

Verification & Validation of Physics-Based Models for Blast Applications

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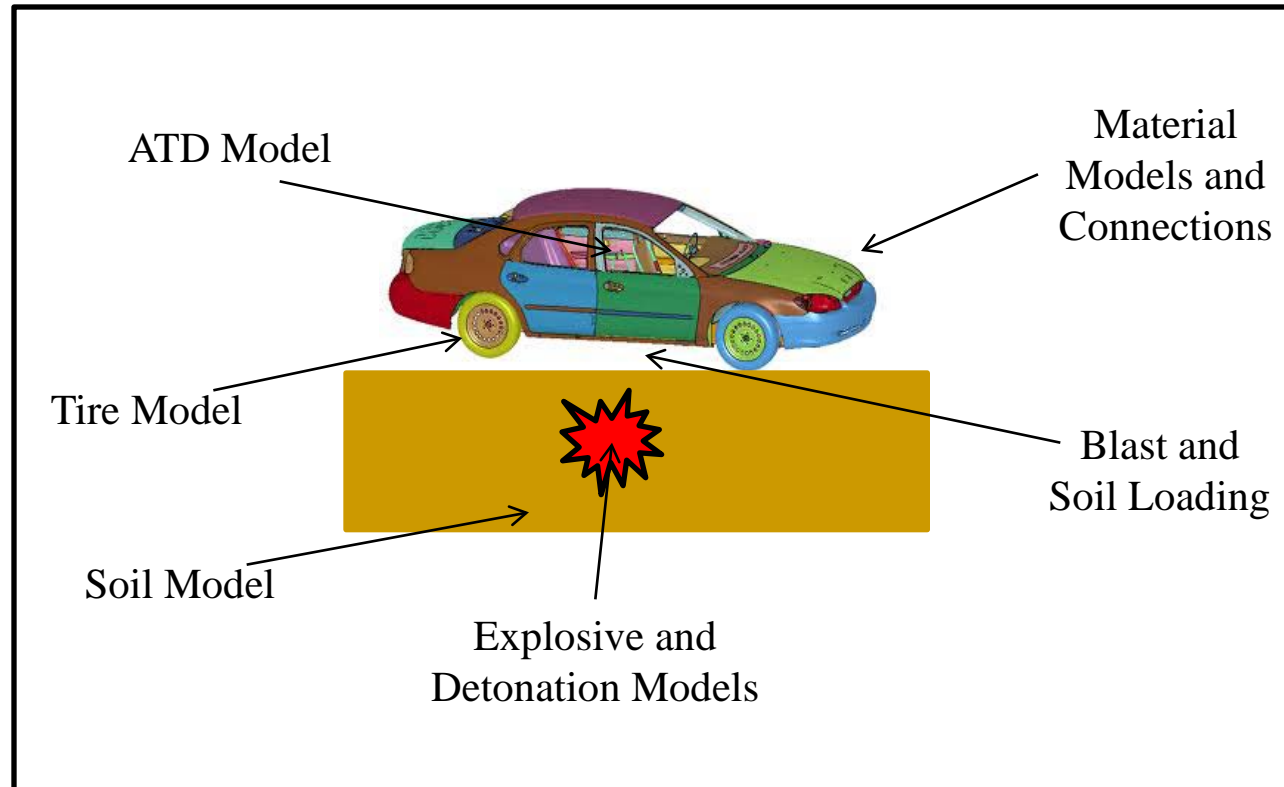
Physics-Based Modeling in Design & Development for U.S. Defense
November 5-8, 2012
Denver, CO

Purpose: Evaluate various survivability scenarios in terms of structural response and personnel injury to buried detonations

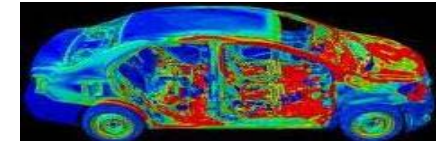
- Predict test events
- Interpolate between test events and support LFT&E planning
- Extrapolate to support survivability decisions and understand theater events

V&V used to answer:

- Is there confidence in the model?
- Is the model credible?
- Is the model fit for the intended use?



Simulation Process



Vehicle

Meshed Model

Vehicle Response

Tech data package
CAD drawing
Scans

Solve conservation equations
(mass, momentum, energy)
EOS
Constitutive models

V&V Process

Verify

- **Meshed model accurately represents production vehicle**
- Fundamental level of physics is captured

Validate

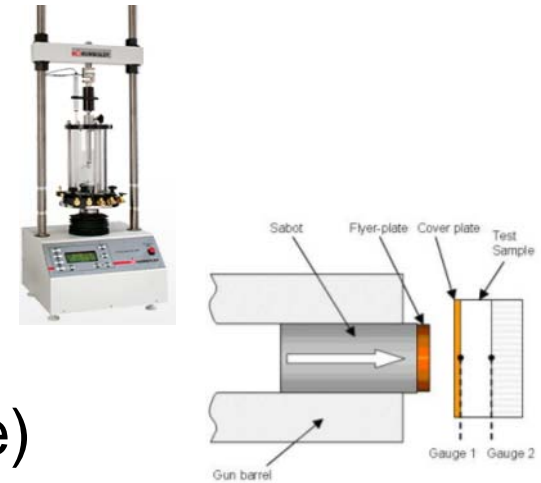
- Fundamental physics by independently predicting simple experiments
- Simulation output by comparing to live fire and theater data**

- *Did I build the thing right?*
- Ensures implemented model and its associated data accurately represent the developer's conceptual description and specification
- Verification of
 - Physics Based Models
 - Vehicle Models

Physics based models should be verified at the fundamental level, each verified independently

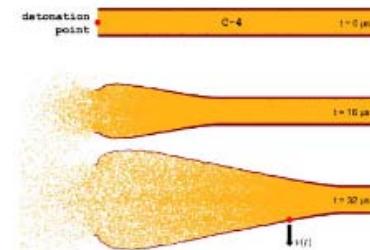
Soil Verification

- Quasi-static material characterization
- Heave tests
- Flyer plate test (high strain rate response)



Explosive Verification

- JWL EOS
- Cylinder test





Vehicle

Tech data package
CAD drawing
Scans
Technical knowledge
Manufacturing knowledge



Meshed Model

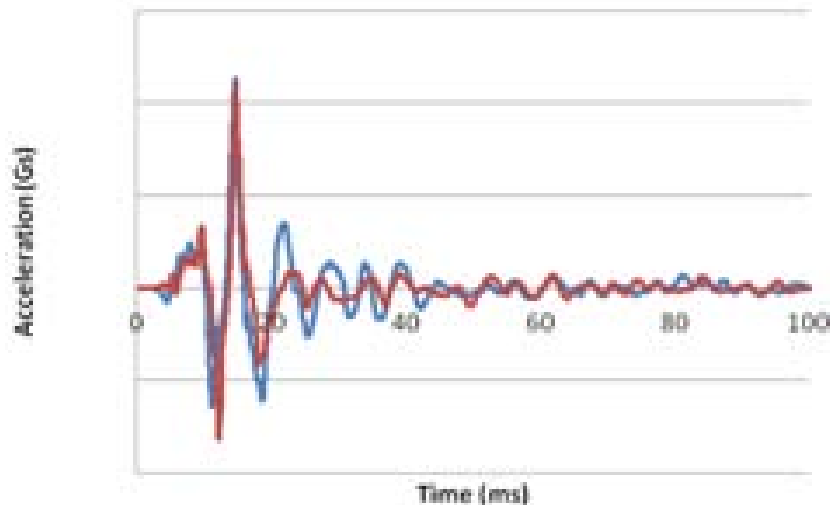
Verify meshed model
accurately represents
production vehicle

Vehicle Verification

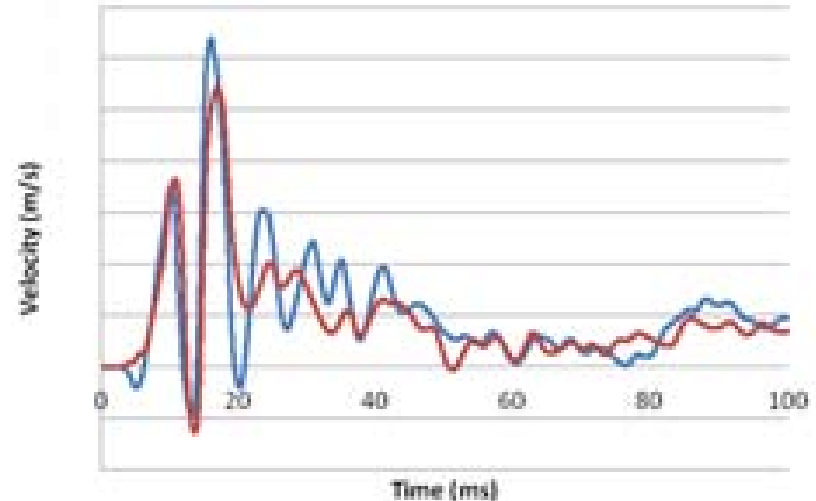
- Compare model to production vehicle
 - Gross vehicle weight
 - Dimensions
 - Center of gravity
 - Materials
 - Correctness and completeness of parts and internal equipment
- Is there enough detail?
 - Internal components
 - Connections: bolts, welds

- *Did I build the right thing?*
- Validation determines the degree to which a model or simulation accurately represents the real world from the perspective of the intended uses
- Commonly used Validation Metrics
 - Vehicle damage
 - Acceleration, velocity, and displacement time histories
 - Frequency response

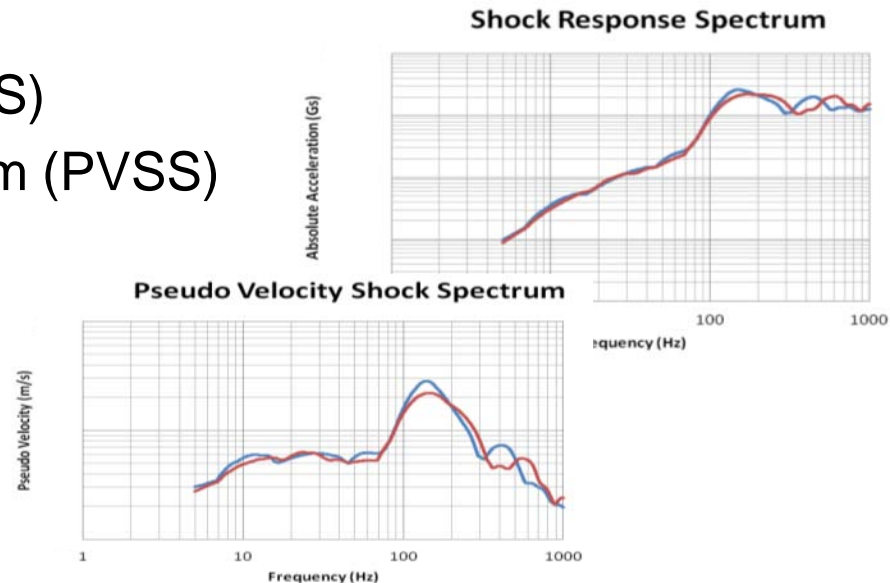
Acceleration



Velocity



- Important to match response in the frequency domain as well as the time domain
 - Matching frequencies reveals how well the model represents reality:
 - Geometry, boundary conditions, and material properties
 - Matching frequency gives an additional level of confidence
- Several options for comparing a signal's frequency response
 - Shock Response Spectrum (SRS)
 - Pseudo Velocity Shock Spectrum (PVSS)
 - Modal Analysis



- Solution to the differential equation governing the motion of a mechanical system subjected to loading from a ballistic event is expressed in terms of a Fourier series

$$A_n(t) \sin(2\pi t \omega_n + \phi_n)$$

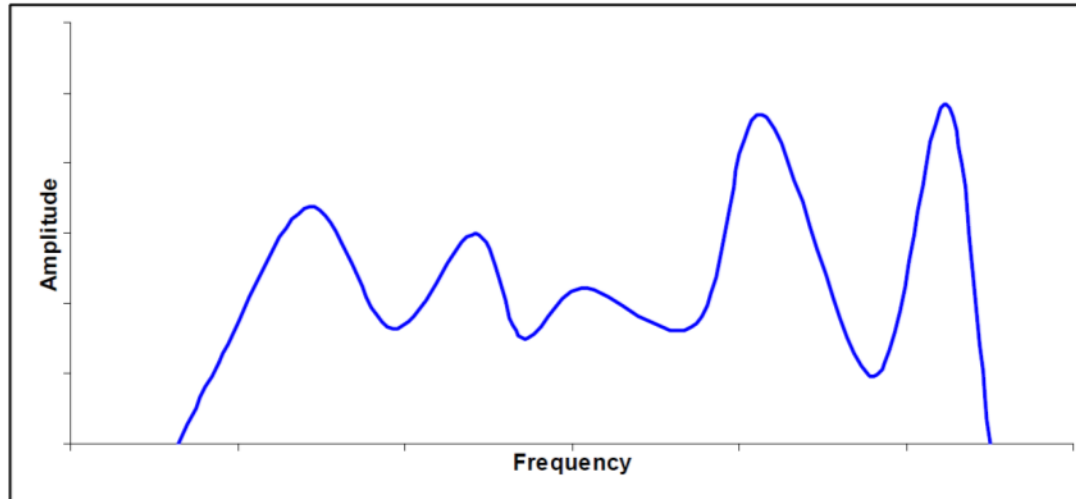
- t is time, $A_n(t)$ is the time-varying amplitude, ω is the nth-term frequency, and ϕ is the nth-term phase angle

- Fourier transform
- Takes the function $g(t)$ in the time domain and converts it to the function $G(f)$ in the frequency domain

$$G(f) = \int_{-\infty}^{+\infty} g(t) e^{-i2\pi ft} dt$$

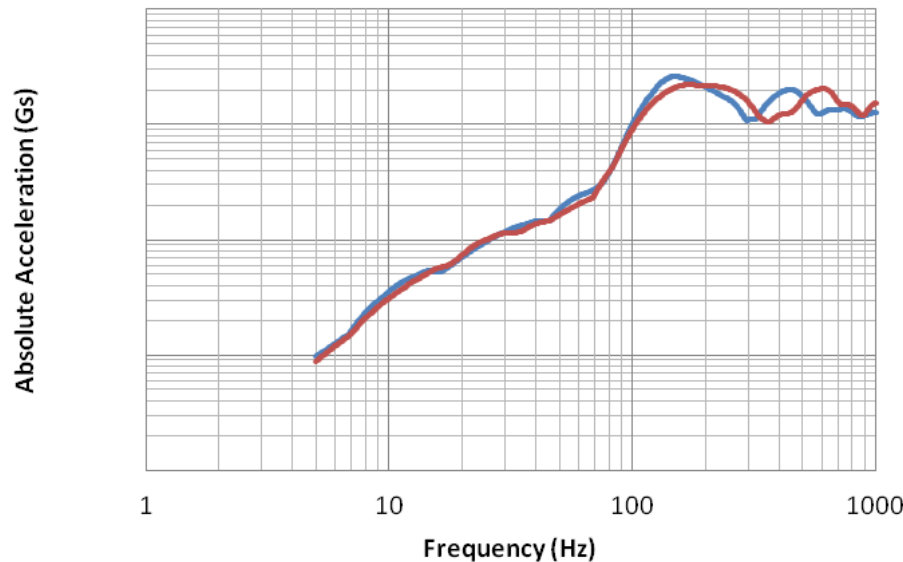
$$G(f_k) = \sum_{n=1}^{N-1} g(t_n) e^{-i2\pi \frac{k}{N} n}$$

- A plot of $|G|$ or $|G|^2$ vs frequency is called the spectrum



- Shock Response Spectrum (SRS)
 - Treats acceleration as input to single degree of freedom mass spring damper systems with various natural frequencies
 - Response represents peak accelerative response

