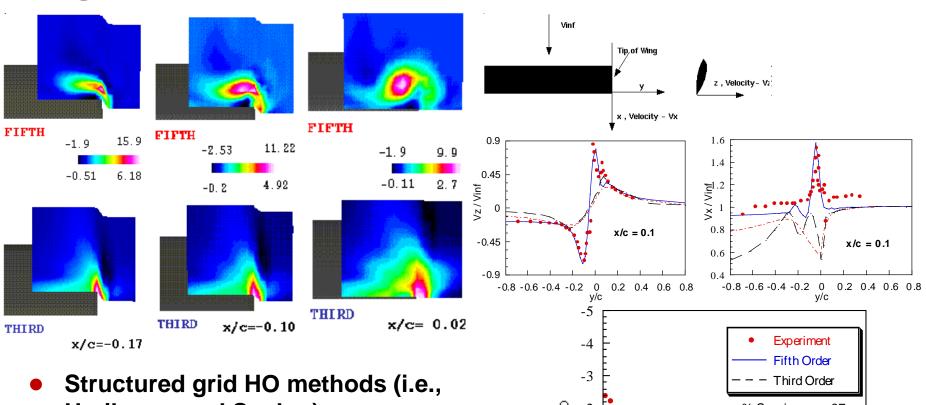
First-Principles Hover: Early/Mid-90s



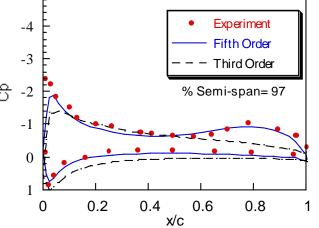
- Structured, cylindrical, periodic (i.e., Srinivasan and Baeder, Duque)
- Unstructured (i.e., Strawn and Barth)
- Second-/Third-order schemes; wake structure dissipated off rapidly



First-Principles Hover Enabler: (i) **High-Order Methods**



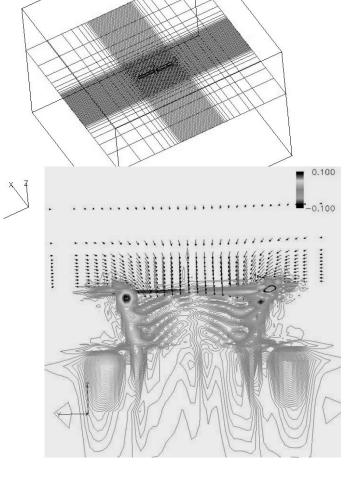
- Hariharan and Sankar)
- 5th- /7th-order spatially-accurate **ENO/WENO** schemes; higher efficiency of wake capturing (5th-order 8-10 points, 7th-order 4–6 points)





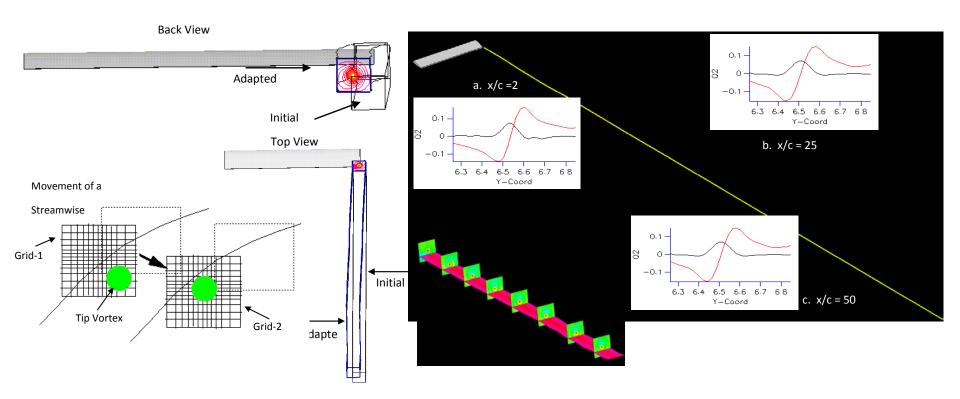
First-Principles Hover Enabler: (ii)
Overset Methods

- Put grid points in the path of wake
- Overset methods: For rotor interactional problems (i.e., McCroskey, Duque, et al., Ahmed, et al., Meakin, et al.)
- Overset + HO methods (i.e., Hariharan and Sankar) – Cartesian background





