

# U.S. Army Research, Development and Engineering Command



#### TECHNOLOGY DRIVEN. WARFIGHTER FOCUSED.

#### **Methodology for Determining Insensitive**

#### **Explosive Material Interface Reliability**

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#### Overview



- Background
- Objective
- Data Requirements
- Review of Required Tests
- Process Overview
- Conclusion





#### Background



- The Army is planning to deploy more Insensitive Munitions (IM)
  - Artillery, Mortars, Grenades, etc.
- Traditional explosive interface tests consist of go/no-go tests
  - Penalty, Bruceton, Langlie, and Neyers tests
- IM explosives with larger critical diameters will need more energy to initiate the main charge
- IM explosives require more in-depth techniques to characterize the material





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**Objective** 



- The objective of this program is to develop an alternative methodology to characterize the reliability of the interface between the fuze initiator and any high explosive (HE) IM fill
- The following methodology can be used to assess initiator/main fill charge interface reliability
  - Parameterize Reactive Flow Model(s)
  - Feed Reactive Flow Model into Hydrocode Simulation
  - Use Hydrocode Simulation to evaluate explosive interface design
    - Optimize initiator geometry, materials, and interface gaps





#### **Data Requirements for Modeling**



- Test data required to parameterize Reactive Flow Models
  - Lee Tarver Ignition & Growth, CREST, JWL++





## **Properties of Reacted Material**

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#### **Reacted EOS**

- Cylinder Expansion (Cylex) Test performed to determine Reacted Equation of State (EOS)
  - Provides Gurney Energy and explosive performance
- Explosive is detonated while enclosed in a copper cylinder
- Resultant expanding wall velocities recorded with a streak camera
- Allows for determination of parameters for reacted equation of state





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## **Cylinder Expansion Test**







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#### **Unreacted EOS**

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- Determined by measuring shock speed into unreacted HE at varying pressures
  - Wedge Test
    - Wedge of HE is shocked with a high explosive to see the detonation run-up distance
    - Data is plotted in a "POP Plot" (Pressure vs Run-Distance)
    - Unreacted EOS is determined from shock speed of HE before detonation
  - Cutback Tests
    - "Cutback" lengths of HE is shocked using a projectile or explosive
    - Cutback lengths need to be very short, so no reaction takes place
    - Unreacted EOS is determined from the particle velocity from the output of the charge
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#### **Reaction at Detonation Front**



#### **Reaction Rates at the Detonation Front**

- Pressure build-up during the detonation ramp-up is required to tune the reaction rates
  - Wedge Tests
    - The run-up distance and other run-up characteristics will be applied to the Reaction Rate Law
  - Cutback Tests
    - Cutbacks of various lengths are tested to determine the pressure build-up
    - Cutback tests are preformed at multiple pressures



## Wedge Test







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"LASL Explosive Property Data" Gibbs and Popoloto. Figure 4.02 page 294. The Regents of the University of California, 1980.

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![](_page_9_Picture_8.jpeg)

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![](_page_10_Picture_0.jpeg)

#### **POP Plot**

![](_page_10_Picture_3.jpeg)

![](_page_10_Figure_4.jpeg)

![](_page_10_Picture_5.jpeg)

![](_page_11_Picture_0.jpeg)

## **Cutback Test**

![](_page_11_Picture_3.jpeg)

- Detonation ramp-up data is needed to parameterize the reaction rates for explosive material
- Cutback test can be accomplished with an embedded-gage gun test, booster driven test, or flat flyer plate impact test
  - Embedded-Gage Gun Test provides 1D data but is expensive
    - Captures wedge test and cutback test data
  - Cost-effective alternative is booster driven test
    - Provides 2D data instead of 1D so additional computational time required for modeling

![](_page_11_Figure_10.jpeg)

![](_page_12_Picture_0.jpeg)

#### **Cutback Test Results**

![](_page_12_Picture_3.jpeg)

![](_page_12_Figure_4.jpeg)

Figure A1. Particle velocity wave profiles from Shot 1133. The input is 5.12 GPa and was created by impacting Vistal on the PBX 9501 at 0.817 km/s. The PBX is of type A.