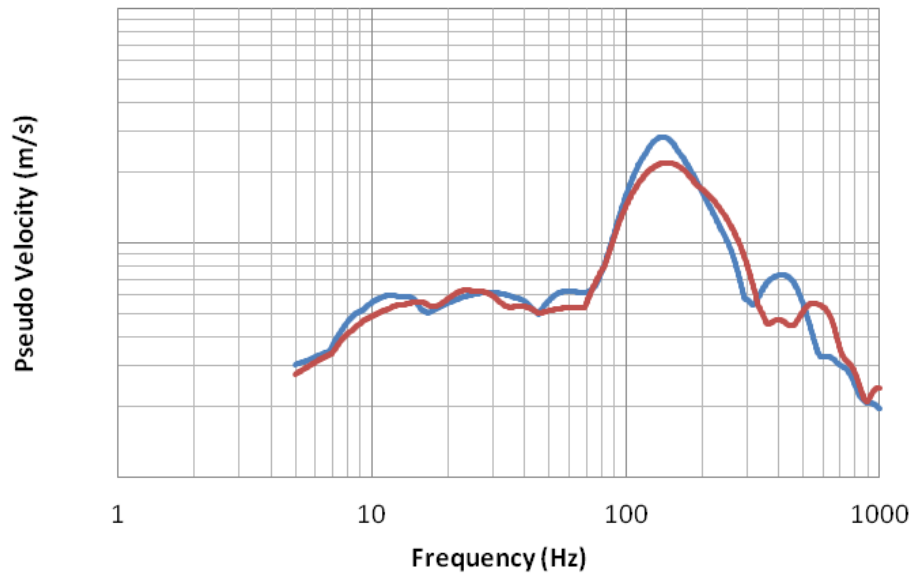
Shock Response Spectrum



*Damping Factor Q = 10 used

- **Pseudo Velocity Shock Spectrum (PVSS)**
 - Similar to the SRS, except peak velocity of each SDOF system is plotted

Pseudo Velocity Shock Spectrum



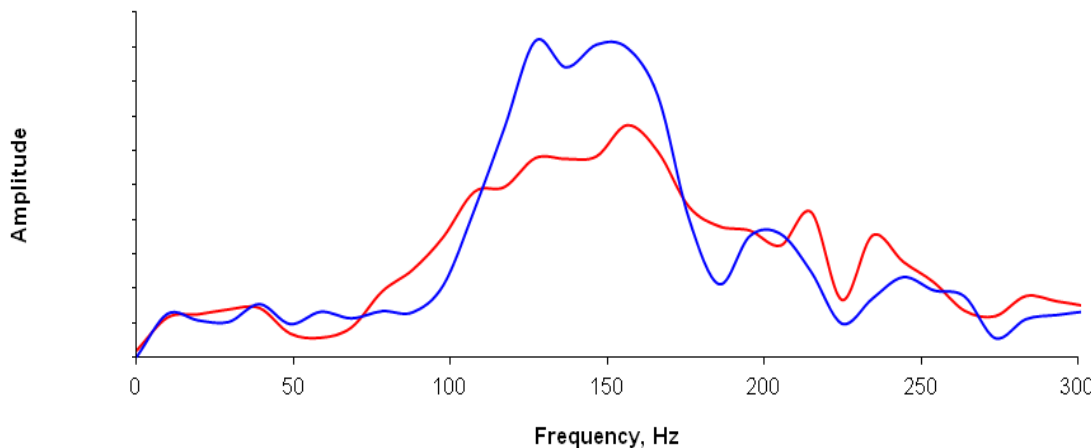
*Damping Factor Q = 10 used

Why Modal Analysis?

- SRS and PVSS
 - Might get the right answer for the wrong reason(s)
 - Summary statistics
 - No way to directly compare test to test or test to simulation
- Modal Analysis
 - Comparison of test data and simulation output is not in how well summary statistics match up, but in how well the constituent parts match up.
 - Comparison between the fundamental mathematical properties of the approximate solution to the differential equation from the simulation and the fundamental mathematical properties of the measured test data

- Alternate look at frequency content
 - Determine modal frequencies, then isolate corresponding modes
 - Modal frequencies found by performing a discrete Fourier Transform on the time series of interest – shown below
 - Regions of frequency content that most strongly influence vehicle response chosen for isolation
 - Table of regions and corresponding frequency ranges shown on right

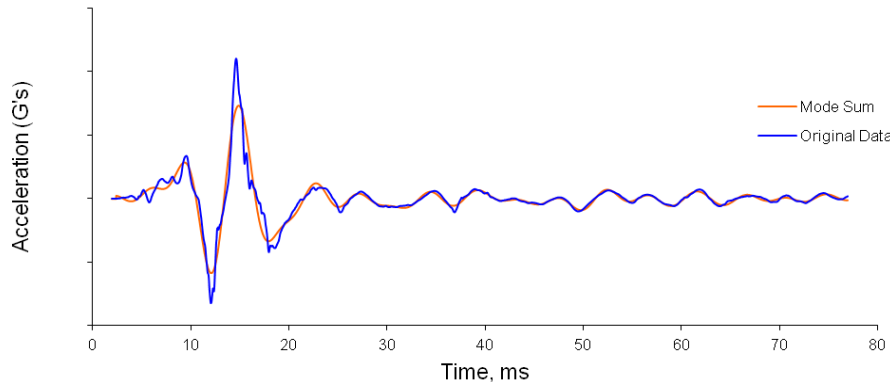
Frequency Spectrum



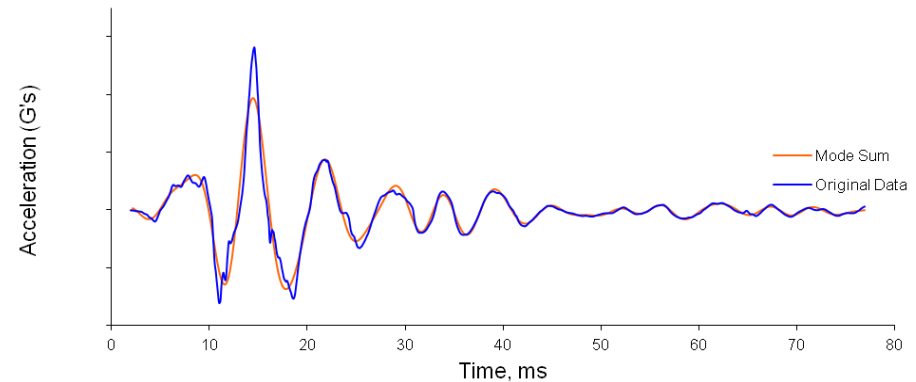
Region	Red	Blue
1	0-59	0-88
2	59-137	88-137
3	137-205	137-186
4	205-225	186-225
5	225-273	225-273

- Sufficient frequency content?
 - Removed all but the first 273 Hz of information
 - Do these modes faithfully represent the original signal?
 - Original Data vs. Mode Sum shown for both test events below
 - Effect similar to that of a low-pass filter

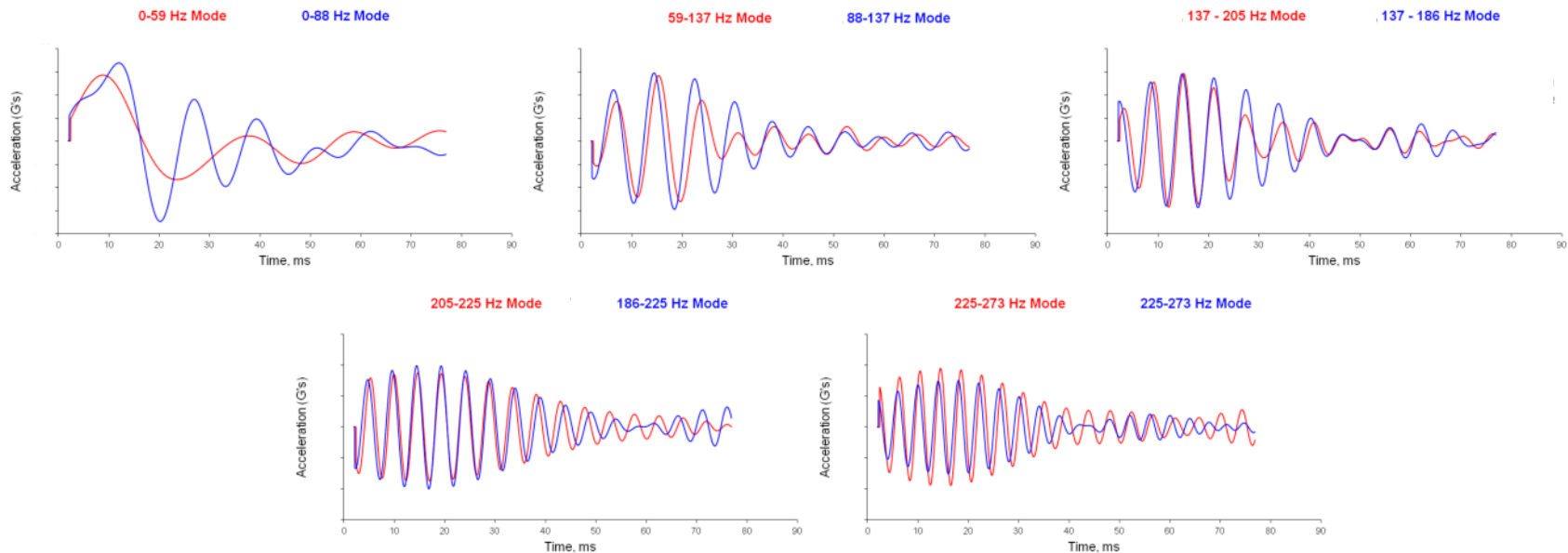
Original Data and Mode Sum



Original Data and Mode Sum



- Isolation via Filter, Transform back to Time Domain
 - Band-pass filters applied to each peak of interest
 - Filter must have very steep roll-off characteristics with minimum ripple in the pass bands and stop bands
 - Isolated spectral bands then individually transformed back into time domain, where they have sine wave-like characteristics

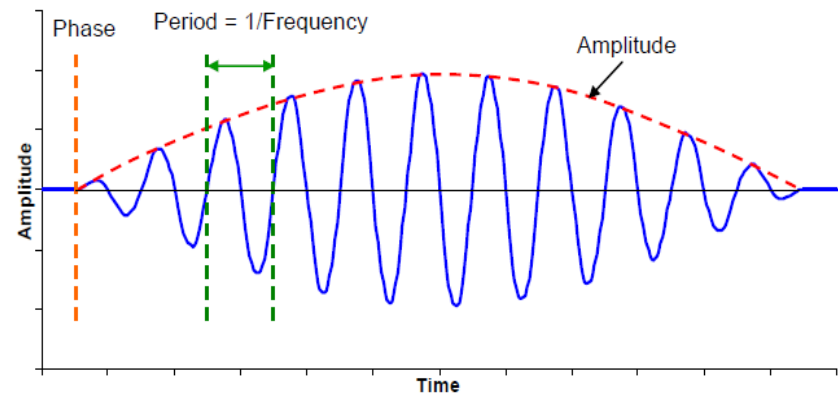


- **Representing Modes with an Equation**

- Modes shown were each sums of the close frequencies in that spectral band
- Goal: find a damped sine wave that approximates the mode, and has the form of $Y()$ and looks like the figure below

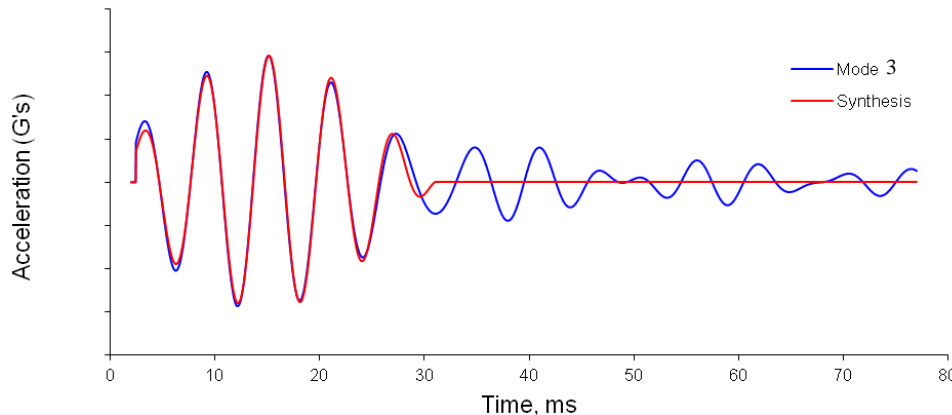
$$Y = \sum_{n=1}^5 A_n * \sin 2\pi \cdot F_n \cdot (T - T0_n) * \sin(2\pi \cdot W_n \cdot (T - ST_n) + \text{Phase}_n)$$

- Finding the equation entails choosing W_n , Phase_n , A_n , F_n , and $T0_n$, and lining up the sine wave with the modal response
- Call this the “synthesized equation”



- **Representing Modes with an Equation, cont.**
 - Example of a mode and the corresponding synthesized equation shown below
 - Red represents best attempt to match the mode with a damped wave
 - Beyond the first 30 ms, the data is of lower amplitude and is of less interest – tends to be eliminated
 - Other synthesized equations incorporate up to the first 50 ms of the mode

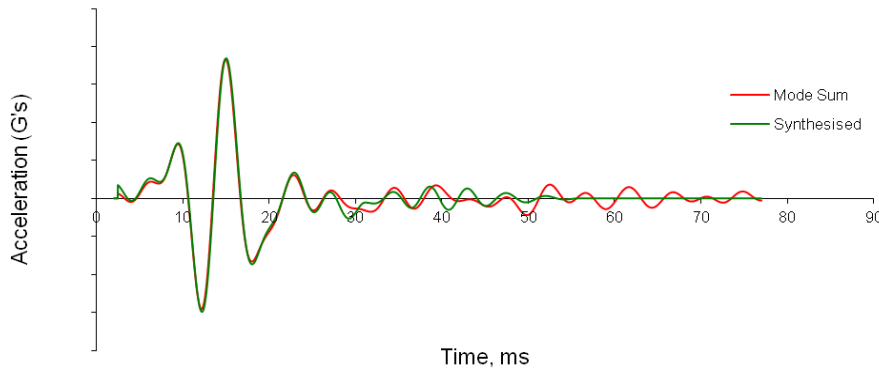
Mode 3 and Synthesis



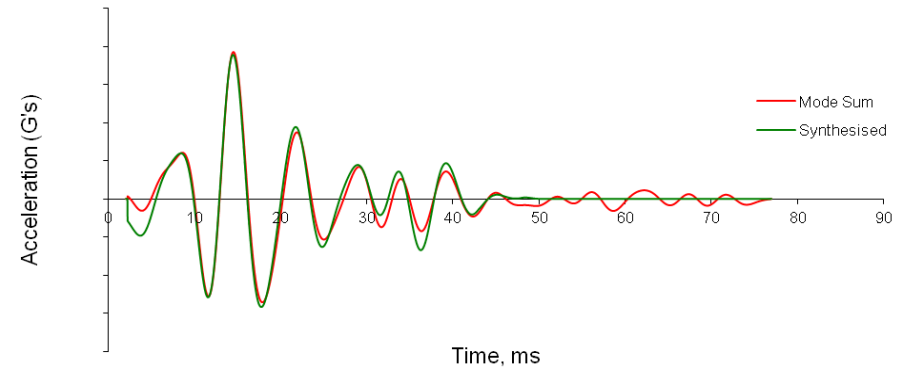
Region 3	
Range (Hz)	137-205
A (gs)	292.7
F (Hz)	15.63
T0 (sec)	-0.001
W (Hz)	167
Phase (Ra)	0.785
ST (sec)	0.002425
ET (sec)	0.031025
Start (msec)	-1
Duration (msec)	32
Amp Adj	1