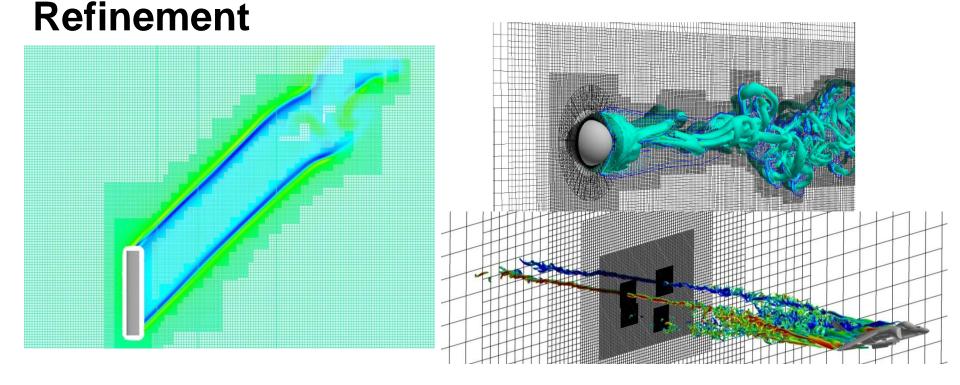
First-Principles Hover Enabler: (iii) Mesh Adaption/Refinement



- Unstructured grid adaptive refinement of wake (i.e., Strawn and Barth)
- Structured adaptive mesh refinement (i.e., Vasilescu, et al.)
- Overset vortex grids (i.e., Dietz, Hariharan)



First-Principles Hover Enabler: (iv)
Distributed, Scalabe Adaptive Mesh

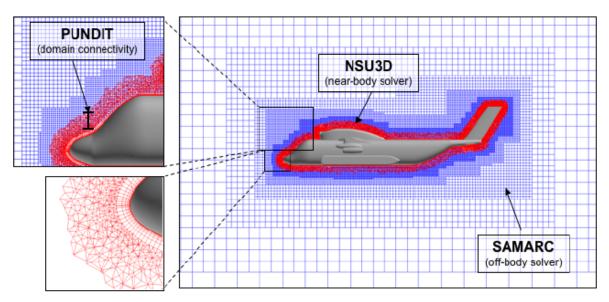


- Overset adaptive mesh refinement to features (i.e., Meakin, Holst, and Pulliam)
- Unsteady parallel AMR (i.e., Wissink, et al.) refines AND de-refines to provide grid points where required
- Parallel automated oversetting (i.e., Sitaraman, et al.)

CREATE-AV Helios



- Cartesian off-body grids
 - No skew, efficient
- Fifth-order spatial accuracy (off-body)
- Flow-based Cartesian grid refinement
- Automated overset infrastructure



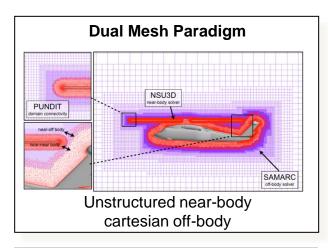
AIAA-2012-0713: Capability Enhancements of the Helios v3.0 High-Fidelity Rotorcraft Simulation Tools