![](_page_12_Picture_6.jpeg)

"Shock Initiation of New and Aged PBX 9501 Measured with Embedded Electromagnetic Particle Velocity Gauges" Gustavsen, Sheffield, Alcon, and Hill. Page 20, <a href="http://library.lanl.gov/cgi-bin/getfile?00416767.pdf">http://library.lanl.gov/cgi-bin/getfile?00416767.pdf</a>>

![](_page_12_Picture_9.jpeg)

![](_page_13_Picture_0.jpeg)

## **Model Validation**

![](_page_13_Picture_3.jpeg)

- Additional validation tests are necessary to ensure the predictive capabilities of the simulation
- Additional Tests include:
  - Expanded Large Scale Gap Test (ELSGT)
  - Unconfined Detonation Velocity Tests
  - 2D Corner Turning Test

![](_page_13_Picture_9.jpeg)

![](_page_14_Picture_0.jpeg)

## Expanded Large Scale Gap Test (ELSGT)

![](_page_14_Picture_2.jpeg)

- ELSGT is performed to capture the detonation wave curvature and particle velocity at the output of the test cylinder
  - The results are used to validate the Reactive Flow Model

![](_page_14_Figure_5.jpeg)

![](_page_14_Picture_6.jpeg)

Courtesy of Eric Welle

# Unconfined Detonation Velocity

Test

![](_page_15_Picture_1.jpeg)

![](_page_15_Picture_2.jpeg)

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- Unconfined Detonation Velocity Tests are performed to determine the critical diameter of the energetic material
  - Ensure hydrocode simulation will be able to predict critical diameter
    - Full-Order performance above critical diameter
    - Dying detonation wave below critical diameter
- Lesson learned from test:
  - Initial tests had charges that were too short, and showed full order detonation, but further testing in longer charges shows the detonation wave dying
    - Ensure length of unconfined material is long enough for detonation to reach steady state TECHNOLOGY DRIVEN, WARFIGHTER FOCUSED.

![](_page_16_Picture_0.jpeg)

## **2D Corner Turning Test**

![](_page_16_Picture_3.jpeg)

- Insensitive explosives usually have poor corner turning performance
- 2D corner turning test characterizes the corner turning behaviors of the material
  - Results used to validate the Reactive Flow Model

![](_page_16_Figure_7.jpeg)

U.S. ARMY RDECOM TECHNOLOGY DRIVEN. WARFIGHTER FOCUSED 2D Corner Turning Test Setup Example

![](_page_17_Picture_2.jpeg)

![](_page_17_Figure_3.jpeg)

#### Materim Bulkrige National Quality Award 2007 Award Recipient

![](_page_18_Picture_0.jpeg)

#### **Process Overview**

![](_page_18_Picture_3.jpeg)

![](_page_18_Figure_4.jpeg)

![](_page_18_Picture_5.jpeg)

![](_page_19_Picture_0.jpeg)

## Conclusion

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- To develop a Hydrocode model this process can be followed:
  - Perform Ignitions Studies
  - Use data from Ignition Studies to Parameterize Reactive Flow Model
  - Plug the Reactive Flow Model into Hydrocode Solver (CTH, ARES, CALE, ALE3D)
    - Develop Hydrocode model for each test and compare results to experimental data
      - Validate/Tune Reactive Flow Model until Hydrocode Models match experimental data.
  - Use Hydrocode Solver to asses design iterations and optimize design
- Conduct sub-scale test to confirm performance of new design
- Conduct full-scale test to confirm operation performance of updated system
- The validated Reactive Flow Model can then be applied to any munition application that wishes to utilize the specific insensitive explosive material

![](_page_19_Picture_14.jpeg)

![](_page_20_Picture_0.jpeg)

#### Acknowledgements

![](_page_20_Picture_3.jpeg)

- Army Research Labs
- Air Force Research Labs
- Lawrence Livermore National Labs
- Army Fuze Management Office
- Armament Research, Development, & Engineering Center

![](_page_20_Picture_9.jpeg)