- Modal equations added
 - The five modal equations added together will approximate the mode sum, which in turn approximates the original time series data
- Mode Sum and Synthesized Sum
 - First 50 ms lines up very well

Mode Sum and Synthesized Sum



Mode Sum and Synthesized Sum



Comparison Process

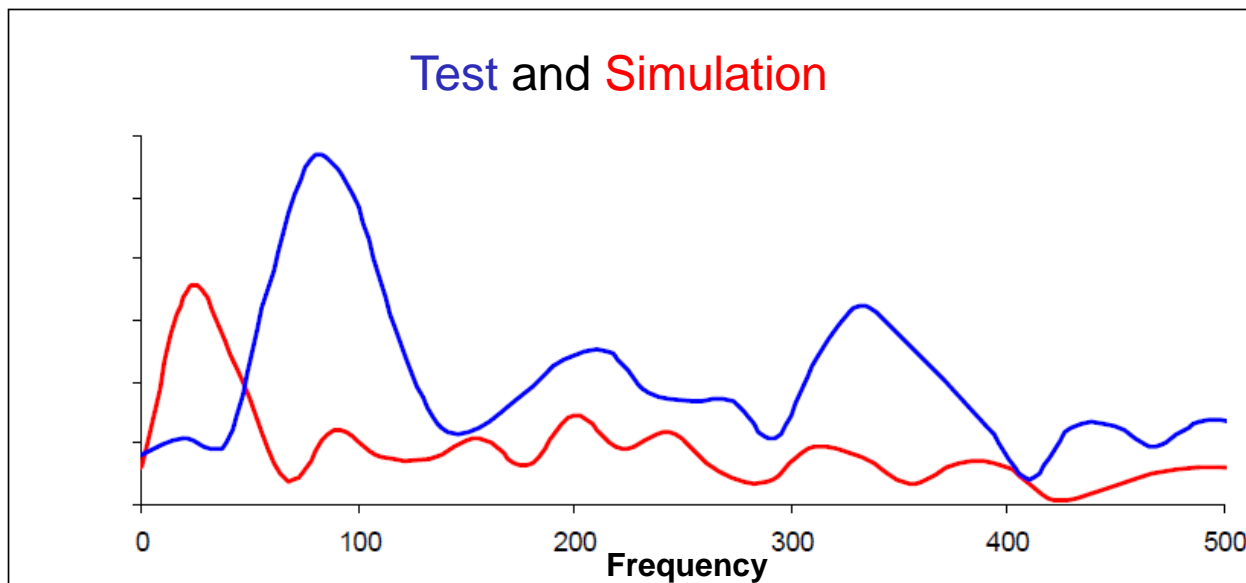
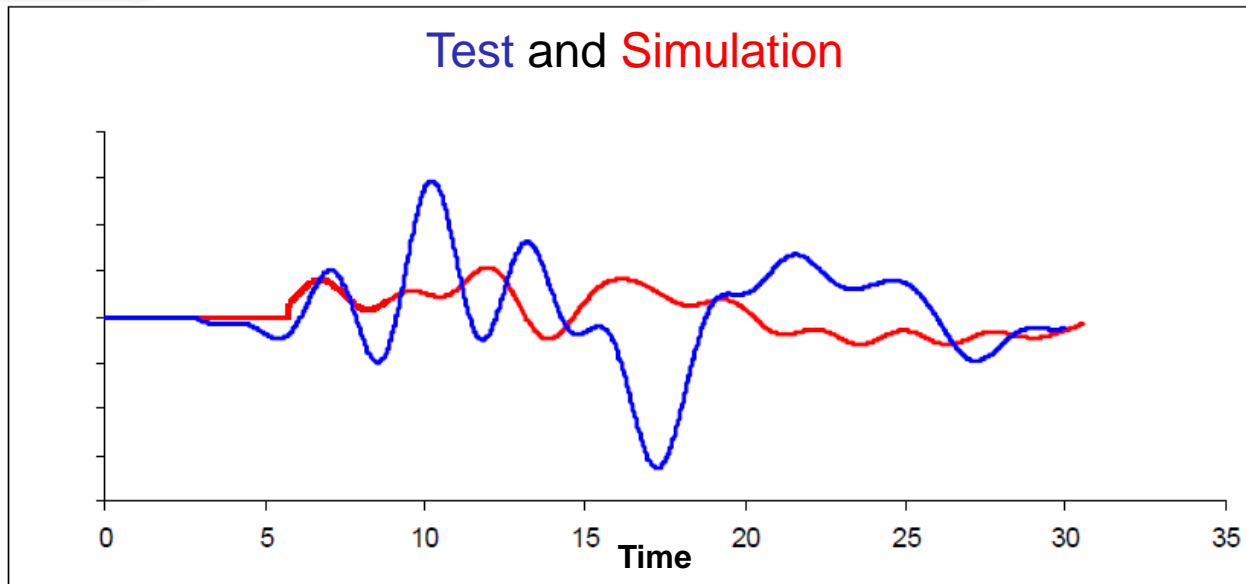
- 1) Isolate the first several terms of the time series for the test data and for the simulation output
- 2) Compare the frequency spectra and decide which frequency ranges are to be isolated
- 3) Isolate those frequency ranges in both data sets and compare the terms for frequency, phase, and amplitude content.
- 4) Derive the equations for the components of both the simulation output and the test data to compare the three parameters and understand how close they are to actual terms of the Fourier series and to one another.

Comparison Process Continued

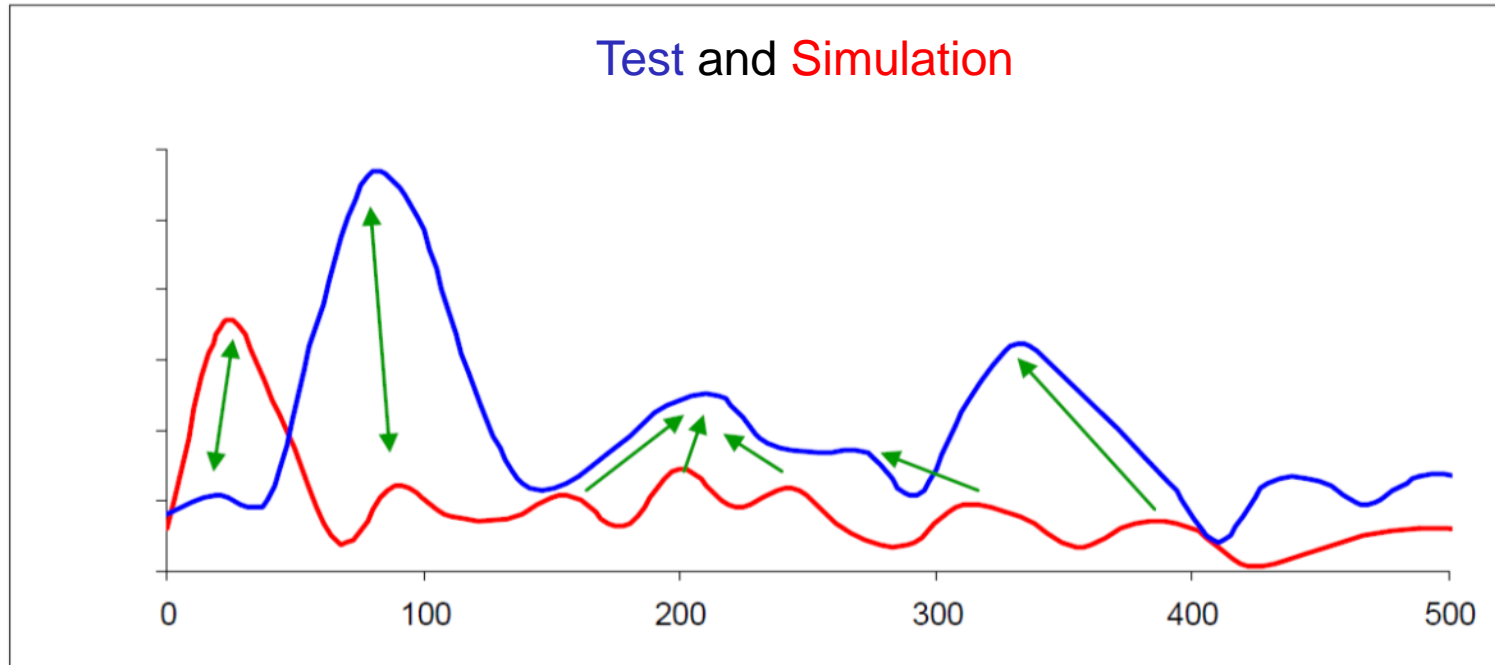
- (5) Amplitude- and phase-adjust the components of the simulation output, if and as necessary, to match those of the test data;
- (6) Compare the sums of the resulting components for curve shape and timing (phasing).

- Good agreement in frequency content indicates a good understanding of the geometric and material properties of the system.
- Good agreement in phasing indicates a good understanding of the relative timing of the events and the path through the structure from the point of application of the force to the analytical point.
- Good agreement in amplitude indicates a good understanding of the system damping and the presence of the considerable luck (that is, the test event happened to produce the same force as was assumed in the FEM simulation).

Example: Modal Analysis Validation



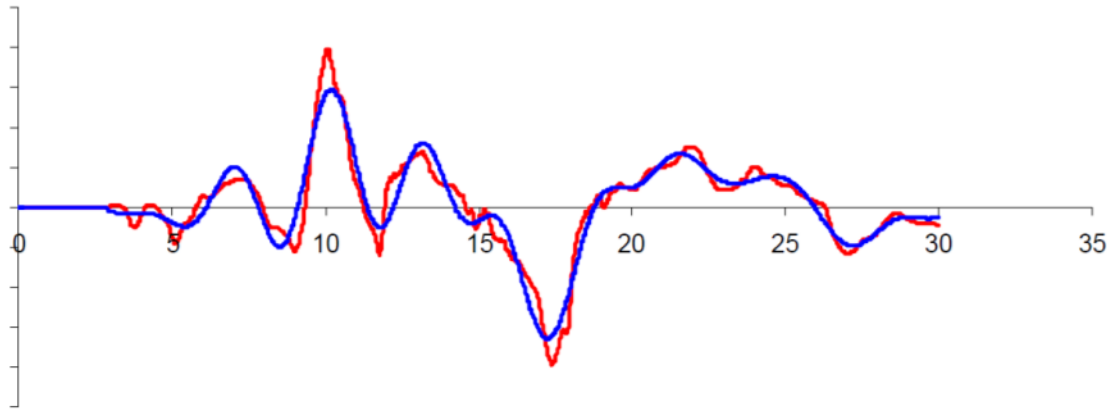
Example: Modal Analysis Validation



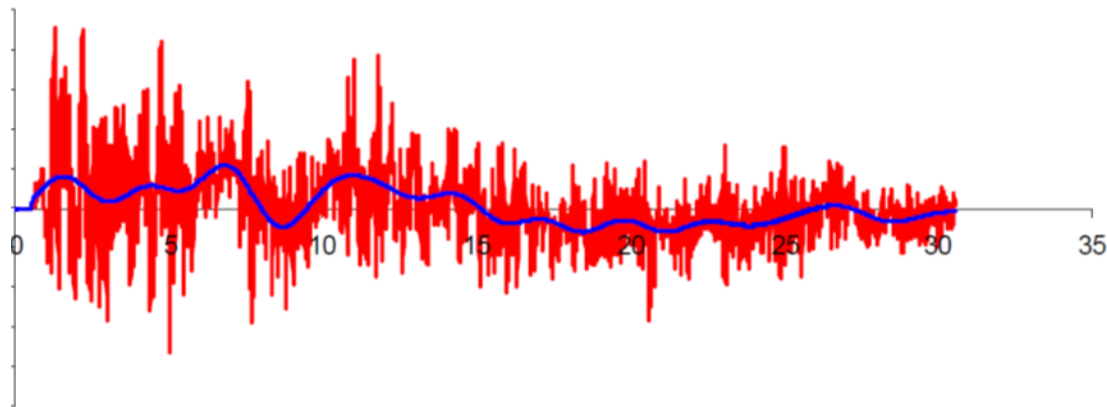
Regions	Test	Sim	Sim Adj
1	0-39	0-67	0-67
2	39-156	67-133	67-133
3	156-254	133-178	133-289
4	254-293	178-222	289-355
5	293-410	222-289	355-422
6		289-355	
7		355-422	

Example: Modal Analysis Validation

Test and Test (0-410)

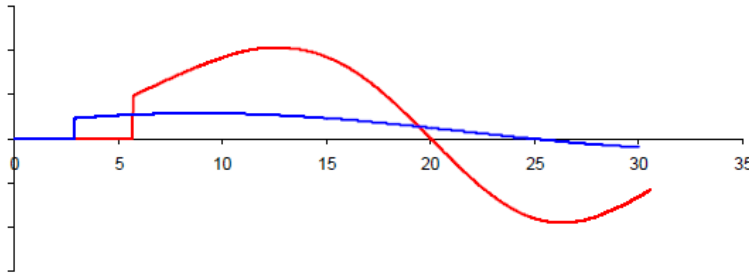


Simulation and Simulation (0-422)

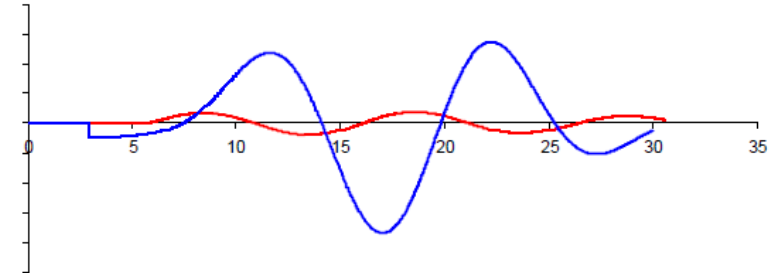


Example: Modal Analysis Validation

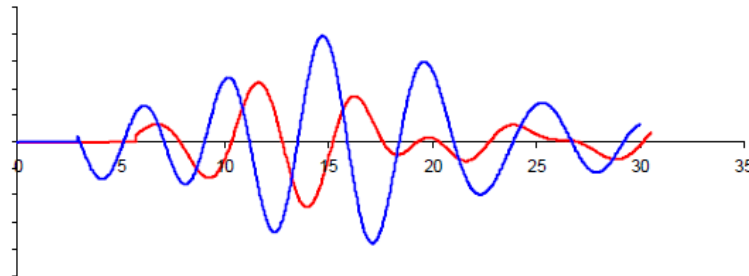
Test (0-39) and Sim (0-67)



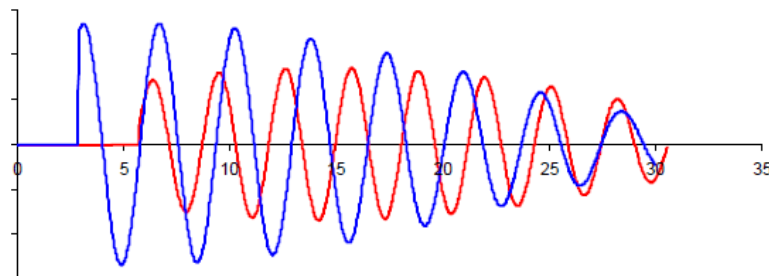
Test (39-156) and Sim (67-133)