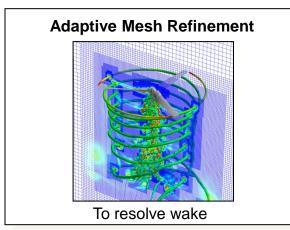
CREATE-AV Helios

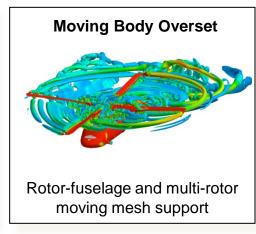


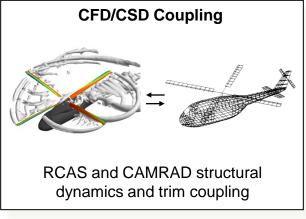
Helios Helicopter Overset Simulations

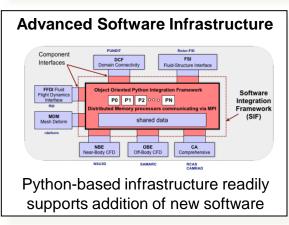


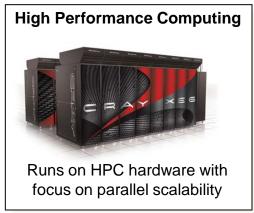














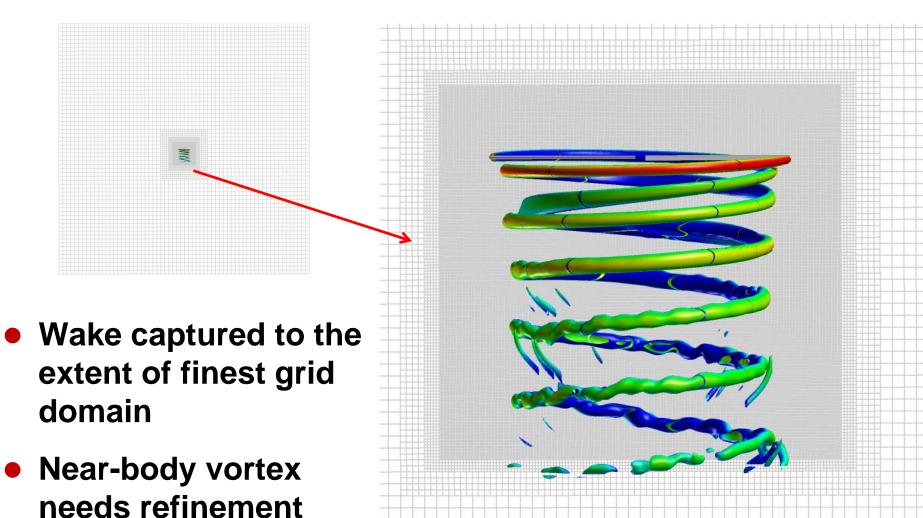


Helios Results from Rotor in Hover

- Two-bladed Rotor, Caradonna and Tung
- Three-bladed Rotor, TRAM
- Six-bladed Rotor, RAH66
- Ducted Rotor

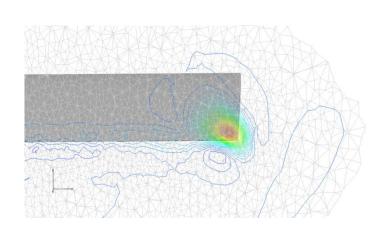


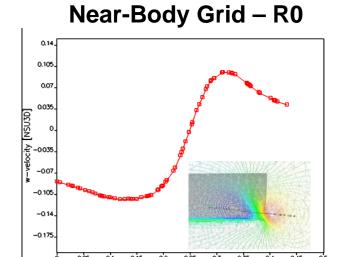
Non-Adaptive Mesh Refinement (AMR) Solution

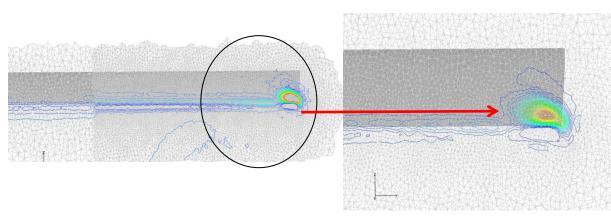


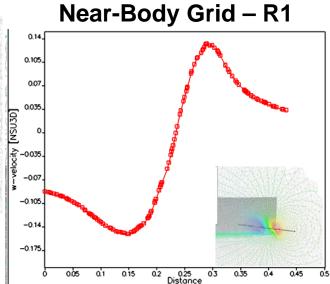


Near-Body Grid Refinement







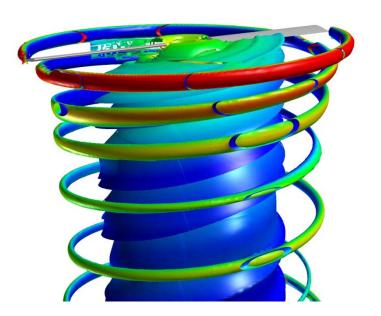


 Near-body tip refinement improves load predictions



Wake of Rotor in Hover

5th-Order Cartesian, 18 cells/chord off-body



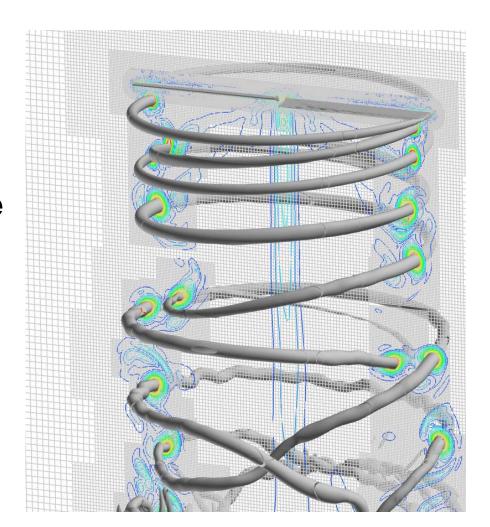
Classical Schematic vortex sheet tip. vortex root: vortex

- Captures the tip vortex and wake sheet structure
- Predicted blade load of $C_T = 0.0048$ (experimental $C_T = 0.0046$)



Wake of Rotor in Hover (AMR)

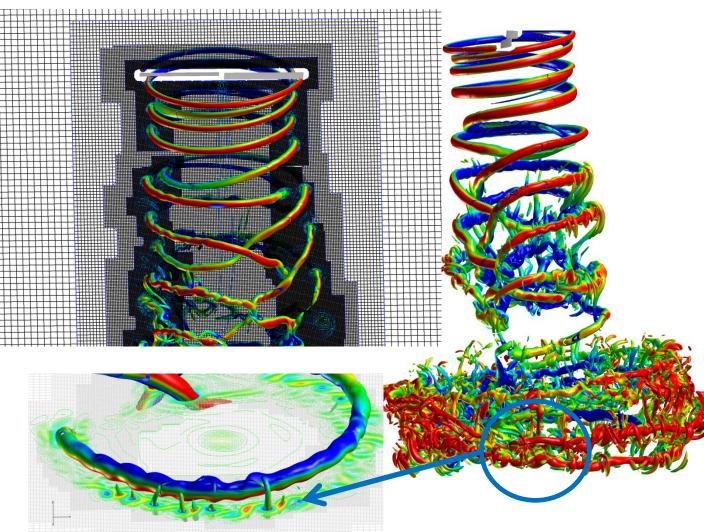
- Cartesian AMR resolves the wake more efficiently targeting the tip vortex (fewer finest-grid cells)
- No further change in blade loading





Secondary Vortex Braids (AMR Solution)

- Secondary vortex braids appear in the far-wake
- No bearing on the load convergence
- Secondary braid vorticity associated with instability patterns when far-wake helical braids come together

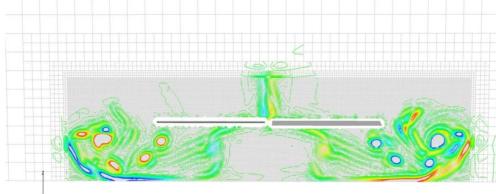




Near-Ground Hover

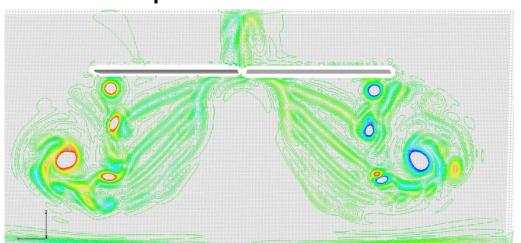
Rotor at z=0.5R

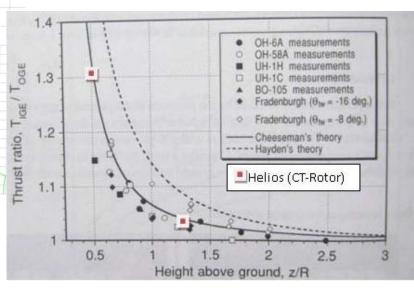
Flared-out vortex wake structure



Rotor at z=1.25R

 Flow-field tending towards OGE solenoidal pattern

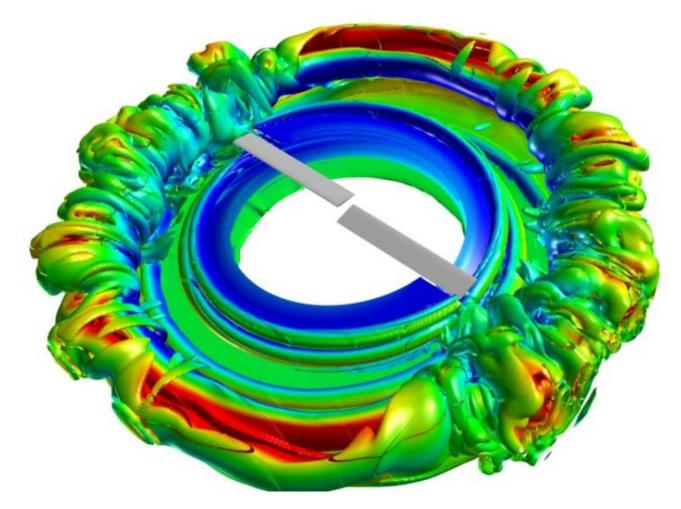




(From Leishman, Helicopter Aerodynamics)