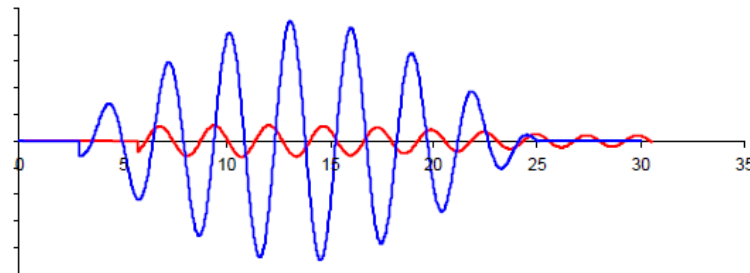
Test (156-254) and Sim (133-289)



Test (254-293) and Sim (289-355)



Test (293-410) and Sim (355-422)

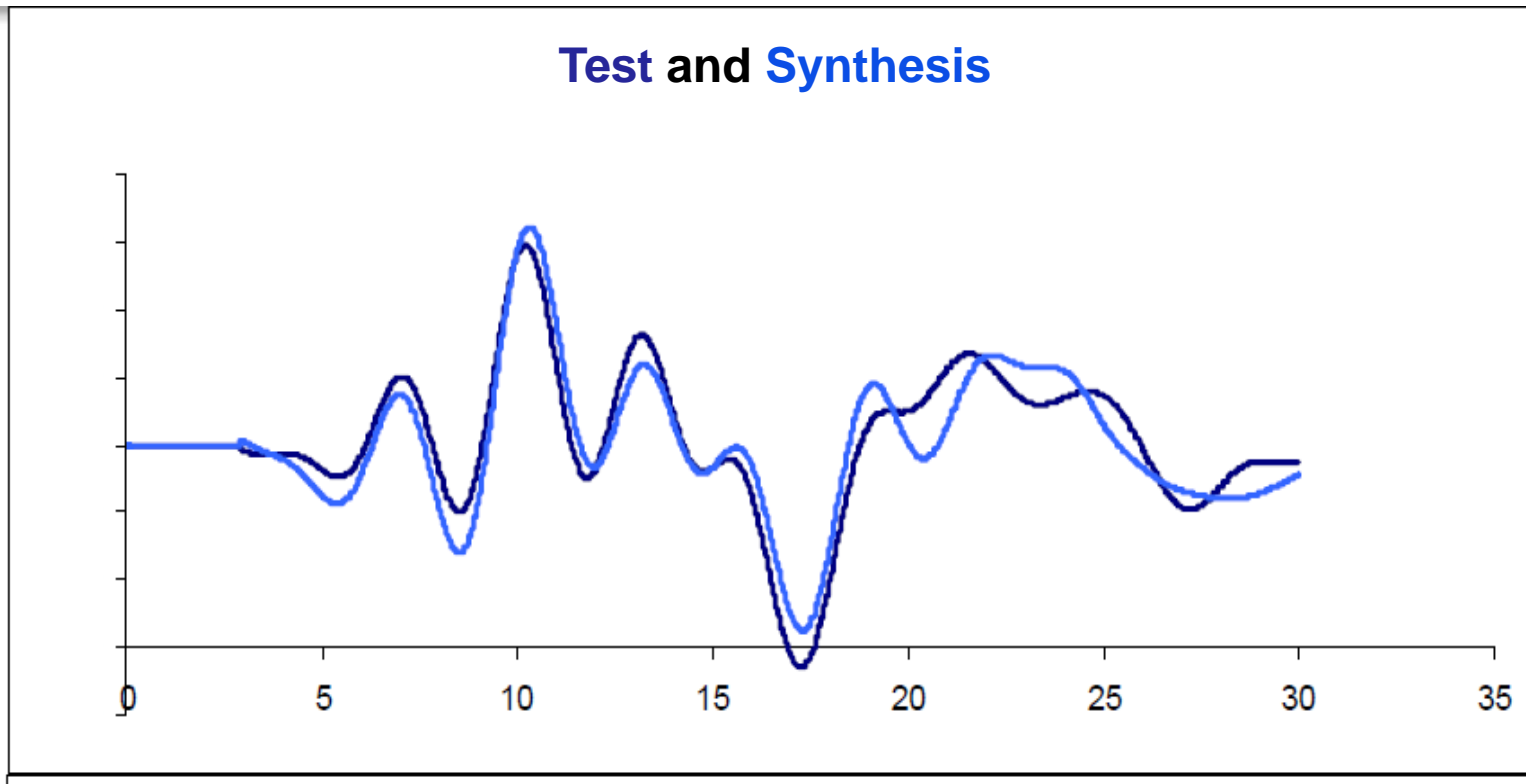


Example: Modal Analysis Validation

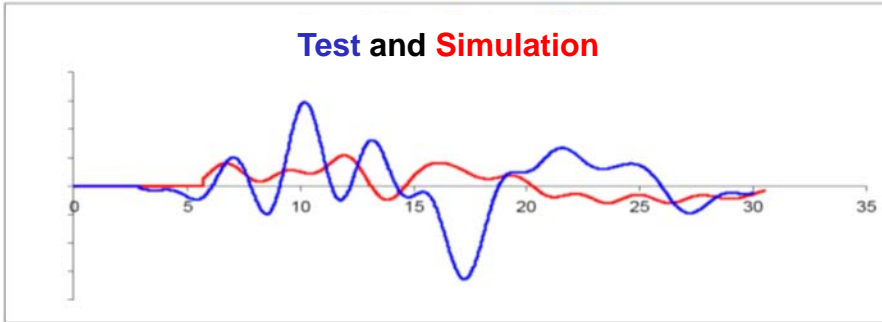
$$Y = \sum_{n=1}^5 A_n * \sin(2\pi * F_n * (T - T_{0n})) * \sin(2\pi * W_n * (T - ST_n) + \text{Phase}_n)$$

SIM	0-67	67-133	133-289	289-355	355-422
A (gs)	102.652	38.471	110.466	33.793	29.446
F (Hz)	7.14857	9.61538	33.3333	11.3636	12.5
T0 (sec)	-0.02	-0.017	0	-0.012	-0.014
W (Hz)	35	97	200	320	383
Phase (Ra)	0.087266	6.25416	0.69813	0.34906	5.28459
ST(sec)	0.000055	0.00055	0.00055	0.00055	0.00055
ET (sec)	0.030536	0.030536	0.015004	0.030536	0.026004
Start (msec)	-20	0	0	-12	-14
Duration (msec)	70	15	15	44	40
Amp Adj	1	1	1	1	1
Rev Amp Adj	0.35	5	1.7	1.4	5
Test	0-39	39-156	156-254	254-293	293-410
A (gs)	31.66	274.081	196.984	53.637	225.739
F (Hz)	10	14.28571	20	11.11111	21.73913
T0 (sec)	-0.01	0	0.001	-0.015	0.002
W (Hz)	14	87	230	285	340
Phase (Ra)	1.29154	3.31613	3.14159	0.69813	4.90018
ST(sec)	0.002875	0.002875	0.002875	0.002875	0.002875
ET (sec)	0.03	0.03	0.026025	0.03	0.025025
Start (msec)	-10	0	1	-15	2
Duration (msec)	50	35	25	45	23
Amp Adj	1.1	1	1	1	1