Near-Ground Hover Vortex Pattern



 Toroidal vortex ring structure with secondary braided circumferential structures

TRAM Isolated Rotor

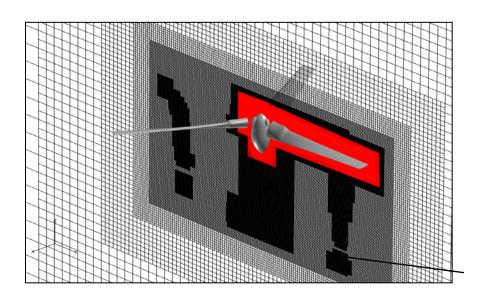


Tilt Rotor Aeroacoustics Model (TRAM)

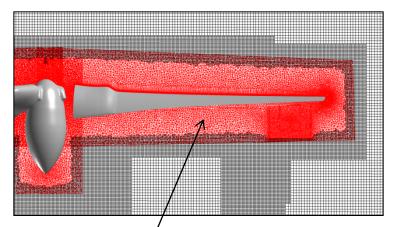
- Quarter-scale model V-22 Osprey
- Experiments at DNW (1998) and NASA Ames (2000)

Computational conditions:

- Rigid blade
- q=14° collective, M_{tip} =0.625, Re_{Tip} =2.1M





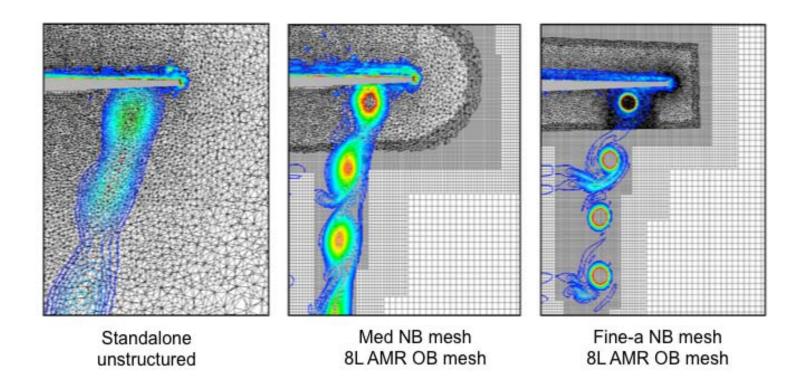


Near-body rótor mesh: 9.3M nodes

Off-body finest-grid resolution: $\Delta x = 0.05c$



Wake of Rotor in Hover (AMR)



Near-body and off-body refinement to get the wake right

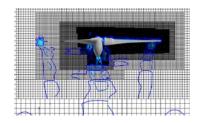
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Feature Detection Augmented with Richardson

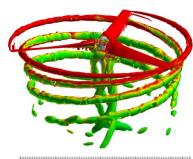
Error

$$err = 10e-3$$



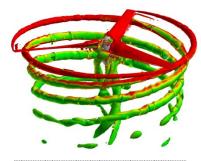


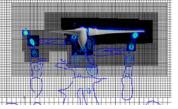
err = 10e-4



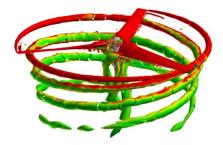


err = 10e-5





err = 10e-6



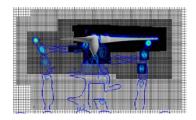


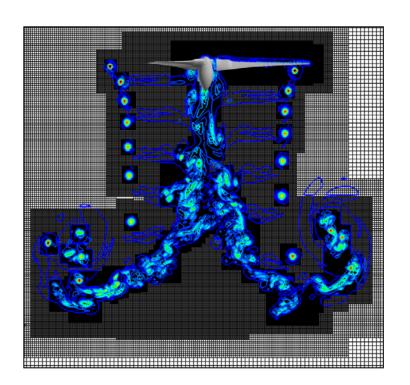
	Figure of Merit	Difference	Mesh Points
Experiment	0.774	-	
err = 10e-3	0.760	-1.8% (+/- 0.4%)	9.6M
err = 10e-4	0.767	-0.9% (+/- 0.4%)	13.2M
err = 10e-5	0.768	-0.8% (+/- 0.2%)	14.2M
err = 10e-6	0.769	-0.6% (+/- 0.2%)	14.3M
no error	0.773	-0.1% (+/- 0.2%)	86M

Tightening error tolerance improves the computed FM

6X fewer gridpoints

Finest TRAM Wake





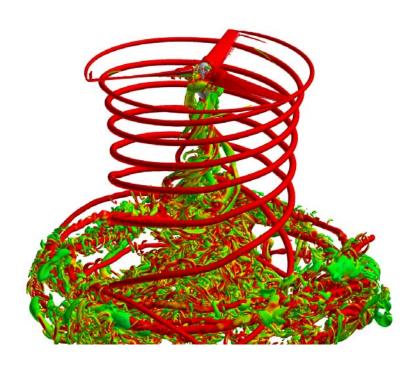


	Figure of Merit	Difference	Mesh Points
Experiment	0.774	-	
Computation	0.773	-0.1% (+/- 0.2%)	86M

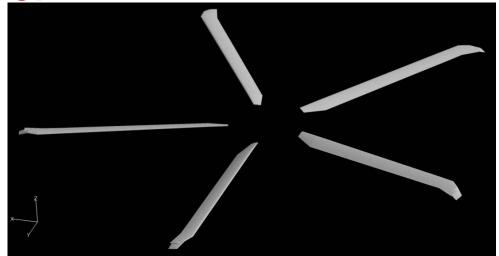
Finest mesh resolution applied to all regions of swirling flow

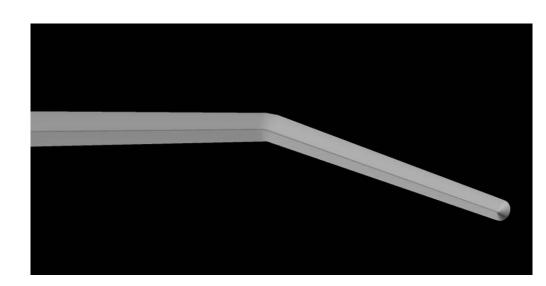


Capability: Anhedral Blade in Hover

RAH Comanche Hover

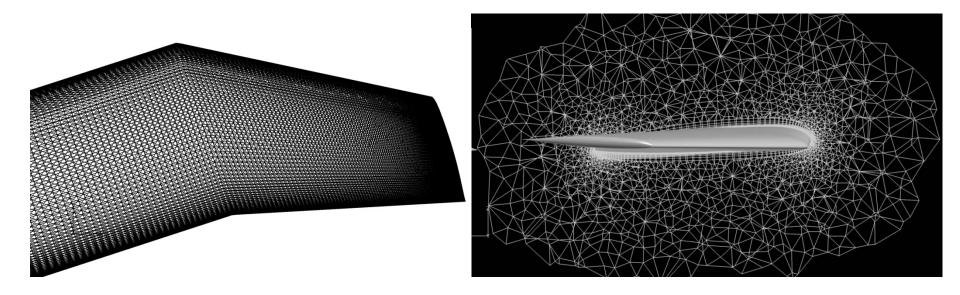
- Five- (5) bladed rotor:
 Straight and improved anhedral tip
- AED (Huntsville, AL)
 ACRB blade solution
 issues inspired this
 case
- Approximate RAH anhedral







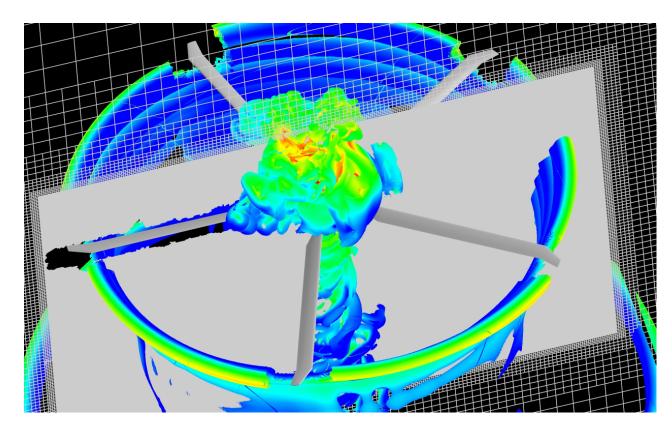
Grids RAH Comanche Hover



- Point-wise surface grids and AFLR volume grids
- Five (5) blades, ~6 million/blade



Fixed Off-Body Grid Solution RAH Comanche Hover



- Straight and anhedral blade solutions ran well with default settings
- Weak vortex system feeding the off-body



Aerodynamic Loads RAH Comanche Hover

Collective Pitch = 0			
	СТ	CQ	FM
Baseline	0.0002627	0.000125	0.024
Anhedral	0.00020181	0.000145	0.014

Collective Pitch =10			
	CT	CQ	FM
Baseline	0.008365	0.0008873	0.609
Anhedral	0.009079	0.000979	0.624
Anhedral (Adaptive)	0.009281	0.000988	0.6397