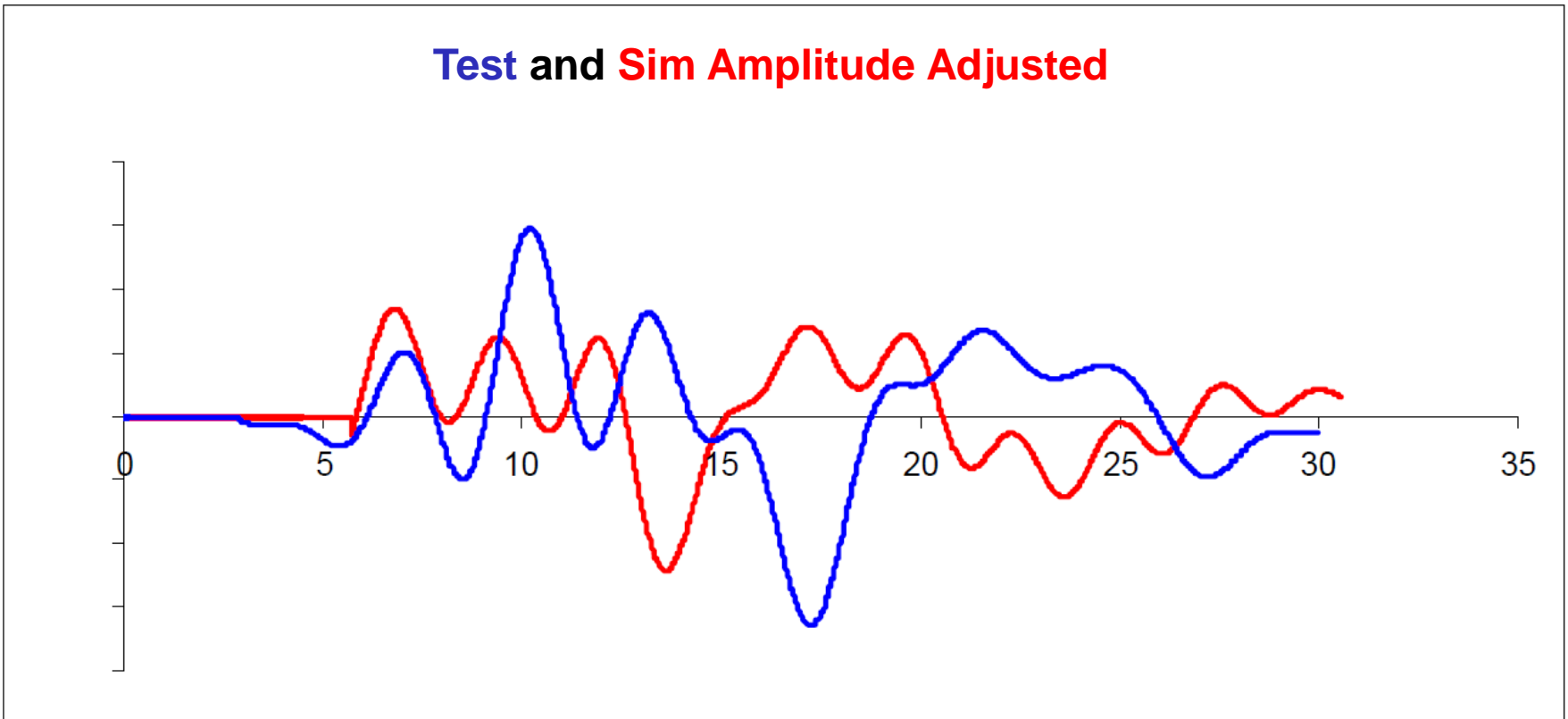
Example: Modal Analysis Validation



Example: Modal Analysis Validation

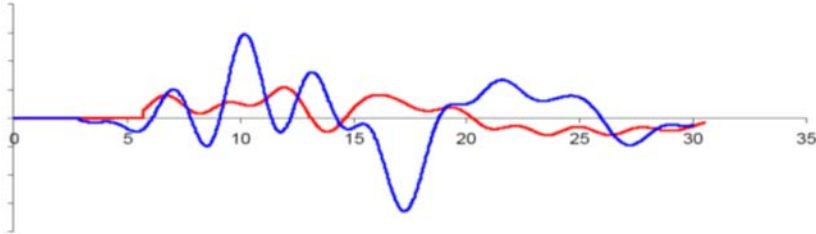


	0-67	67-133	133-289	289-355	355-422
Amp Adj	0.35	5	1.7	1.4	5

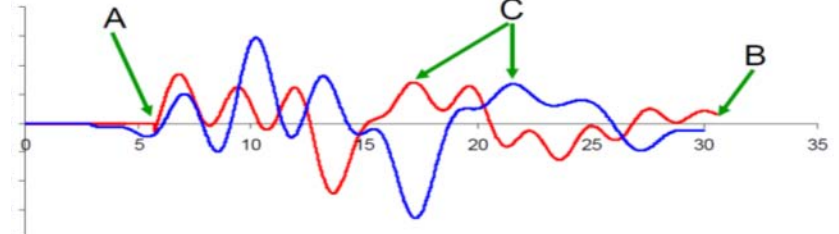


Example: Modal Analysis Validation

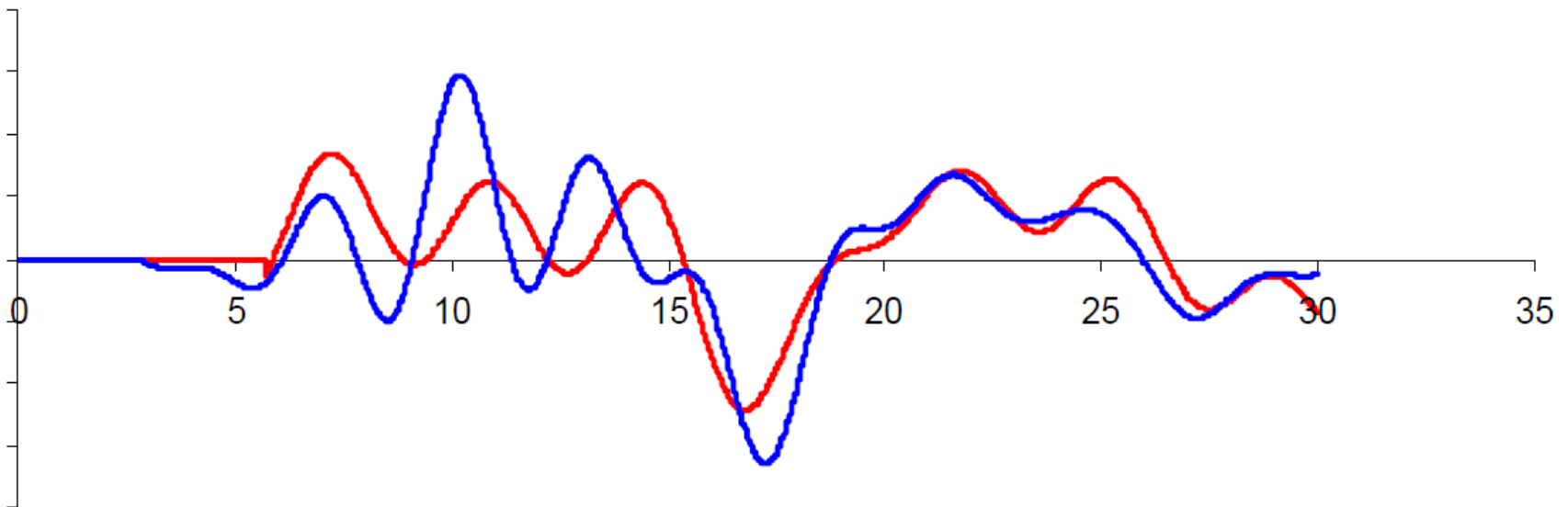
Test and Simulation



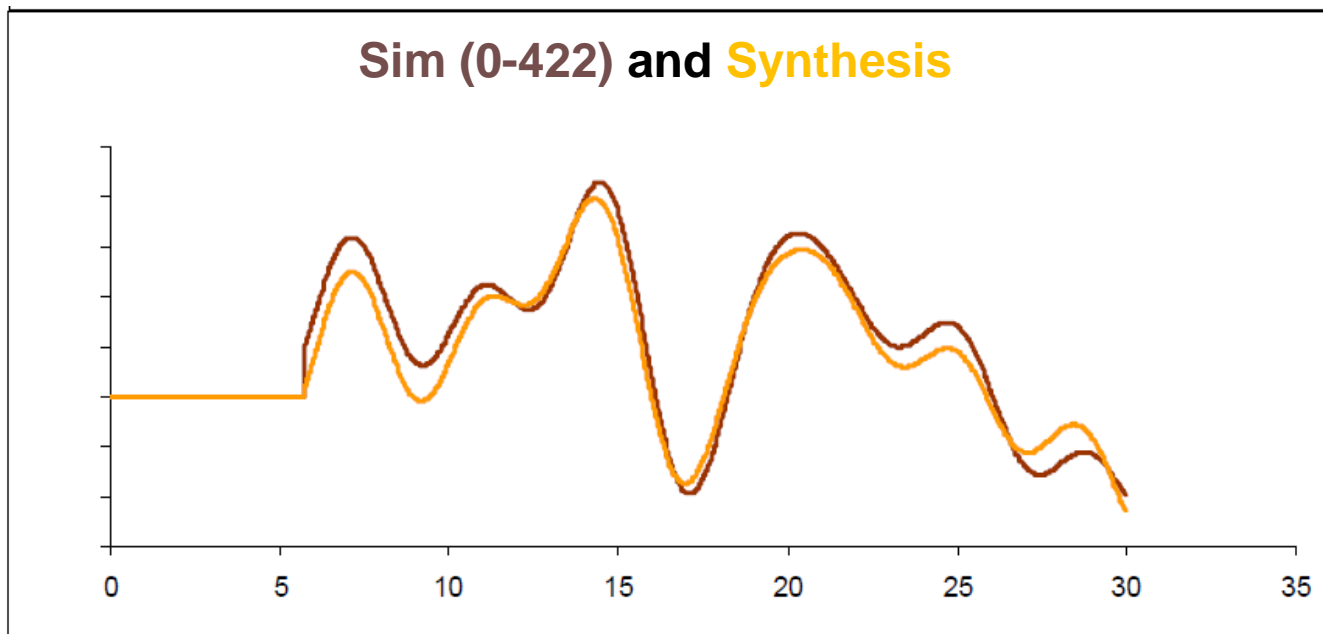
Test and Sim Amplitude Adjusted



Test and Sim Amplitude Adjusted and Time-Stretched

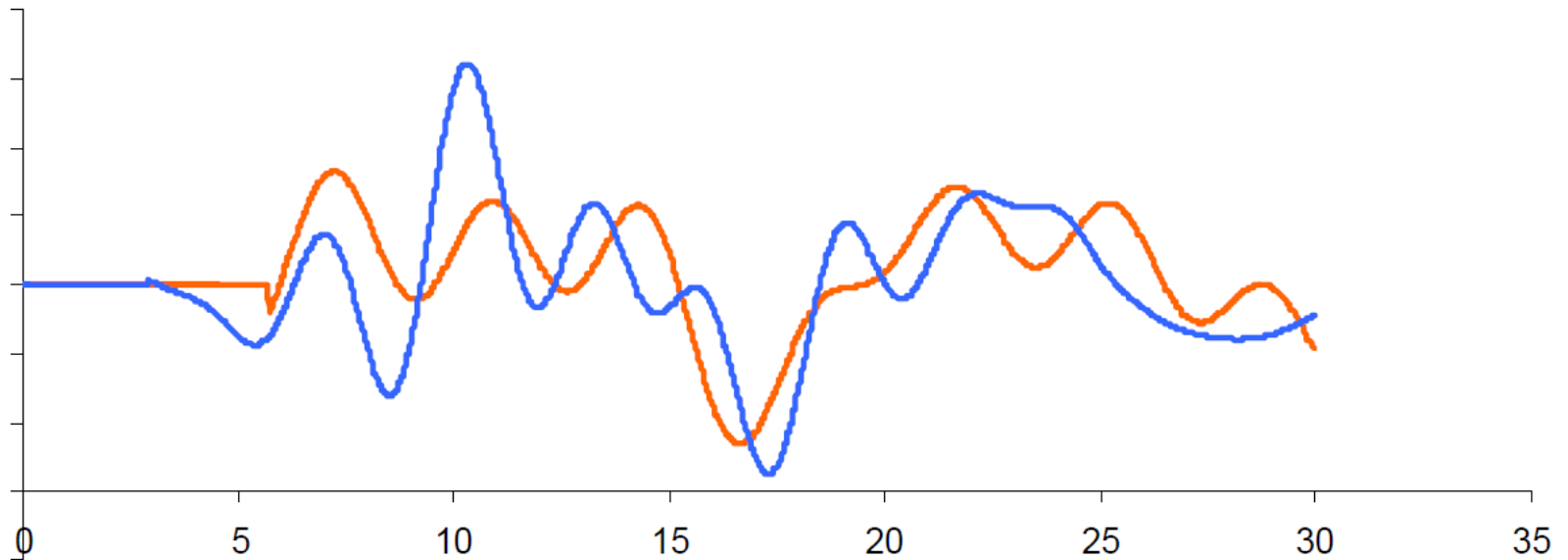


Example: Modal Analysis Validation



Example: Modal Analysis Validation

Synthesis **Test** and **Simulation** (Amp and Time adjusted)



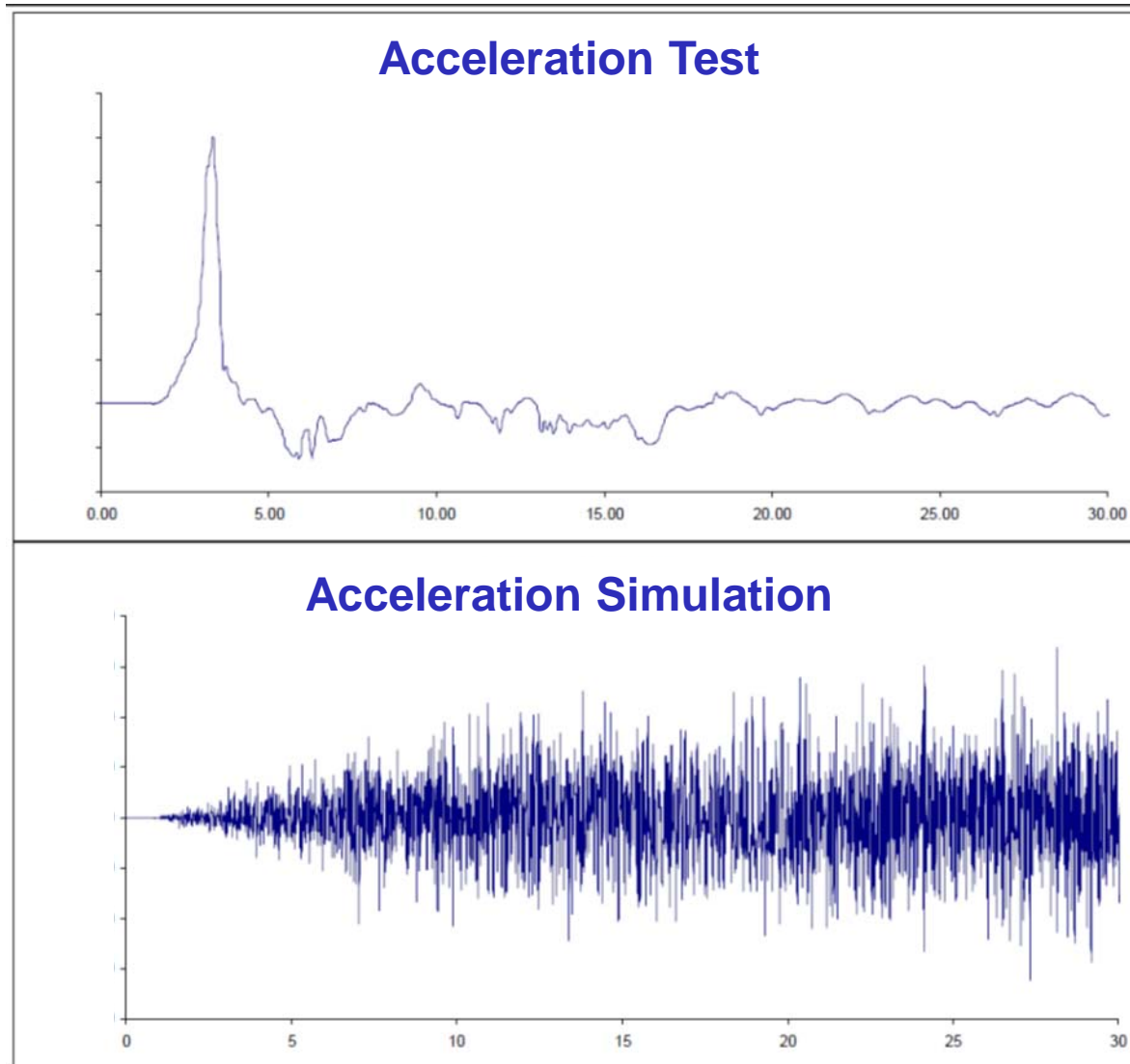
Conclusion

- Shape of simulation data curve is quite good
- Timing (phasing) and amplitude show some differences
- Actual system-level response is slower than predicted in the simulations
- System damping is not well modeled at lower frequencies

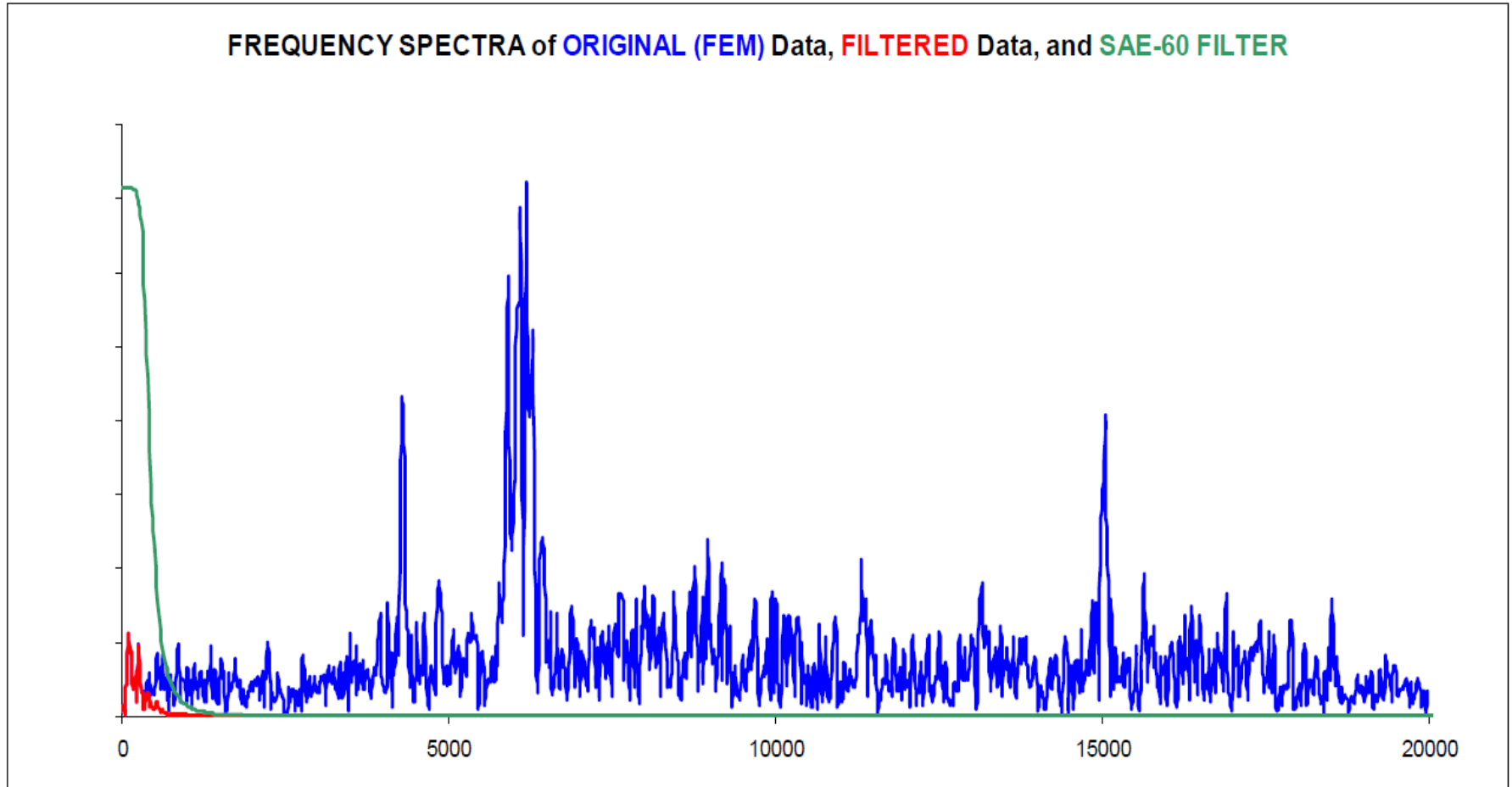
Other considerations

- Variability and uncertainty in tests
- Not the answer, but an answer
- Instrumentation: LOFFI accelerometers
- Vehicle condition/variation vehicle to vehicle