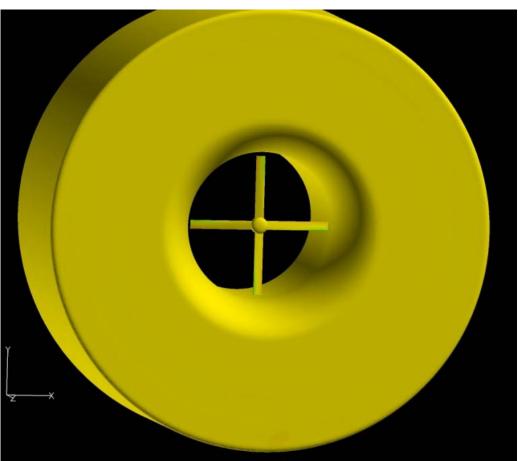
Correct trending – Anhedral improves hover efficiency at operating collectives



Capability: Ducted Fan ARL Ducted Fan

- ARL (Aberdeen, MD) conceptual design case
- Multi-component, close proximity
- External/Internal flow
- Point-wise/AFLR grids for duct and rotor+hub

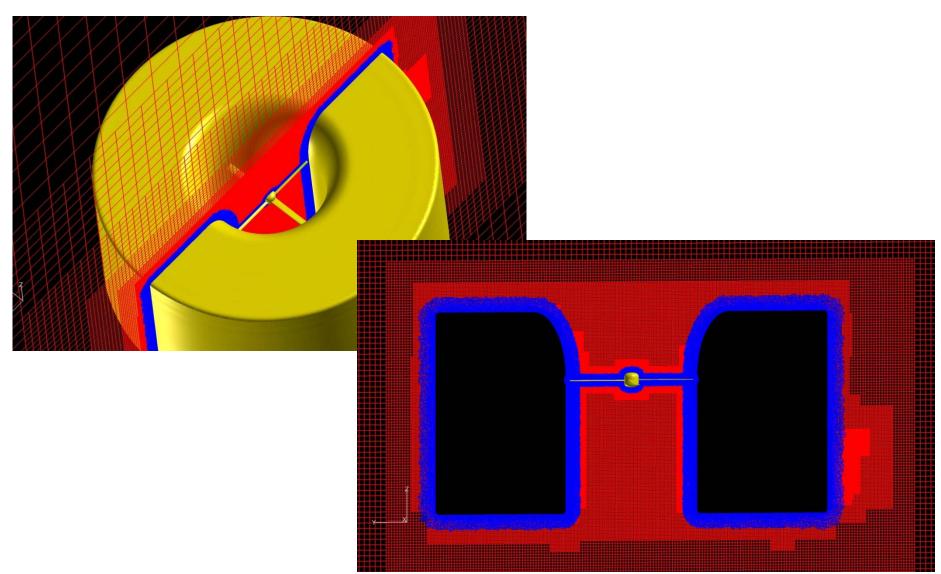






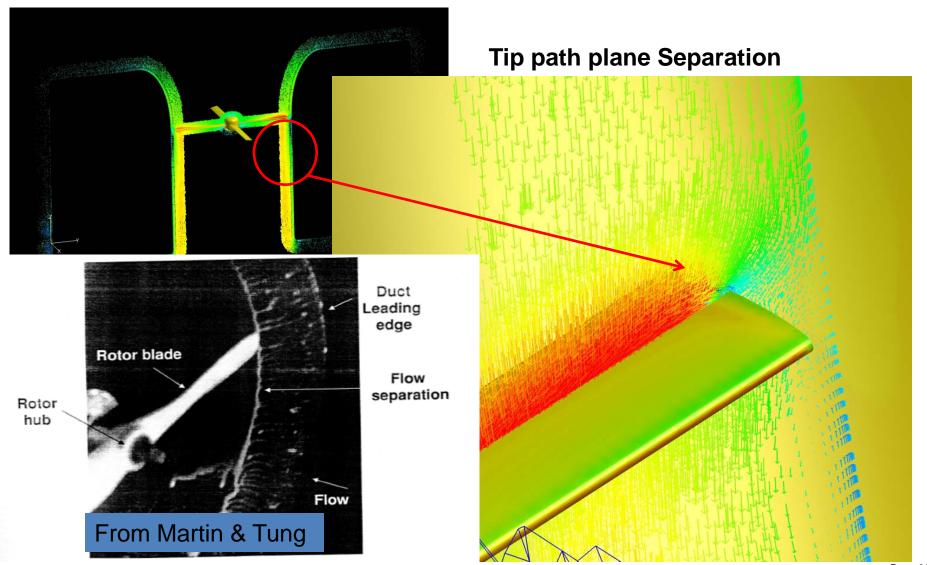
Near-Body and Adapted Off-Body Grids

ARL Ducted Fan



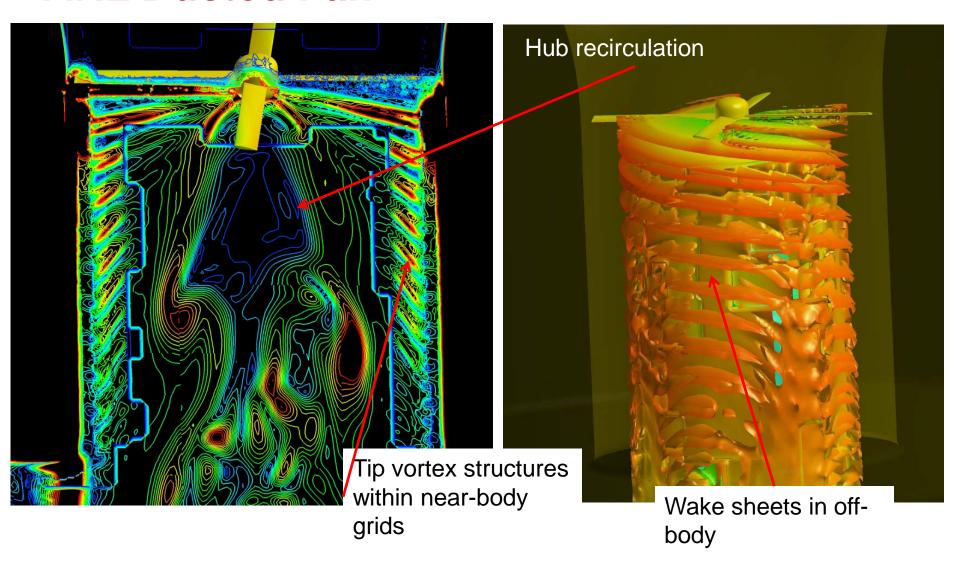
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QAT 2012 – Helios v3 ARL Ducted Fan





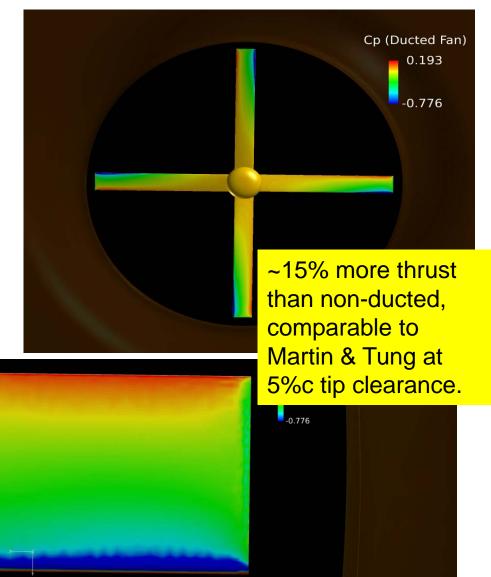
Duct Vorticity Contours ARL Ducted Fan



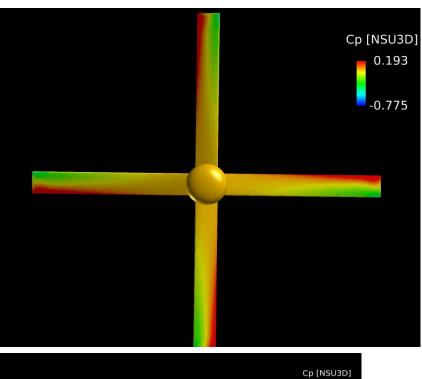
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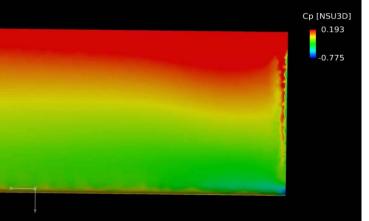
Ducted Rotor Tip Efficiency

ARL Ducted Fan



Ducted Wake







Concluding Thoughts

- First-principles hover simulations without external inputs or vortex methods have become a practical reality
- A combination of (i) High-order methods; (ii)
 Oversetting; (iii) Cartesian framework in parallel; and
 (iv) Scalable adaptive mesh refinement, such as in
 Helios enables routine first-principles hover
 computations
- For certain rotor-blades in hover, challenges remain in form of being able to resolve helical wake instability physics correctly. Some future things to looks at:
 - Resolve tip vortex core further accurately
 - Explore mechanisms to damp-out braid instabilities while still resolving the necessary part of the wake