Example of Bad Simulation Output

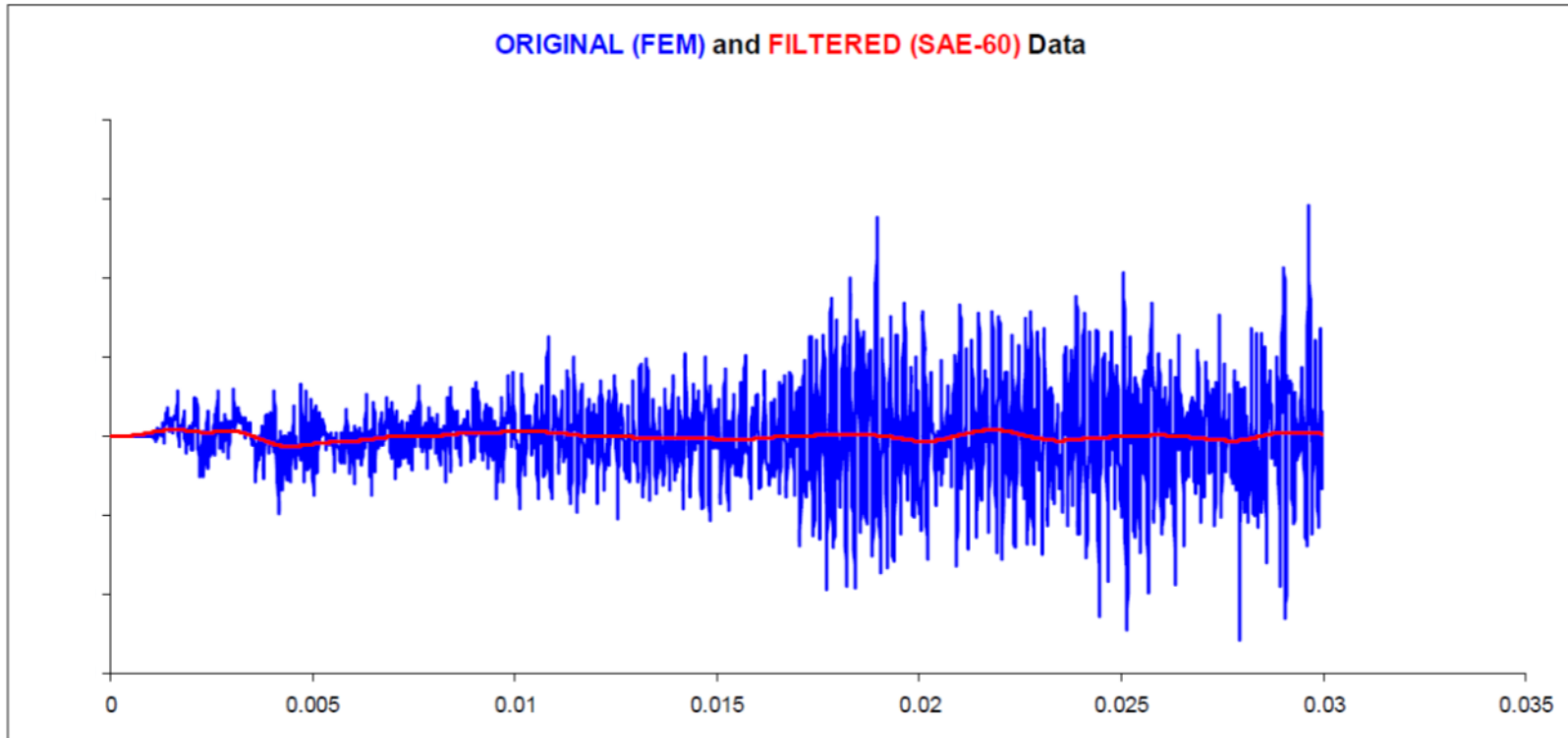


Example: Selecting an Appropriate Filter



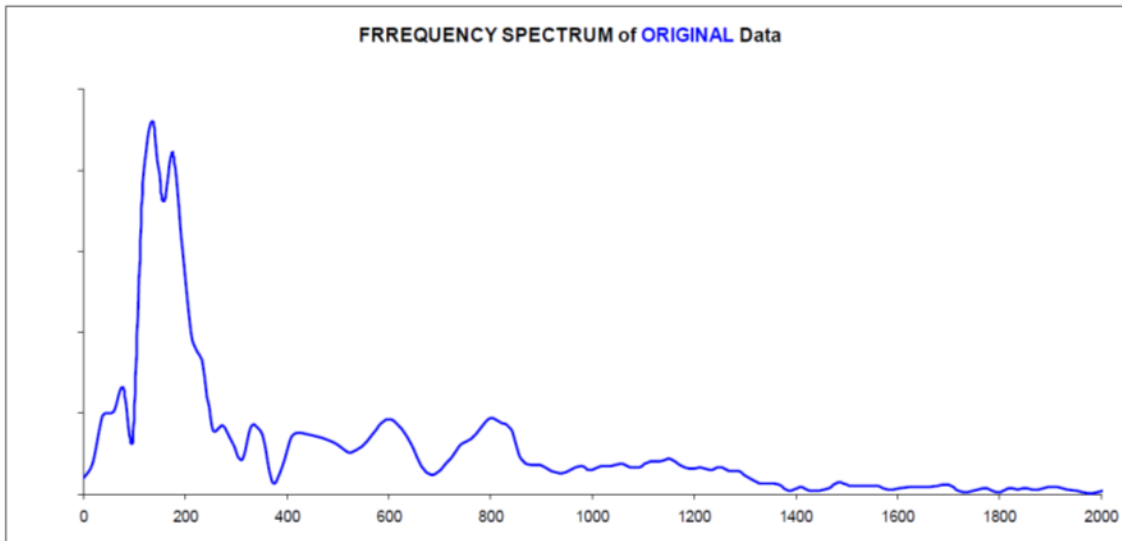
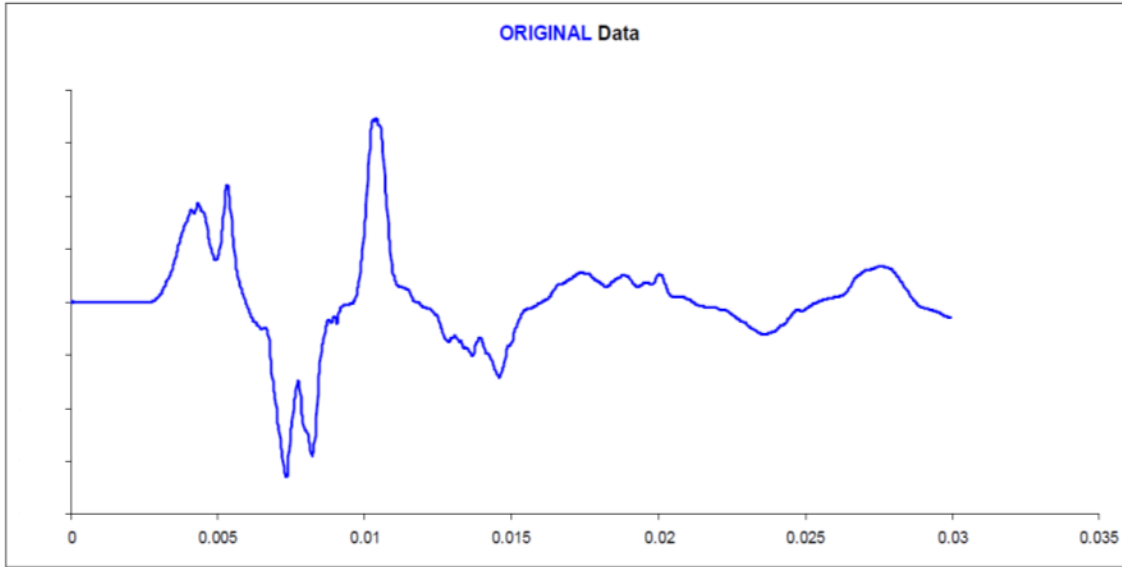
Frequency spectra of FEM output, SAE-60 filter and filtered data

Example: Selecting an Appropriate Filter

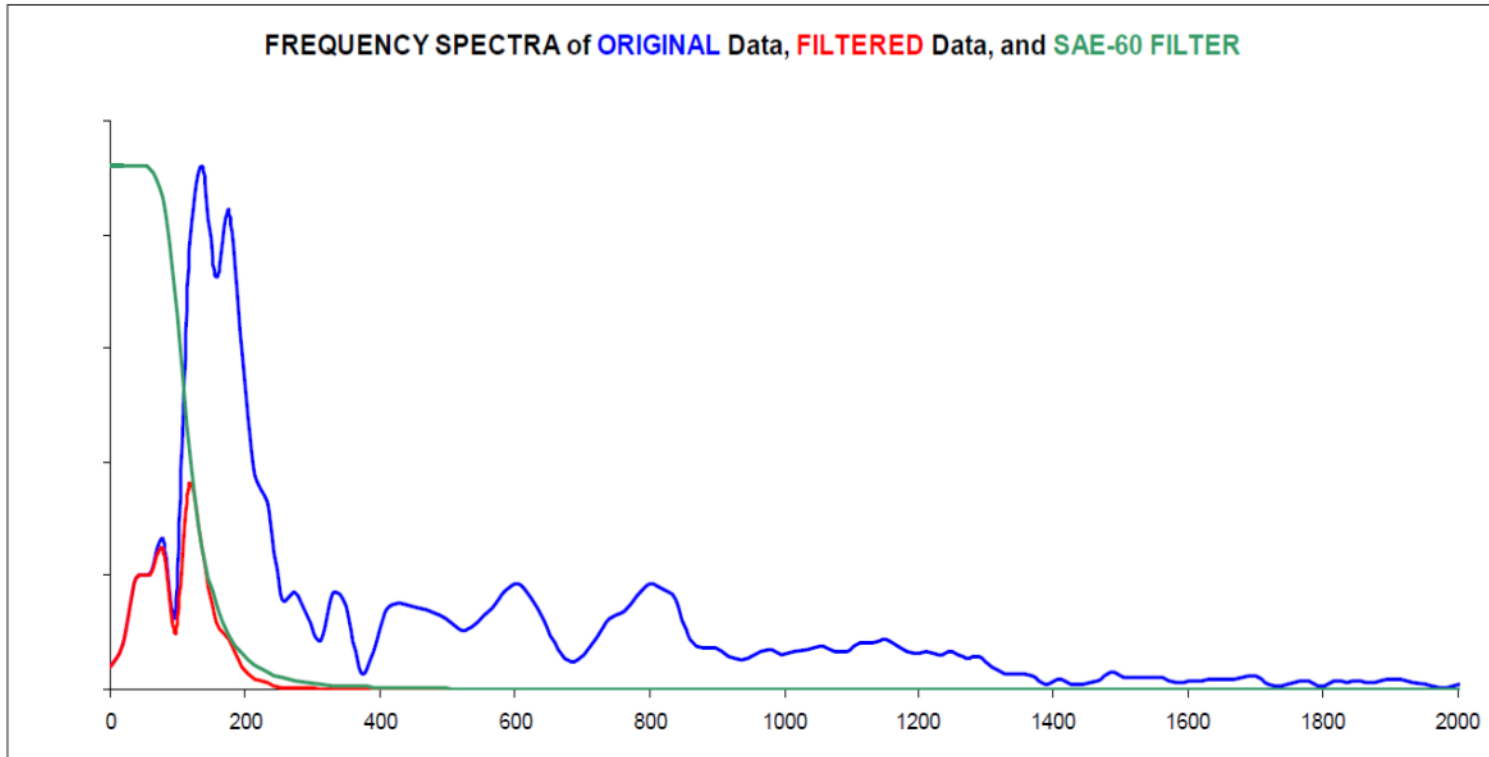


Time history of simulation output, and SAE-60 filtered data

Example: Selecting an Appropriate Filter

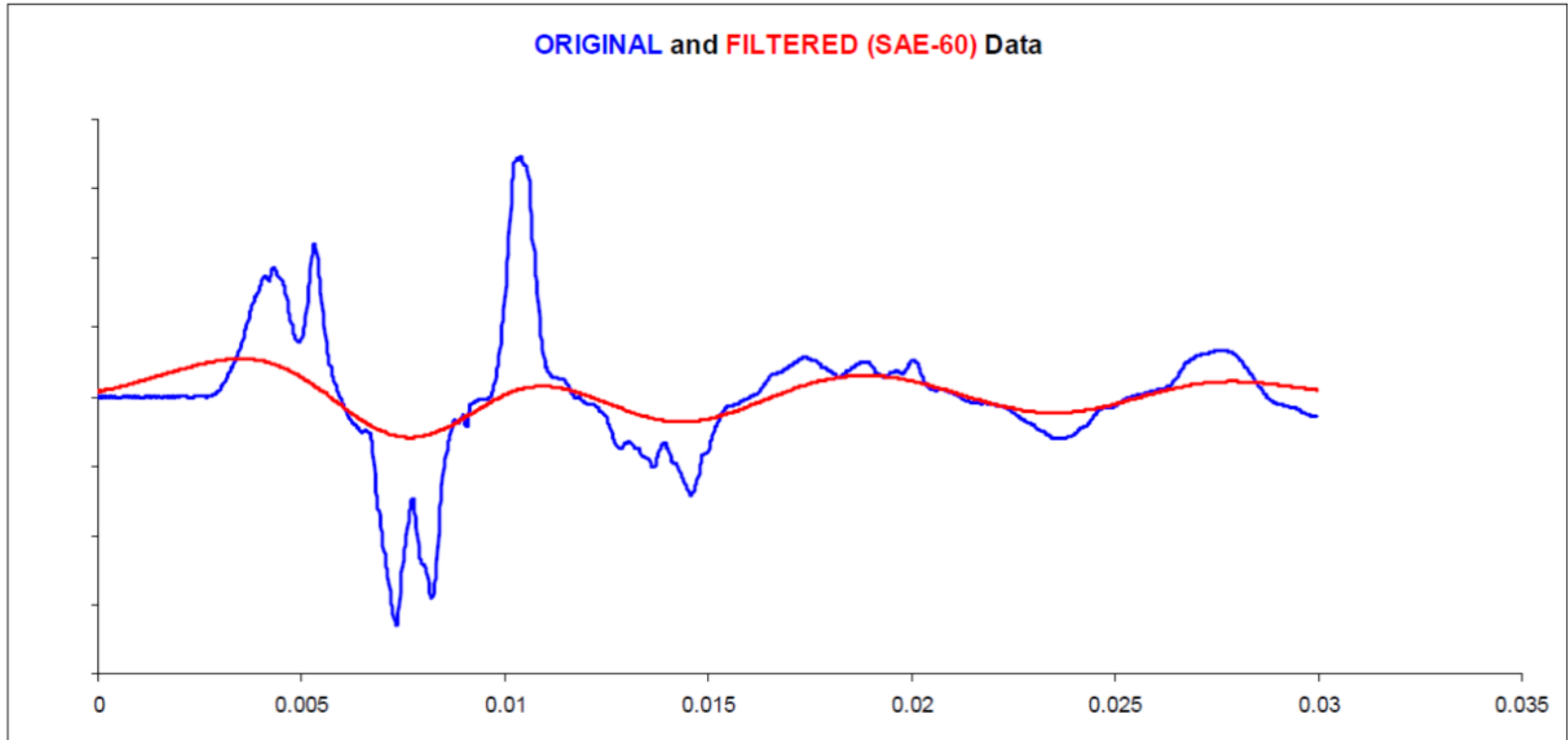


Example: Selecting an Appropriate Filter



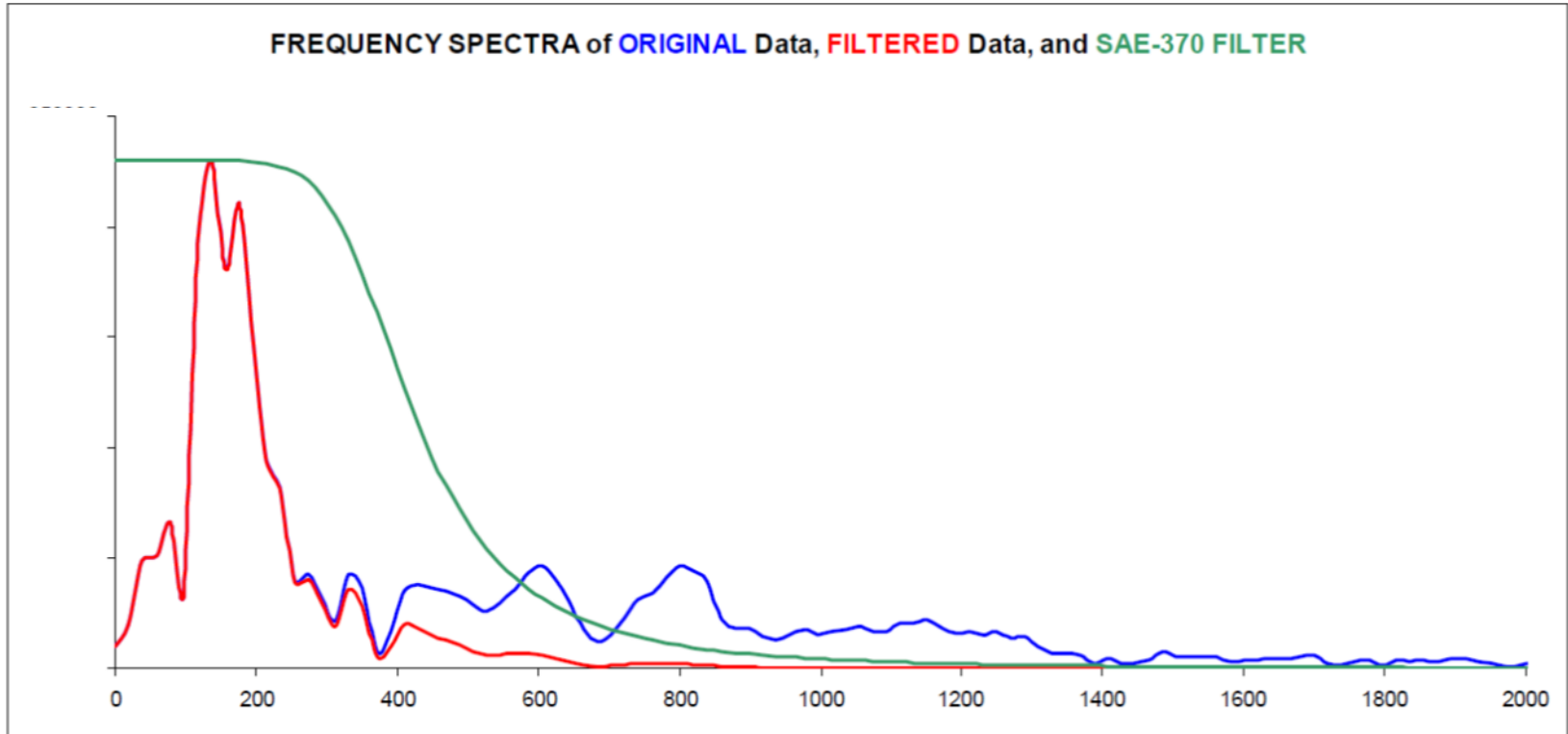
Frequency spectra of acceleration from test along with filter and filtered data spectra (SAE-60 filter)

Example: Selecting an Appropriate Filter



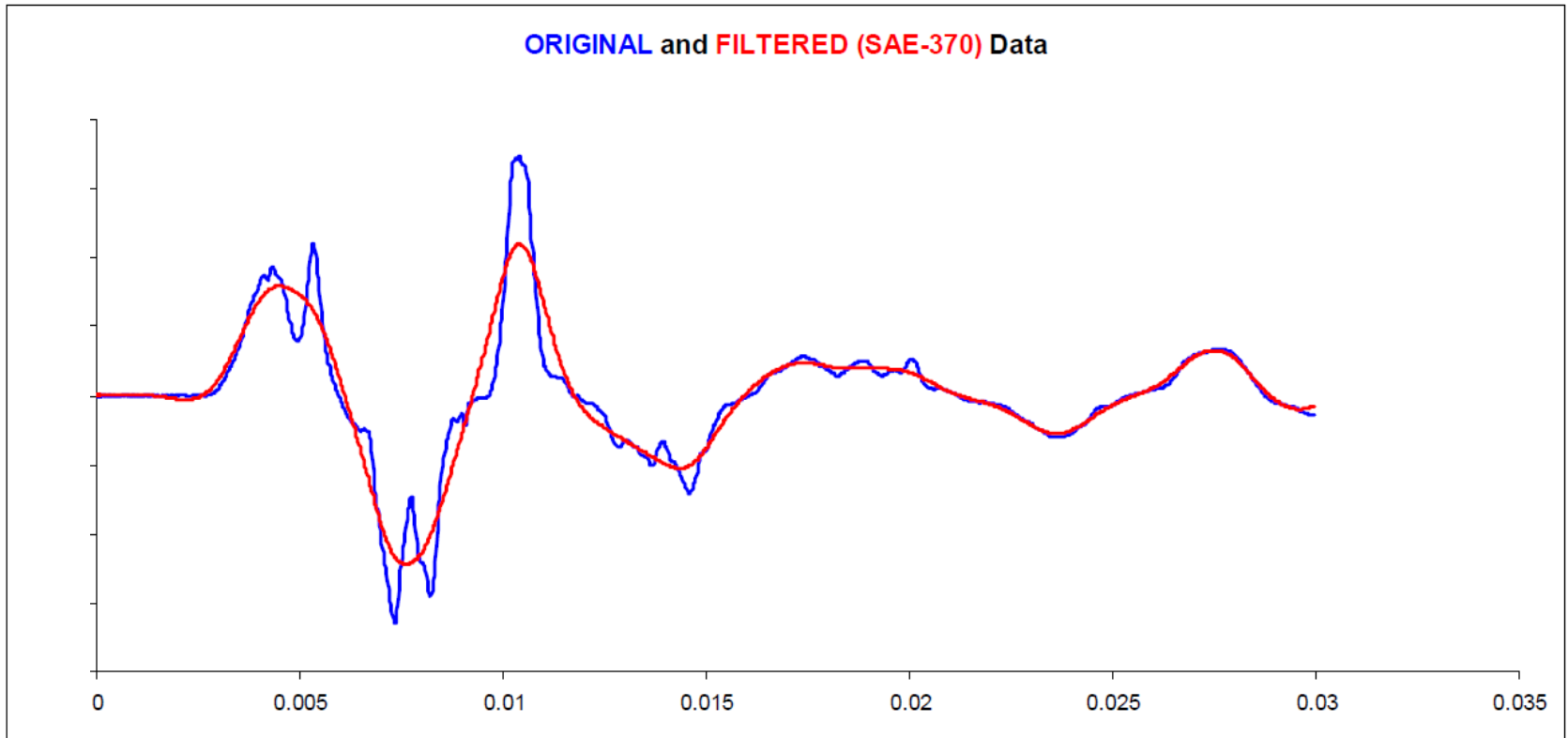
Acceleration from test and after applying an SAE-60 filter

Example: Selecting an Appropriate Filter



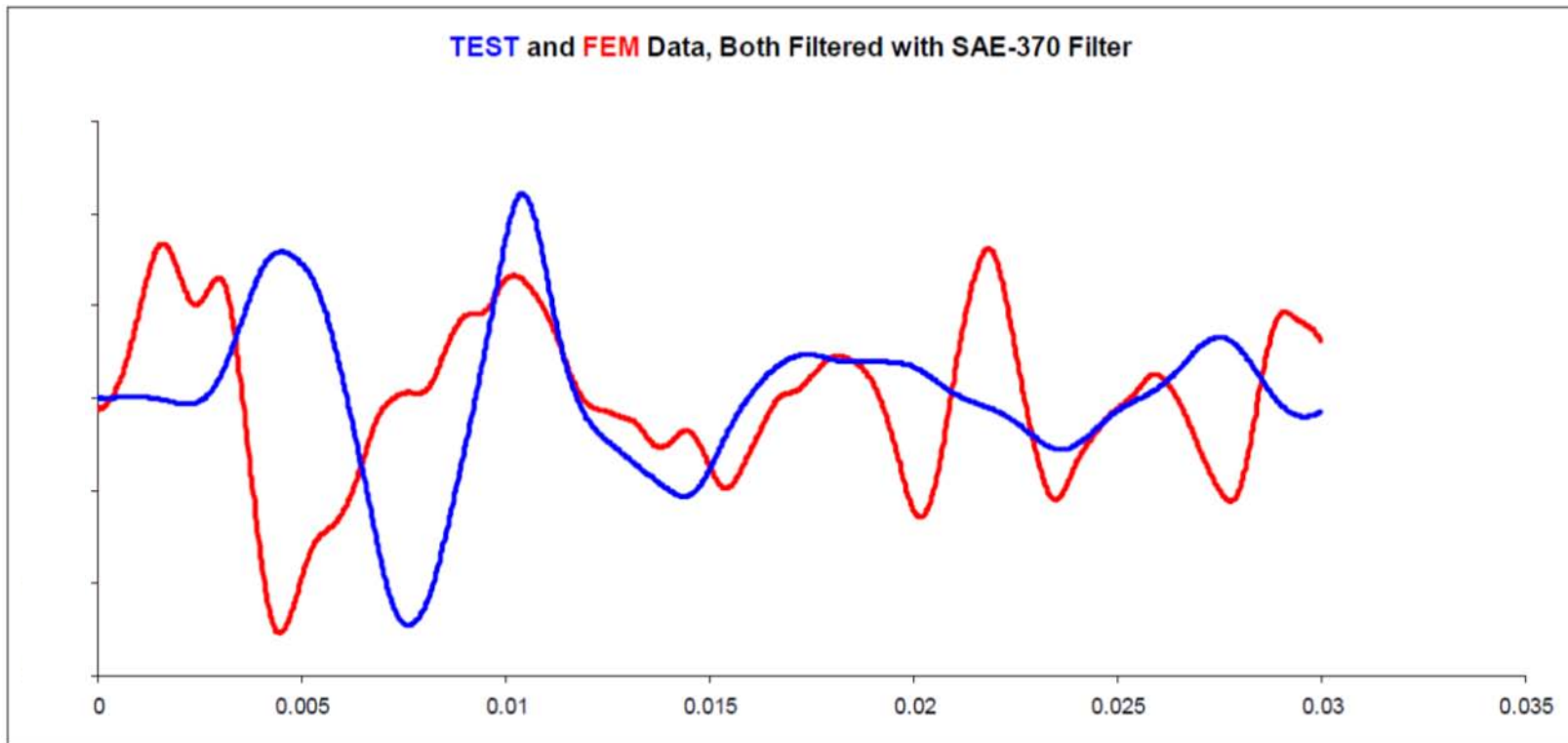
Frequency spectra of acceleration from test along with filtered data and SAE-370 filter

Example: Selecting an Appropriate Filter



Acceleration from test along with SAE-370 filter output

Example: Selecting an Appropriate Filter



Time history of FEM and test data, both SAE-370 filtered

Example: Selecting an Appropriate Filter and Applying the Validation Technique

- Up to ~9ms there is a phase problem with the simulation data
 - Shift that portion of the data roughly 3 ms to the right
 - Will line up fairly well in amplitude and frequency
- From 9 to 17 ms phase and frequency content are about right: amplitudes are close
- After 17 ms the simulation output lacks damping
 - Evidence in the frequency spectrum
 - No longer bears any resemblance to real-world acceleration

V&V process

- Defining the purpose and system of interest
- Determining intended use
- V&V Loop
 - Verify
 - Fundamental physics (model developer)
 - Vehicle model
 - Validate
 - Fundamental physics (model developer)
 - Vehicle and Occupant response
- Validation method based on modal response
 - Compare fundamental mathematical properties
 - Provides confidence and credibility in model for the intended use

Questions?

Contact

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References

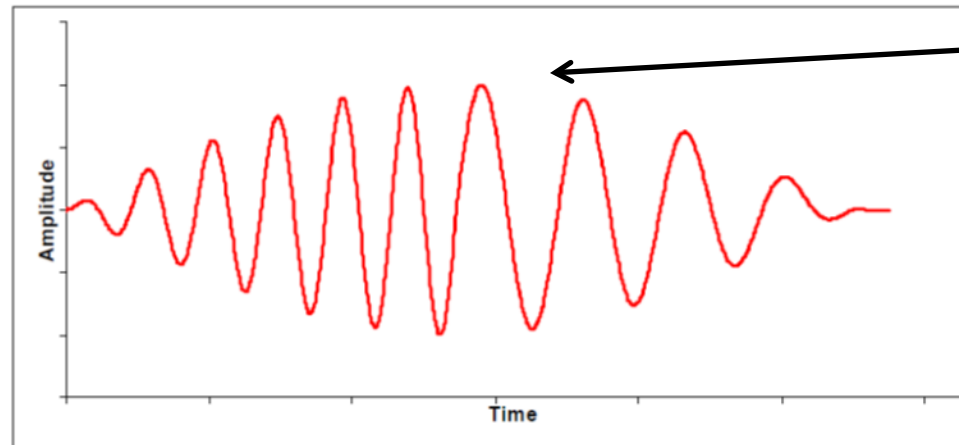
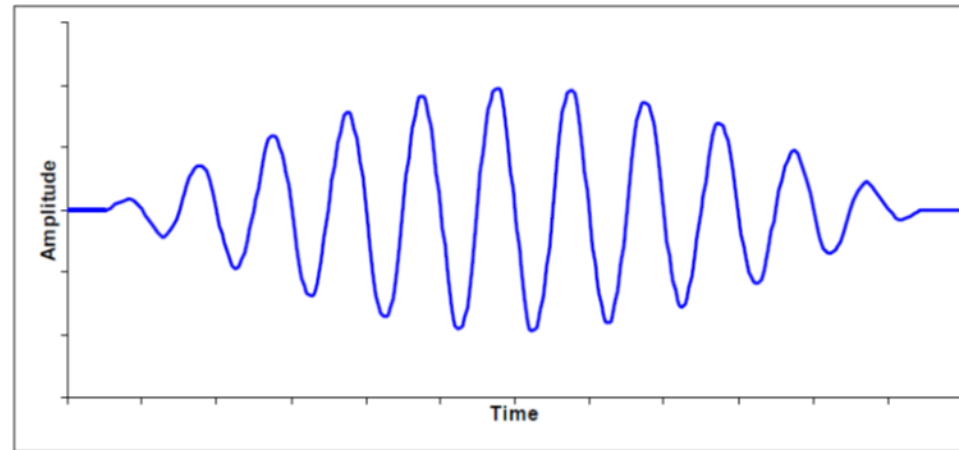
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Backup Slides

- Additional information to be gained from this technique
- When things break, deform etc...

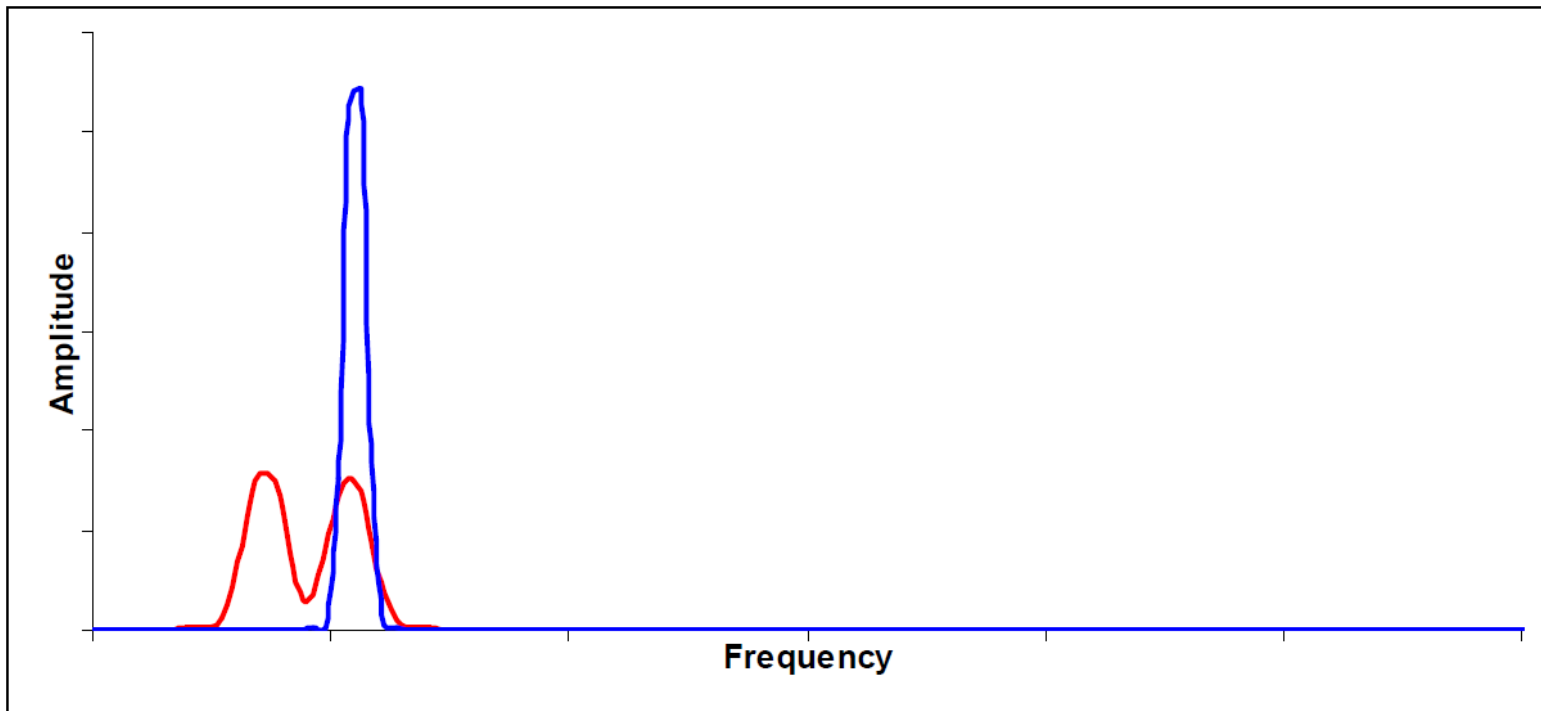
Determining when deformation occurs

- Frequency and phase are properties solely of the geometry and material make-up of the system
- Properties only change when the system becomes deformed

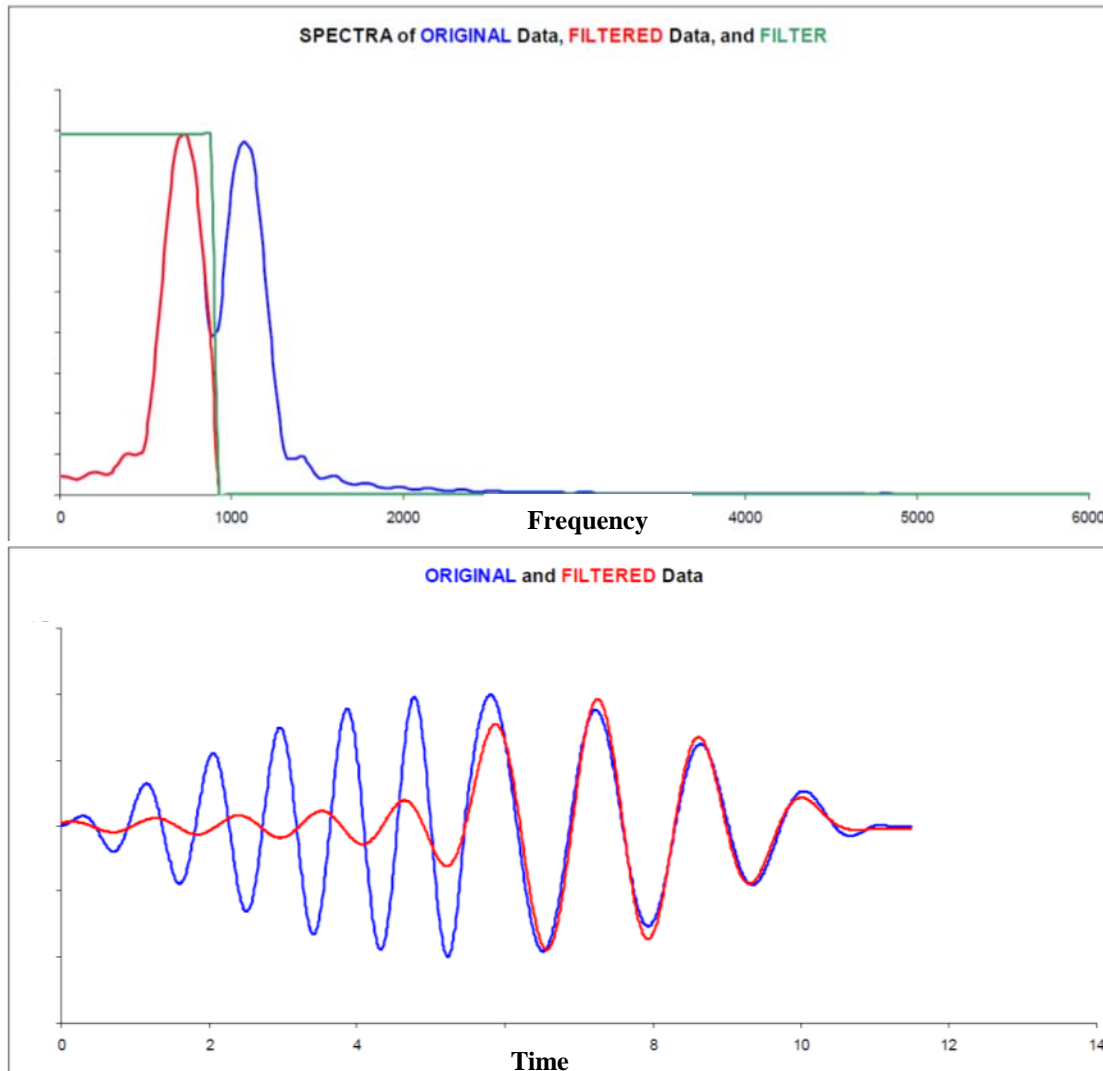


Change in
Frequency

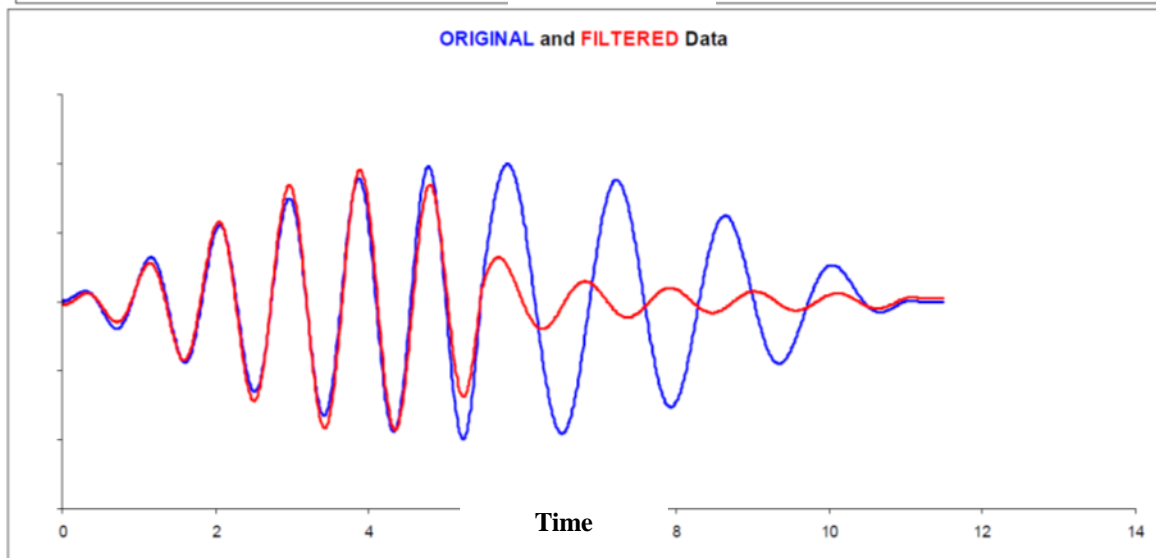
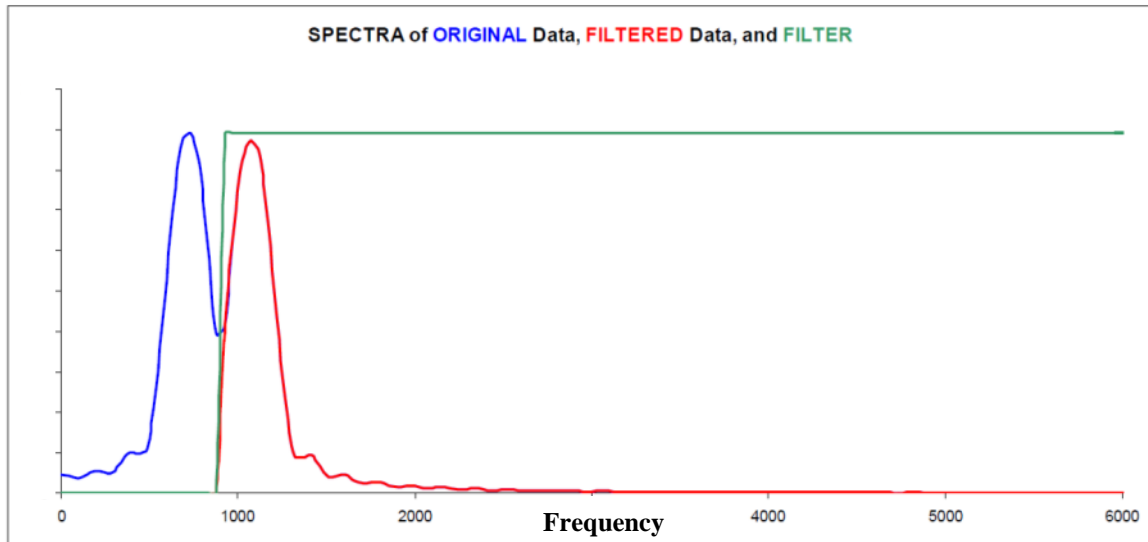
- Frequency Spectra
- Presence of two distinct time series components?
- Single time series showing deformation?



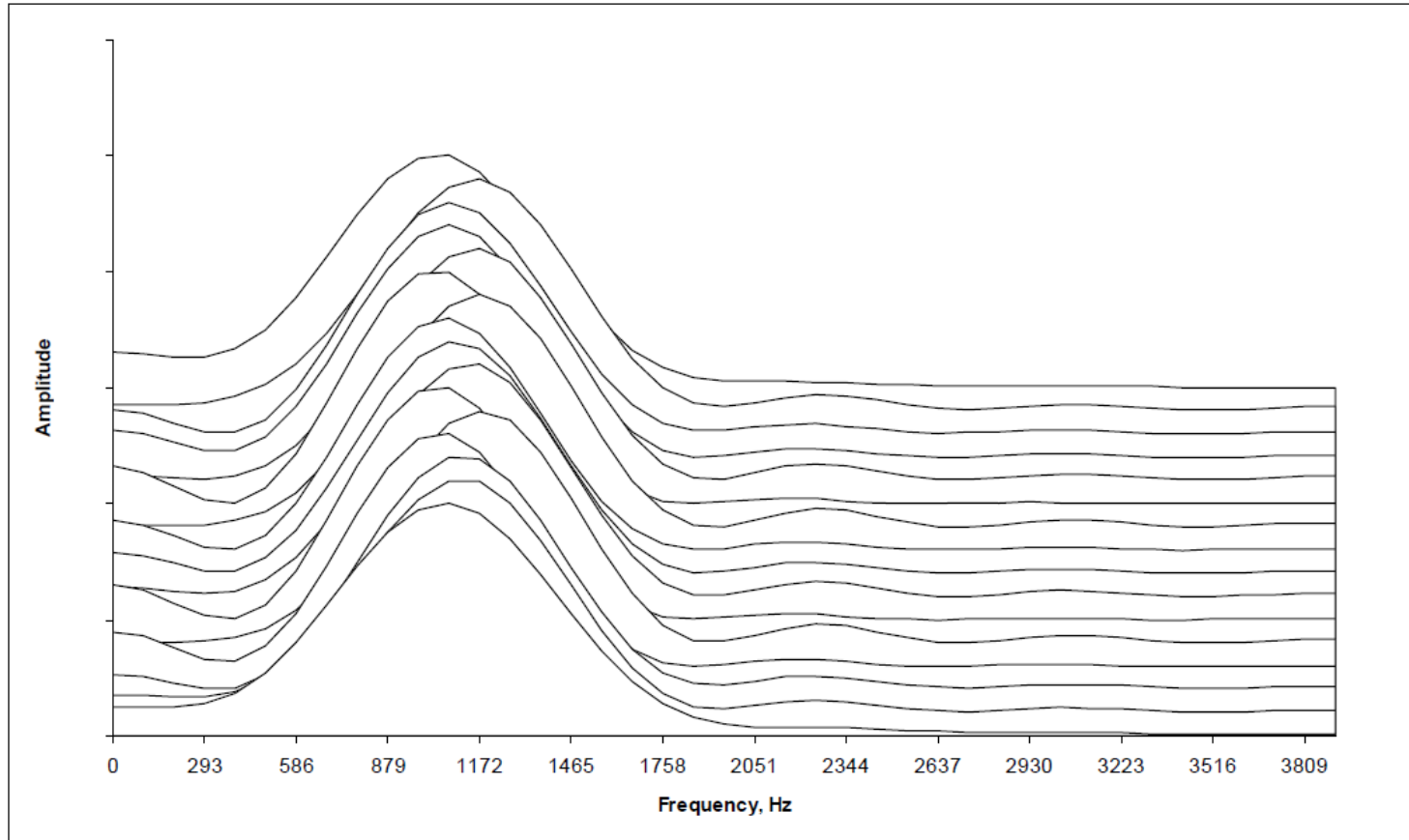
Determining when deformation occurs



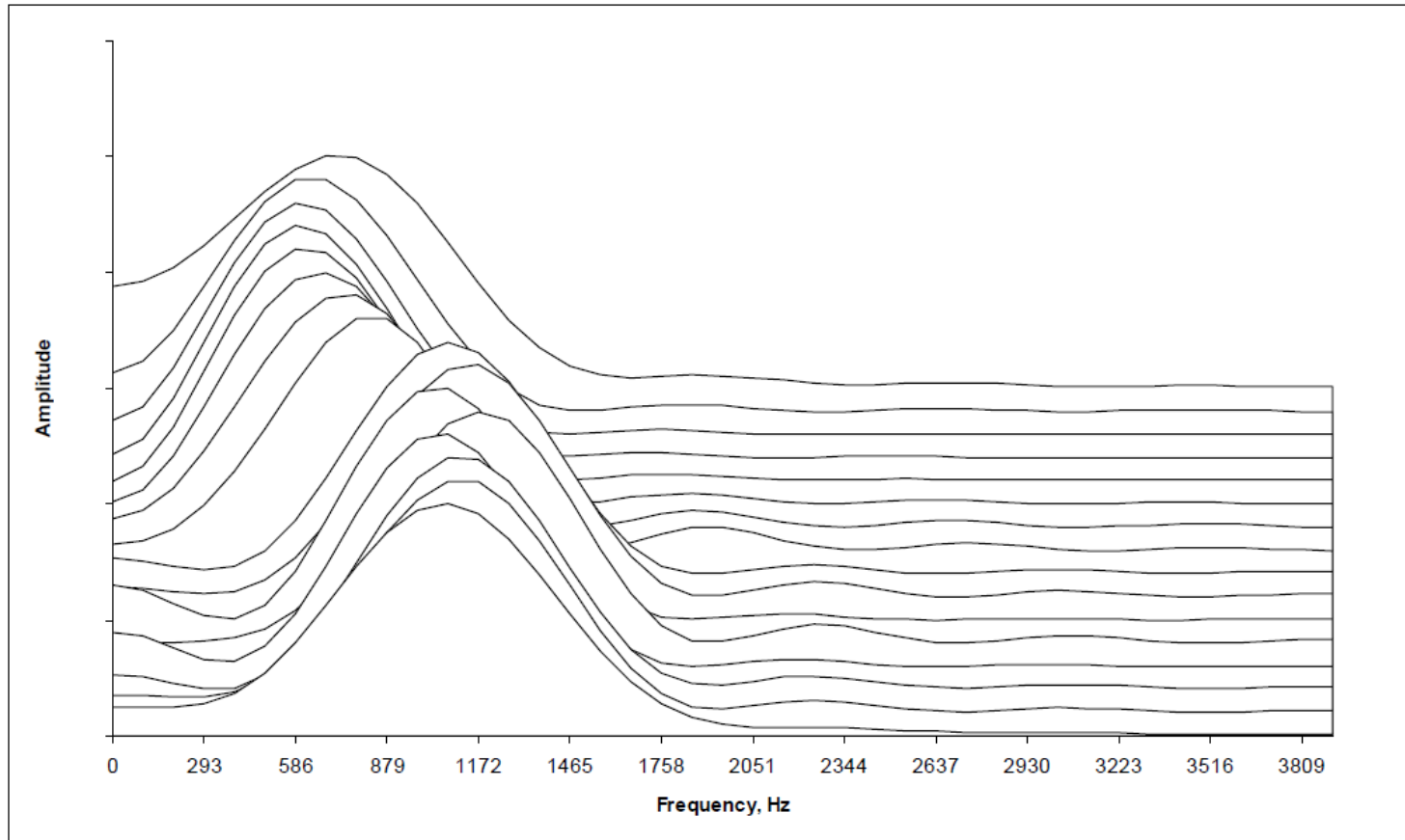
Determining when deformation occurs



Determining when deformation occurs



Determining when deformation occurs



Determining when deformation occurs

